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EDITORIAL

Editor David Fenner Tel/Fax: 01738 583832

Editorial Administrator sarah.paine@nexusmedia.com

PRODUCTION

Designer Carol Philpott

Production Manager Sifa Symons

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SALES & MARKETING

Tel: 01322 660070

Group Sales Manager Colin Taylor

> Sales Manager Tony Robertson

Marketing Executive Gillian Lawrence

CIRCULATION

Sales Development Manager Rachel Murthwaite

Circulation Manager Brian Donnelly

MANAGEMENT

Divisional Publisher Dawn Frosdick-Hopley

Associate Publisher Jez Walters

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Contents

On the Editor's Bench Dave Fenner's commentary

Milling Projects for Beginners (7) 12 Accessories to enhance the versatility of the grinding rest.

Internal Boring Bar 17 Easily made with replaceable tips

A Magnetic Picker Upper 18 A cleaner, easier way to lift ferrous swarf

20 Fitting Slip Dials to a Drill/Mill A straightforward improvement to save time and frustration.

25 Readers' sales and wants.

25 **Next Issue**

Workbench Additions (2) 26 Woodworking aids and accessories.

Oxyacetylene Welding (1) 30 Maybe out of favour for industrial production, but versatile, and available for the amateur.

Dividing on the Super Seven (2) 36 Additional methods, equipment, and improvements

40 **Trade Counter** New items from suppliers.

outlined.

Drill grinding with the Quorn 41 Several attachments and systems considered.

48 **Some Thoughts on Quick Change Tooling**

> which have evolved over many years in the workshop.

54 **Scribe a Line** Reader to reader.









Front Cover

The rustic setting of the arguably old fashioned oxy-acetylene gas welding set gives clues to some of the versatility described by Trevor Marlow on page 30.



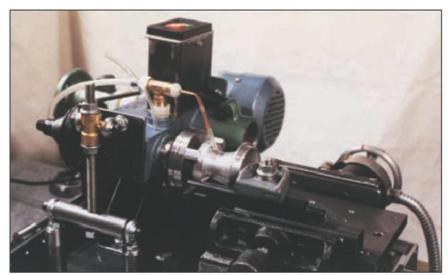
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Model Engineering Workshop Ad Index

ADVERTISER	PAGE
BW Electronics	9
Camden	9
Chester (UK) Ltd	OBC
Chronos	57
Compucutter	4
Compumil	60
Emco	58-59
Emco (single)	IFC
Folkestone Engineering	7
Glendo Corp	7
GLR	61
G+M Tools	10
Home and Workshop	IBC
IM Service	7
JC Payne	9
Machine Mart	5
Model Eng. Services	9
Newton Tesla	8
Nexus Special Interests	62-63-66
Tracy Tools Ltd	61
Warco	6
Welding centre	60



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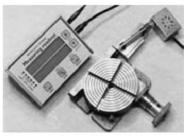




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How to Convert Wood into Charcoal &

Electricity • [Buxton] £ 8.10
This book perhaps demonstrates where you can end up if you read too many of Lindsay's books. Richard Buxton did just that, and realised he could produce good quality charcoal, and generate electricity at the same time, using the 'Producer Gas' given off during the making of charcoal as fuel for a portable, caravan type, generator. It is a neat idea and the author describes all the stages carefully, but you do need a fairly

sophisticated retort, plus "scrubber" for the gas, and to modify the generator motor's carburettor. To a clever person like you none of this should present problems and, when the system is up and running, you have non pollutant fuel, plus electricity. Good stuff! 63 page paperback, well illustrated with drawings, schematics and photographs.



Telescope Making • {1905} • [Hasluck] £ 9.20 Another reprint from Paul Hasluck, this describes how to build a 31/2" portable telescope with altazimuth mounting. It is very detailed and whilst it may be old, is certainly the book to have on constructing such an instrument. However, whilst it describes the calculations involved, what this book does not tell you is how to make the lenses; it is assumed that these will be purchased. Otherwise it is first rate. 160 pages. 218 drawings. Paperback.

AND - from other publishers:



• The Fibreglass Manual • [Noakes] £17.39 Very good guide to using fibreglass, or reinforced plastics, for a whole range of items - all full size, no models, although the techniques could be used in smaller sizes. Includes chapters on making moulds and patterns, polyester & vinylester, and epoxy laminating by hand, phenolic laminating and spray laminating, positive pressure laminating, close-mould laminating, resin casting and much more. 128 page large format

paperback, comprehensively illustrated with drawings and photographs.



• Converting a Six String Guitar to Four Strings • [Gingery] £ 5.50
From retired master of writing on engineering matters Dave

Gingery comes this new book on one of his retirement projects and it makes a good and different, project for the musical model engineer. If you convert a six string guitar to four strings you create a tenor guitar which sounds and plays like a tenor banjo, but with a sweeter and more resonant

tone. Plentiful earlier in the 20th century, as their tone was excellent for playing "mood music", four string guitars are now hard to find, but here Dave tells you how to convert a six string guitar to this configuration - it isn't just a matter of removing two strings! This book covers the conversion of an acoustic guitar, but it is surmised the principles could be applied to converting electrical guitars. Usual Gingery quality instruction - its nice to have Dave back again! 22 pages. 28 photos and drawings. Softcover.

• Making Crucibles • [Gingery] £ 8.50 We have sold hundreds, if not thousands, of books on making your own furnace, so that you can melt metal, but all of these books assume you will purchase a crucible for use with the furnace. As most of these books were written by Dave Gingery it is logical that Dave's son Vince has now written a book on making your own crucibles. Two methods are described - both depend on making molds, but differ as to how these are used. Either way looks straightforward, and a lot of fun - the second method, which involves concrete molds and some ancillary presses, is probably the best if you melt a lot of metal, and need a lot of crucibles. Covers making the clay for the crucible, firing it etc, and making crucuble tongs. Excellent instruction as always from this source. 60 pages. I 17 photos and drawings. Paperback.

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The notions of missing and control from a virtual basing section of the formatic Virtual Residual Purpose Machine Similar Triple Head Special Purpose Machine Similar Triple Head Special Purpose Machine 12 To devisite Sitting Machine (Choice of 3) 12 To devisite Sitting Machine (Choice of 3) 12 To devisite Sitting Machine (Choice of 3) 14 To devisite Sitting Machine 16 To devisite Sitting Machine 17 To devisite Sitting Machine 18 * x 30* Cast Inso Surface Table 18 * x 30* Cast Inso Table 18 * x 30* Cast Inso Table 18 * x 40* Cast Inso Table 19 * x 50* Cast Inso Table 19 * x 50* Cast Inso Table 19 * x 50* Cast Inso Table 20 * x 50* Cast Inso Table 20 * x 50* Cast Inso Table 20 * x 7* Cast	17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 17150.00 171
The notions of missing and control to the Arch Search Sear	7.759.00 1.709.00 1.759.00 1.759.00 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900
The notions of missing and control to the Arch Search Sear	7.759.00 1.709.00 1.759.00 1.759.00 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900 1.900
The notions of missing and control to the Arch Search Sear	7.759.00 1.759.00 1.759.00 1.759.00 1.90 1.90 1.90 1.90 1.90 1.90 1.90
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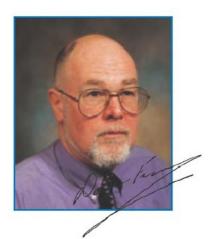


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Learning something new every day

Preparation of Issue 89 of MEW encouraged a rapid bout of computer education. Two of the articles featured computer monitor screen shots which, in the first instance the authors had saved by using the "Print Screen" facility, yielding an inkjet print. In this form they were not suitable for processing to the required standard by our long suffering studio designer, Carol Philpott. Consulting available books and manuals on Windows did not provide any answers, and it was indeed fortunate that contributor Mike Haughton had encountered the problem before, and was able to offer a solution. As it is likely that with the continual advance of computers into workshop activities, the process may be of interest to some readers. I feel that it is worthwhile to publicise the "Save" procedure for the benefit of others who may wish to store screen displays in higher resolution electronic format. To save a screen display:

Press the "Print Screen" button Click on "Start", "Programs", "Accessories", "Paint", then "Edit" and "Paste".

It is then possible to paste a copy of the screen image into "Paint" and then save to file probably as a jpg or bitmap. It can then be saved to disk or e-mailed as appropriate. Mike makes the additional comment that the higher the resolution of the monitor, the higher will be that of the image.

ON THE EDITOR'S BENCH

A correction

One reader has been in touch as having seen the hacksaw built by Mr D. Richmond depicted on page 51 of issue 88, he had been unable to track down the supplier of the castings. I have since been advised that the castings supplier was E.W. Cowell Ltd., Sydney Road, Watford. This information may assist other readers.

Miniaturisation taken to extremes

A recent lecture given by Mr Peter Rigby to the Scottish Model Engineering Trust left members with a general feeling that their model making scales are in some respects positively gigantic. The title was MEMS or Micro Electronic Mechanical Systems, and illustrated the leading edge industrial work on these devices. Actuators, gear wheel trains, and even ball races are manufactured by processes somewhat similar to those used in micro electronic chip production. The result can be a gear cluster less than the diameter of a human hair. Rotational power is produced by push/pull electrostatic actuators which, when arranged in 90 deg. Vee twin formation give self starting characteristics. Speeds of over 250,000 rpm were mentioned.

Free service from SAGA

The SAGA name frequently conjures up in the minds of the younger generation caricature images of overweight American style geriatrics on holiday. Being nearer the age of sixty than fifty, I now find myself part of their target market. For

Engineering at the College of North West London

One of the best kept secrets of the model engineering world must be the model engineering evening class which has been running at CNWL for over 20 years where enthusiasts are involved not only in the anticipated steam engines, but also model boats and trains, clocks, auto parts, microlites, and more. In a more recent development, around two years ago, the college introduced a new machine shop course where new students studying either model or production engineering, could gain an NVQ level 1 or 2 in Performing Engineering Operations. Other courses cover such things as fabrication and welding. One of the interesting administrative aspects is that the college operates a roll on - roll off system so that many students do not have to wait until September to start a course. Some also find courses that they cannot easily find elsewhere. For further information contact the college on 020 8208 5000 or check out the website www.cnwl.ac.uk

people aged over 50, Saga Circles is a free website service designed not only to help individuals revive past contacts from school, work, and the armed services, but also to make contact with others who share a similar interest. It has been developed to be easy to use and above all, to be secure, as personal details are only available if the user wishes to reveal them. Saga Circles is accessed via the Saga Group homepage at www.saga.co.uk

Bikes at Ingliston

The annual Scottish Motor cycle show took place at the Royal Highland Showground, near Edinburgh 8th-9th March, offering a mouth watering display of machinery and



action for two wheel enthusiasts. Along with many others of a certain age, we made a beeline for the classics display to find somewhere in the region of 200 machines dating from 1903 onwards. Some names, such as Excelsior Manxman, Triumph Tiger 100, and Norton Dominator evoked happy memories of a misspent motorcycling youth, long ago in the days before the Gatso and the 70mph limit. Others such as the immaculate Triton reminded me of my own similar project some thirty years ago which had to be sold due to a house and job move. The buyer was a young American, so it probably went across the pond. The differing varieties of Rickman Metisse also tend to grab my attention as one of these (a Rickman Suzuki) is an ongoing personal project.

Looking at the more modern exhibits, one might be forgiven for concluding that motorcycles are some way ahead of cars where technology is concerned. Specific power outputs are frequently in excess of 200 bhp per litre (normally aspirated), and extensive use is made of aluminium and titanium alloys, and also carbon fibre.



MILLING PROJECTS F Grinding Res



1. Milling the web on the fence.

n the last issue we completed the adjustable off hand grinding rest. The full extent of its capabilities will though, only be realised by the addition of various accessories. The sections covering these will bring the milling series to an end over the this and the next two issues of the magazine. At this stage, description of the manufacturing processes will be kept to a minimum as by now these should not present a problem. Only where something special surfaces will I go into detail. Much of the article will centre around the use of the accessories and includes photographs to illustrate the operations that can be performed. First however, very important safety considerations must be aired.

The accessories

Fence and stop assembly AS1

This is an essential part of the system being used to accurately guide the part being ground, either across the face of the wheel or down its side. A stop screw can be fitted when required to ensure that the part being ground cannot pass beyond a certain point.

Throughout the series I have emphasised that much milling work can be carried out without using a vice as the work holding device, perhaps to the point of giving the idea that it is not an essential requirement. Where a vice does come into its own, is with the smaller items which

are much more difficult to hold by other means. The adjustable fence (11) is a typical instance. Machine lower web Photo 1. Turn over, hold on web just made, and machine top surface to reduce thickness to 6mm. Drill and tap holes. Radius web ends using a file. Note that the two M4 tapped holes are shown blind. If drilled through, then grinding dust will find its way very easily into the threads.

The assembly also requires some

Harold Hall follows up with additions which allow fuller use of the Rest

turned washers. However, where simple parts are required throughout the rest of the series, I will not comment on them in the text, as the drawings should give all the information required.

Photo 2 shows the fence fitted. It can of course be in any one of the three slots. The web which fits into the slot is shorter than the slot permitting coarse adjustment of the stop screw position. Final adjustment will be achieved using the fine feed facility of the rest. You may find it easier to fit the fence (and clamp screw assembly AS 2) to the table if you remove the table from the remainder of the rest.

Swivel base clamp screw, AS 2

This enables an accessory to be fixed to the rest's table where the accessory itself feeds the workpiece, typically when using the end mill sharpening assembly as will be seen in the concluding issues.

Manufacture of the clamp screw mount (22) follows very closely that for item 11 above.

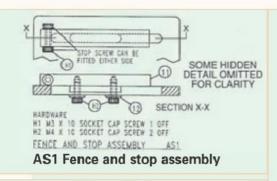
Square workpiece holder and swivel base, AS3

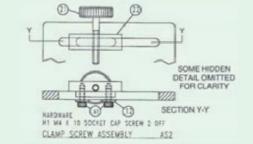
The main purpose of the holder is to hold square section lathe tools but no doubt other uses will surface. The base (31) is

IMPORTANT SAFETY REQUIREMENTS

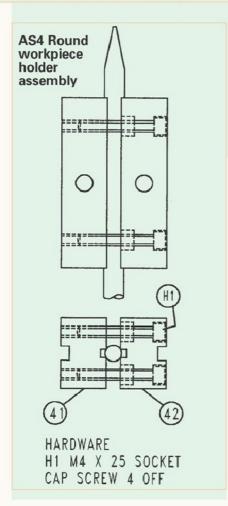
- Do wear safety glasses or face mask, and ensure wheel guard is fitted.
- Due to the item being ground often being unsupported close to the wheel when using the accessories, only take very light cuts. The depth of cut should be controlled by the fine feed and the fence rather than manually.
- Make multiple passes rather than try to remove a great depth at a single pass.
- Keep the overhang of the tool, from the accessory holding it, to a minimum.
- In view of the overhang do ensure the accessory is held firmly down on the rest's table.
- Keep the table and the sliding surfaces of the accessory as free of grinding dust as possible. This results in easier hand feeding and makes for safer working.
- The rest can be used as a conventional off hand grinding rest in which case ensure that the front edge of the table is no more than 1mm from the grinding wheel and the item being ground supported by the rest's table.
- When the grinder is running do not make adjustments to the rest, other than using the table's fine feeds,.
- Make sure that all locking levers are firmly tightened before starting grinder.
- Due to grinding dust getting into the locking lever assemblies they can become
 difficult to undo, but becoming free quite suddenly as more force is applied. This
 can cause rapped knuckles with unpleasant results. Make a lever extension as per
 Sk 1 to prevent this. However, do not use it for tightening the levers, as this may
 result in over tightening.
- As the grinding rest is not directly mounted off the bench grinder it is essential that both are mounted on a very robust base. If this is not done the rest will be able to move relative to the off hand grinder when in use. At best this may result in inaccurate results but much worse be the cause of a serious accident.

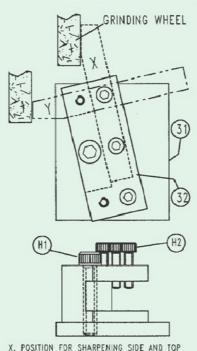
OR BEGINNERS (7a) t Accessories





AS2 Clamp screw assembly





X. POSITION FOR SHARPENING SIDE AND TOP CLEARANCES AND RELIEF. Y. POSITION FOR SHARPENING FRONT CLEARANCE AND RELIEF.

THE FIXTURE IS GUIDED BY A FENCE MOUNTED ON THE REST TABLE USING THE SWIVEL BASE (21) TO SET THE ANGLE. THIS IS ALSO USED WITH OTHER FIXTURES BUT FOR SIMPLICITY IS NOT INCLUDED ON THEIR ASSEMBLY DRAWINGS.

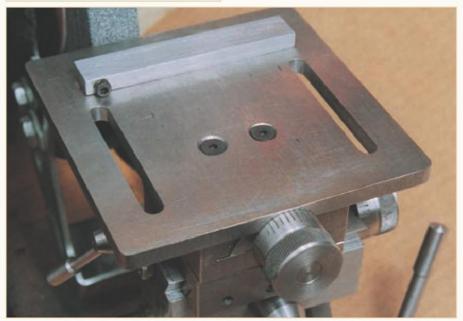
H1 M6 X 30 SOCKET CAP SCREW 1 OFF H2 M4 X 16 SOCKET CAP SCREW 3 OFF

NOTE X. LEAF SPRING (52) MAY REQUIRE BENDING TO ACHIEVE ACCURATE INDEXING HARDWARE

NOTE Y. CLEARANCE ANGLE OF GROUND TOOTH SET BY ADJUSTING LEAF SPRING(52) H1 M6 X 12 SOCKET CAP SCREW 1 OFF H2 M3 X 12 SOCKET CAP SCREW 1 OFF

AS5 Slitting saw sharpening assembly

AS3 Square workpiece holder assembly



2. Fence fitted to the rest's table. Note the stop screw at the left hand end.



3. Sharpening a square lathe tool.

used for setting the angle of the workpiece relative to the feed direction and is also used with many of the remaining accessories. For simplicity it is not shown on their drawings but can be seen in the photographs.

To machine the square workpiece holder (32) mount on an angle plate using a parallel to ensure the part is parallel to the machine table. Commence machining grove with an 8 or 10mm slot drill, working to the 5mm dimension. Open up to 13mm using an end mill. Drill and tap holes. Cut a length of 50 x 6mm for the Swivel Base Machine (31) ends to 75mm, again using the angle plate for mounting. Drill and tap holes.

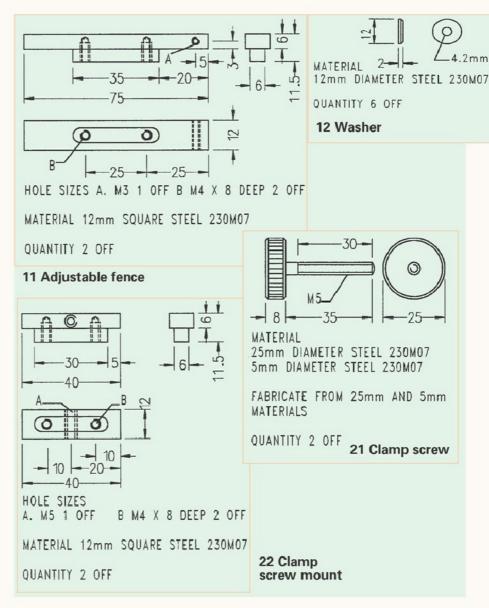
To sharpen a lathe tool, mount the holder on the swivel base at an angle to suit the tool's side relief and with the rest's table angled left to right to suit the tool's side clearance. **Photo 3** shows this operation.

If you have studied the grinding rest in detail you may consider that the angle set using the swivel base would actually be achieved using the rest's swivel facility. This is not so, its use, with a few exceptions, is purely to set the approach angle of the face being ground to the wheel.

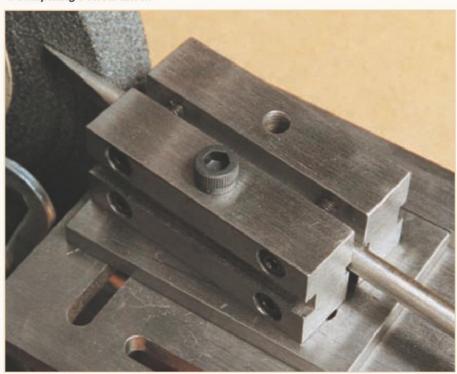
When grinding a portion from the side of a workpiece it would seem obvious that the feed direction should be parallel to the side of the wheel, see Sk2(A). However, any small error in the approach angle could cause the part to be additionally ground on its side, as in Sk2(B). In view of this, feed direction is deliberately set to an angle to the side of the wheel to avoid this possibility. Sk2(C) shows this arrangement. This may seem like a procedure to overcome the accuracy limitations of the home workshop, it is though frequently adopted practice in industry. Sk2(D,E and F) show the same situations relative to the front face of the wheel. This angle, set by the rest's swivelling facility, should only be a degree or two maximum.

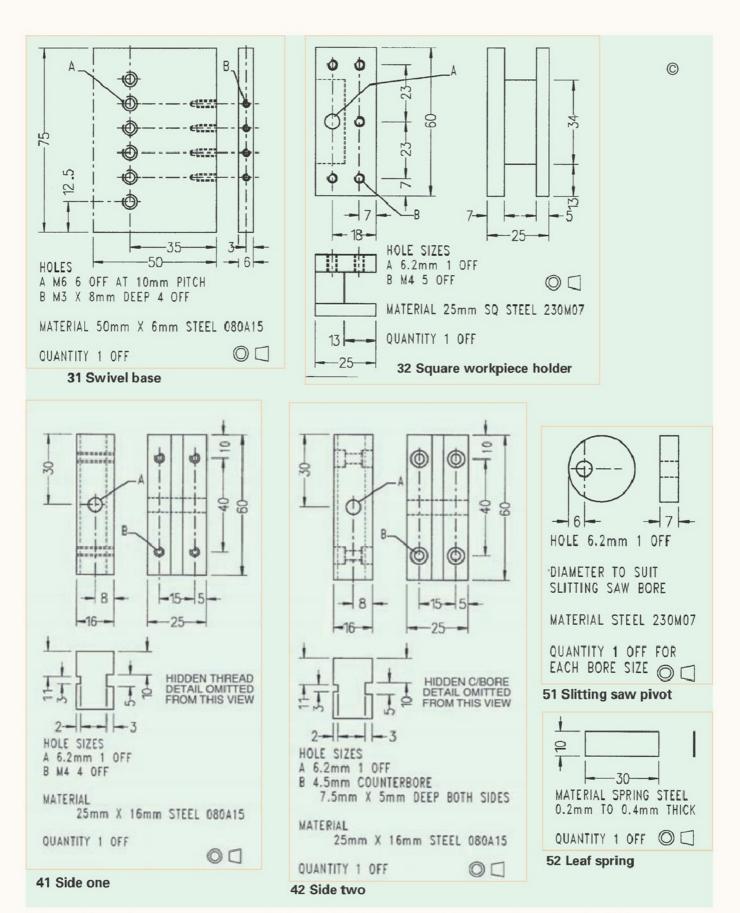
Round workpiece holder AS4

This is normally mounted on the swivel



4. Sharpening a screw driver.



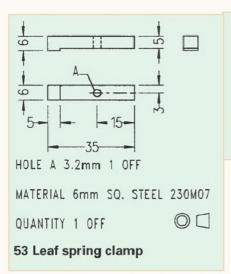


base, similar to using the square workpiece holder, and is used typically for holding screwdrivers, a wheel dresser and round section lathe tools, etc..

Cut two lengths of 25 x 16mm, one each for Side one (41) and Side two (42). Using an angle plate for supporting parts, machine ends and grooves. The grooves

must be central or else they will not align if one part is turned over relative to the other. Drill, tap and counterbore.

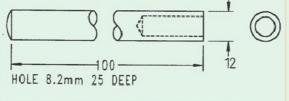
When clamping round items, the two halves of the holder should be progressively tightened ensuring that the halves remain parallel to each other, and present flat top and bottom surfaces in use. During use to sharpen a screw driver (Photo 4) the holder will need to be removed from the swivel base, turned over, and the second side ground. This will necessitate the fine left to right feed being adjusted again as it is unlikely that the result on both sides will be the same without this being done.





5. A parallel end to the screw driver is easily achieved, not the case when attempting this by off hand grinding

The screw driver end will now require grinding to bring the thickness to that required. Remove the holder from the swivel base turn on its side and grind the end to establish the required blade width. Do not be tempted to feed this free hand, even for this simple operation it is safer to use the fine feed, assisted by the fence, making multiple passes until the required blade width is achieved. Sharpening a screw driver free hand may seem like a simple exercise but anyone who has tried it will have experienced the difficulty of getting the two sides parallel. Photo 5 illustrates how good a result can be achieved, and simply, with this accessory. The photograph also shows a centre



MATERIAL 12mm DIAMETER STEEL 230M07

SK1 Locking lever extension

punch which will be discussed later.

Typical other uses are wheel dressing, Photo 6, (note this still uses the fence and the swivel base) and sharpening round lathe/boring tools. Note that, with the fence mounted at right angles to that in the photo and the wheel dresser turning through 90 degrees on the swivel base, the right hand side of the wheel can be dressed. However, dressing the side should be kept to an absolute minimum as it will reduce the width of the wheel and therefore its strength.

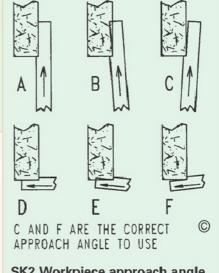
Slitting saw sharpening assembly AS5

This comprises the swivel base with a few simple parts (51, 52 and 53) added. The method for sharpening slitting saws should be clear from Photo 7. Do remember that the saw is fed by hand with the swivel base held firmly against the fence and the saw against the swivel base. The inward fine feed is used to control depth of cut. With the large teeth on the saw no stop is required. However, with an accurately dressed wheel, saws with very small teeth can be ground when a stop fitted to the fence will be necessary to avoid the wheel touching the adjacent tooth. In this case the left to right feed would be used to accurately set the stop position. The bush on which the saw rotates is drilled off centre to provide adjustment for differing saw diameters. The leaf spring may required bending at "X" as shown, to improve indexing on smaller tooth saws.

This completes the minor assemblies all of which can be seen in Photo 8.

End mills and slot drills

Whilst many items, typically lathe tools, screw drivers, etc., can be sharpened free hand with some success, this is almost impossible in the case of end mills and



SK2 Workpiece approach angle



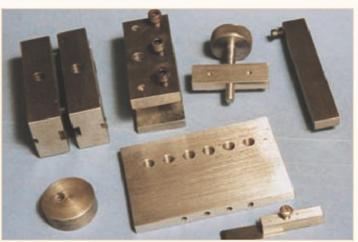
6. The same accessory used for the screw driver is also used to hold the wheel dresser.

slot drills. An accessory enabling these to be sharpened, both on their end teeth and cutting edges, is the subject for the remaining two issues.

7. Sharpening a slitting saw.



8. The set of minor accessories.



Model Engineers' Workshop

INTERNAL BORING BAR



hen making a model engine, be it steam or internal combustion, one is frequently making jigs, fixtures and special tools, most of which are applicable only to that particular project. In the process of making the cylinder head for a small two stroke aero engine of my own design, I needed to machine a combustion chamber of 0.625in. diameter, 0.145in. depth with a radius of 0.125in. Accuracy was essential to ensure the calculated compression ratio. I needed a tool to start in a hole of 0.375in. diameter. Achieving accuracy in diameter and depth would not present any problem. But hand grinding an accurate radius would be another matter altogether so far as I was concerned! I use indexable carbide inserts where possible and therein, I thought, lay the answer! Needless to say, round inserts of the size required could not be found at the time, and there does not appear to be a commercial boring bar for that insert configuration. (I have since come across the 5mm round tips supplied by Greenwood Tools, and it would undoubtedly be possible to redesign the seating to accommodate these.) Anyway, solving problems is one of the satisfactions we gain from our hobby, so make one!

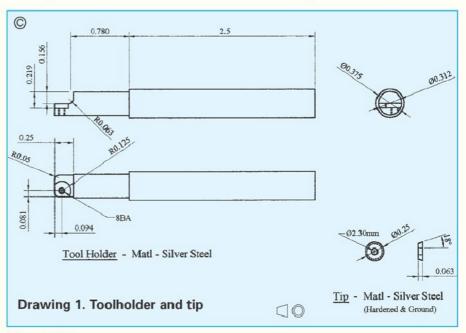
Tool Holder

(Drawing No.1)

Take a 3in. length of %in. diameter silver steel and reduce it to %in. diameter for about 1in. (The dimensions 0.780in. and 2.50in. shown on the drawing are not critical).

Mill the shoulder, preferably with a radiussed endmill. Using an edge finder, or whatever is your customary method, centre the spindle over the position indicated on the drawing. Drill through 1.80mm. Without altering the setting follow with a ¼in. slot drill to take out the insert seating to a depth of 0.0625in. (I reground the end teeth on the slot drill to remove the concavity so as to produce a completely flat surface for the insert to seat on. Alternatively, one could make a D-bit for the purpose). Tap the hole 8BA. Complete by hardening the first ¾in. inch or so to protect the seating and the thread.

Shelley Curtis describes his solution to boring small holes



Tool Tip

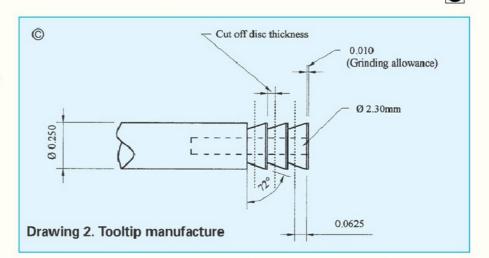
(Drawing Nos.1 & 2)

This is made from ¼in. dia. silver steel, to the dimensions and angles shown in the drawing. Before commencing, note that a cut off disc is used later and its thickness needs to be added to the 0.0625in. and 0.010in. dimensions at the turning stage. Set over the lathe top slide to machine the relief angle, producing the finest surface finish you can, because it will not be ground. (Whilst you have things set up, it's a good idea to take the opportunity to make some spares.) Drill 2.30mm dia. to a depth appropriate to the number of inserts you are making.

After hardening, set up on the tool and cutter grinder. With a cup wheel remove the grinding allowance on the top surface of the insert to produce a sharp cutting edge. (Don't overdo it or the diameter will be reduced). Replace with a cut off disc and part off to length. Repeat for the remaining inserts.

Assemble using an 8BA socket cap screw to secure the insert to the tool holder.

This tool was made for a specific job but I foresee that it will be used in other applications, so it's a welcome addition to the "armoury". Additional tools, to accommodate other radii, can easily be made when the need arises.



A MAGNETIC PICKER UPPER



1. Magnetic Picker Upper finished project.

o, this has nothing to do with record players or gramophones, but is a little weekend project that will find many uses around the workshop and home for picking up small ferrous objects. Examples might include separating filings from sawdust, finding that elusive screw in the ubiquitous muck(!) on the workshop floor, and collecting swarf for transfer to the waste bin. But whatever you use it for, do keep it away from floppy discs and tape cassettes; and colour TV screens and monitors!

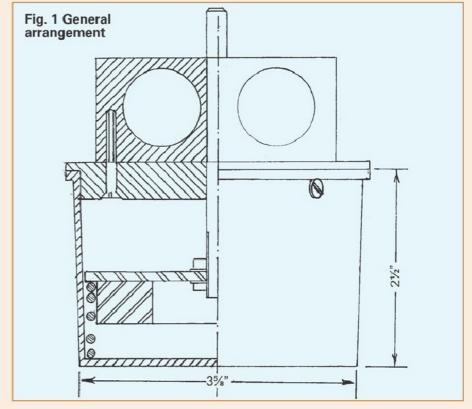
Description

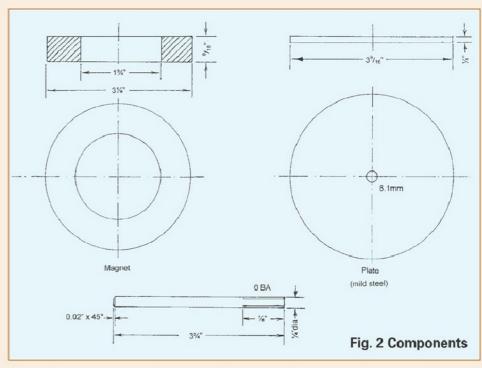
The unit is based around one of a pair of focussing magnets salvaged from an old TV set, and is housed in a plastic container. One salvaged from a loudspeaker might serve equally well. The ring shaped magnet is "stuck" on to a ¼in. thick steel disk which rests on a brass spring. The

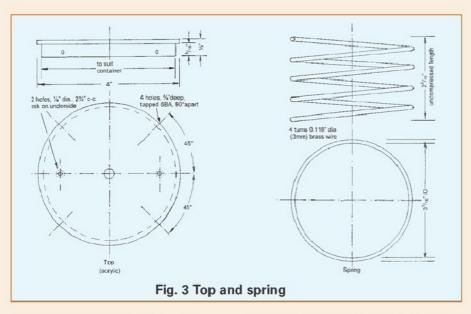
2. Top removed showing plunger / magnet assemble resting on spring.



Paul Boothby has come up with a cheap and cheerful idea for cleaning up ferrous swarf, filings etc.







disk acts as a convenient anchor for the magnet and for the plunger; and therefore its actual size bears little relevance to the operation of the unit. Indeed, the photographs show that two flats exist on this part, simply because it was cut from a piece of 3in. wide plate, rather than from a wider (4in.) piece. The spring holds the magnet away from the bottom of the container. When the plunger is depressed, the disk acts against the spring, and pushes the magnet down to make contact with the bottom of the container. By placing the unit on top of a pile of say, steel washers or swarf, and depressing the plunger, the magnet attracts magnetic material to it. By releasing the plunger, the spring decompresses, the magnet lifts away from the bottom of the container, and so attracted items falloff.

Design considerations and construction

Construction is straightforward, and requires little comment. The container needs to be reasonably tough, and must be non-ferrous. Most margarine type tubs, whose size is ideal, will be too flimsy to use. The prototype was made from an old

fish-food container ("Aquarian" Goldfish Flakes, 50g size). The dimensions shown in the figures are based on this container. UBM sell putty (1 kg size) in suitably robust pots but these are slightly taller than that used. If such a taller pot is used, then the spring and plunger may need to be redesigned. The original snap-on lid used on the fish-food container, although pretty thick, was found to be too flexible: when the unit was lifted from the bench, the lid flexed so much under the weight of the assembly, that it allowed the magnet to move away from the bottom of the container, causing all attracted items to falloff prematurely. (The force compressing the spring was acting through the plunger, fingers and thumb onto the lid, thus flexing and moving the lid, and container bottom further apart). The lid was redesigned lid using ½inch thick acrylic sheet, and held in place with four- 6BA cheese head screws. When drilling the holes for these screws, first fit the lid on to the container, and drill through both.

The spring should be made from nonmagnetic material to prevent ferrous objects adhering to the rim of the pot after the plunger has been released. Brass seems to fit the bill nicely. It needs to be stiff enough to support slightly more than



3. Interior view showing spring location.

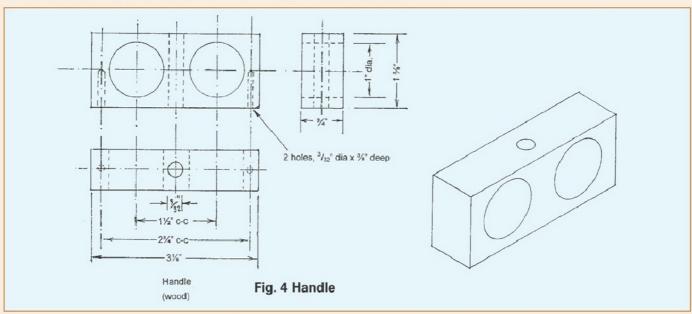
the combined weight of the magnet, the plunger and all attracted materials. If the spring is too weak, then when the plunger is released, the magnet will not rise, and this will prevent attracted materials falling off. Conversely, a spring that is too strong will be awkward to use, and is expected to cause fatigue to the fingers and thumb after prolonged use.

The plunger, like the spring, needs to be made from non-ferrous material, such as brass. Its design shows what appears to be an excess of screw thread. This allows for the initial adjustment of the height of the plunger, and compensation for any of the flexing of the container base when the plunger is depressed. Set the height of the plunger so that the top protrudes 3-4mm above the handle when the magnet touches the bottom of the container.

The handle was made from hardwood, sanded and varnished, and mounted on the top with two 1" x No. 4 countersunk woodscrews.



4. Picker Upper - partly assembled.



FITTING SLIP DIALS TO A DRILL/MILL



1 Components of table X drive. Note angular position of roll pin hole and "moth eaten" shim washer.

y drill/mill is the smallest manifestation of the well known range of Taiwanese machines; it is designated RF-15. The dials have black markings engraved on a satin chrome background, and are very clear; but they were fixed in relation to the shaft rotation. It is possible to use a lead pencil to mark start and finish of settings and to later to remove these marks with an eraser, but this is nowhere near as convenient as the use of slip dials, such as were fitted to my Taiwanese lathe saddle, cross slide and tailstock. I later modified the lathe top slide dial to a slip form using the same concept as the lathe designer had for the original slip dials.

After 15 years or so I finally tired of the pencil and eraser routine and set out to convert the drill/mill to slip dials also, and this article relates to that exercise.

Assessment

In order to devise a suitable arrangement it was first necessary to dismantle the existing X, Y, and Z feed assemblies to determine exactly how they were put

2. Hardwood cradle with knockout hole.



together and their part dimensions. It was intended also to take the opportunity of this dismantling to ascertain whether there was sufficient space to substitute ball screws in order to eliminate the significant backlash in the X and Y table motions. The thrust bearings were found to be stuck in their housing with old grease but were set free with the extractor depicted in drawing 4(a).

The X and Y arrangements as found are shown in drawing 1 and the Z arrangement in drawing 2(a) - this latter will be separately addressed later in the article.

What was immediately apparent was that while the design concept for the X and Y movements was conventional and sound, the detail design and particularly the assembly workmanship was poor. Reference 1 indicates that for thrust ball bearings of the size used the axial clearance should be in the range 0 to 0.075 mm; what was found was for the x movement 1.35 mm and for Y 0.35 mm. The actual axial play of the feed screws in their nuts was almost negligible - so the ballscrew idea was set aside as unnecessary.

3. Boss, dog clutch end and dummy shaft. Also shown is bearing extractor.



Philip Amos describes a simple modification to a Mill /Drill to improve convenience and accuracy

Essentially there were two related problems -

(i) The collar (part 2) was a very loose fit on the screw shaft and hence its axial location against the end of the screwed portion was rather indeterminate - see drawing 5(a) which displays a possible extreme cant of 0.75 mm.

(ii) The dog clutch/engraved dial was fastened to the screw shaft with a roll pin in a hole very carelessly positioned and drilled. On the X screw the hole was not at right angles to the shaft (see **photo 1**) and on the Y screw the hole was not through a diameter of the shaft.

Design

After consideration of the dimensions of the various parts it was decided that it would be possible to re-machine original part 1 so as to retain the engraved dial and the dog clutch end. To do this the part was carefully cut in two (using a hacksaw to minimise the amount of axial material removed) and the two sawn surfaces faced smooth and at right angles to the axis.

A new boss was designed to extend the dog clutch, and on which a bored out engraved dial could turn. This boss embodied a radial spring loaded ball to provide frictional restraint to hold the dial in its set circumferential position.

The same dimensions apply to both X and Y assemblies, which differ only in the length of the screws, and that the X screw is right handed while the Y screw is left handed (both with Acme threads).

Detail

It was clear at the outset that multiple assembly/dismantling operations would be required. While it is possible to drive out the roll pins and drive them in again, these are really a semi permanent arrangement. To initially remove them, a hardwood block was machined to match the radius of the dog clutch end with a hole drilled opposite the position of the roll pin -see photo 2. This block then acted as a cradle to support the dog clutch while the roll pin was driven out with a pin punch into the hole in the wooden block, thereby avoiding damage to the dog clutch/engraved dial surface.

To improve convenience the 5 mm diameter hole for the roll pin was drilled out $\frac{1}{2}$ inch diameter (5.56 mm) and then opened out to accept a No.4 taper pin. The

taper pin (38 mm long) is easy to tap in and out and positively retains the parts in their intended position.

It will be seen from **drawing 3** that provision is made for the new boss to be attached to the dog clutch end by means of two socket head capscrews and that there is also a dowel pin to transmit torque. Together with the main shaft hole and the side hole for the ball and spring, the boss starts to look a bit like a Swiss cheese. The sequence of operations required is lengthy but all are straightforward- the sequence is listed at **Appendix 1**.

From comparison with my lathe it seemed that an appropriate thickness for the engraved dial might be 6 mm. Starting from a scale diameter of 49 mm this means a nominal boss diameter of 37 mm. As the dog clutch end is 40 mm diameter it provides a small shoulder which limits axial movement of the engraved scale ring.

The diametral clearance on my lathe slip dials averages 0.08 mm which corresponds to Tubal Cain's suggested Normal Running Fit - see reference 2. Thus an outside diameter of 36.92 mm was adopted for the boss and 37.00 mm for the engraved dial hole diameter.

The axial length of the engraved dial measured 21.74mm, and the boss axial length aimed for was for this plus 0.08 or 21.82 mm to ensure that the dial could turn freely on the boss without axial constraint.

The side hole in the boss for ball and spring was made 6.5 mm diameter copying the lathe precedent, for a ball 6.35 mm diameter and a stock spring 6.1 mm diameter. The spring selected had a wire diameter 0.8 mm and the axial space available for it was 6 mm. When the ball is fully depressed the spring should not go solid - a solid length of 5.5 mm will result from just over 6½ turns which was adopted.

The dog clutch main hole is a somewhat loose fit on the screw shaft, and it was desired that the new boss should be close fit. Thus when these two parts were to be joined together a short stepped shaft was made to fit both parts and ensure they were coaxial - see drawing 4 (b) and photo 3.

In order to perform their function the thrust bearings must stand proud of their housing if engaging an item of greater diameter than the outer diameter of the bearing. This is particularly so on the outside of the housing, and can be achieved by the use of shim washers between bearing and housing if necessary.

The final matter to address is the axial length of the stop collar which engages the end of the screw thread. The shape of the thread end is depicted in drawing 5. If the collar internal diameter is a close fit on the screw shaft, its axial location will be determined by its engagement with the corner between shaft and thread - this is not a good design to rely on for resisting significant thrust. Measuring the axial space between this corner and the outer transverse surface of the thrust race is quite a problem as most of the normal measuring devices do not seem appropriate. I used gauge blocks and a magnifying lens to observe this (see photo 4), but I am not very confident of the accuracy of the result. At any rate I used this information to define the thickness of the thrust collar. The whole assembly can then be checked to see that it rotates freely without any axial play. If tight the thrust



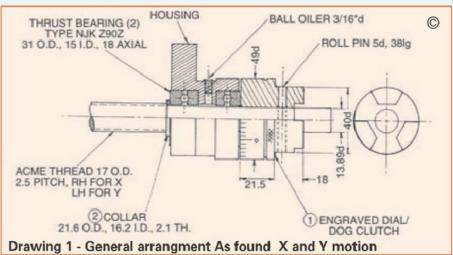
4. Measuring axial gap for stop collar.

collar can be filed or ground thinner. If there is play it can be removed with shim washers.

When this desired state has been achieved the stop collar can be secured to the screw shaft with Loctite (680) adhesive, with the other components in position to ensure that the collar is in the correct location.

The inside diameter of the engraved dial

is machined to dimension with the part protected from the chuck jaws with thin card. When assembling the scale ring on to the boss it is necessary to first fit the stepped shaft mentioned above so that the ball and spring can be positioned without falling out into the bore. The scale ring can then be moved axially over the boss, depressing the ball against the spring with



SOCKET SETSCREWS

5/16'BSW
1/4'BSW
3/8' LG

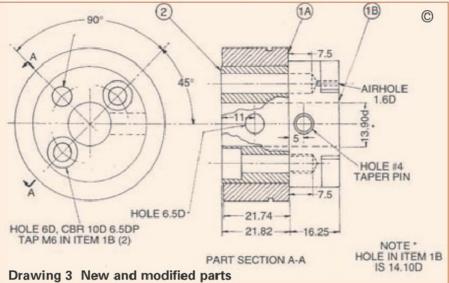
GAP 0.1

HANDWHEEL BOSS

(A) AS FOUND

Drawing 2 General arrangement
Z motion







6. Drill jig and assembly tool.

the flat of a screwdriver blade until the scale ring itself is in position to hold the ball down.

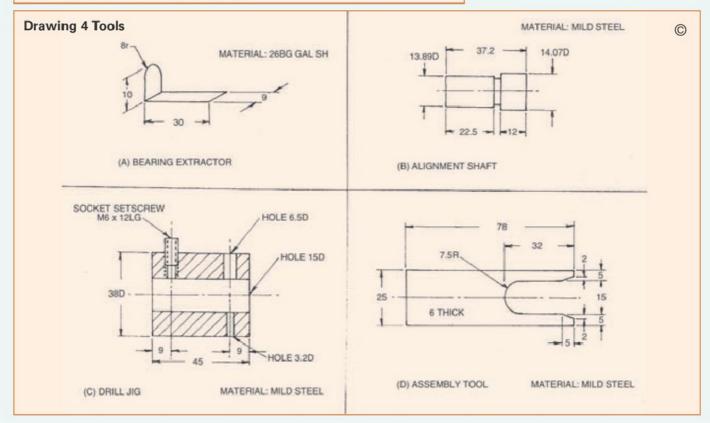
The assembly of the dog clutch/boss and scale ring is then moved axially on to the screw shaft which pushes the stepped shaft out. It is important to note that the spring and ball hole must be radially at right angles to the taper pin hole in the screw shaft, lest the spring and ball expand into that hole and jam the axial movement - in which case it all has to be taken apart and started again.

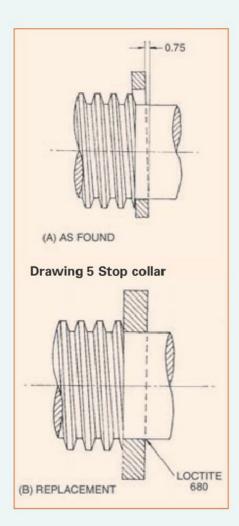
When all these steps have been completed it only remains to coat the screw thread and the thrust bearings with Molybdenum Disulphide grease and reassemble on the mill/drill.

The components of the X drive arrangement after modification are shown in **photo 5**.

In my case there is now no axial play in the bearings, and the total arrangement backlash is -

X direction 0.25 mm Y direction 0.10 mm.





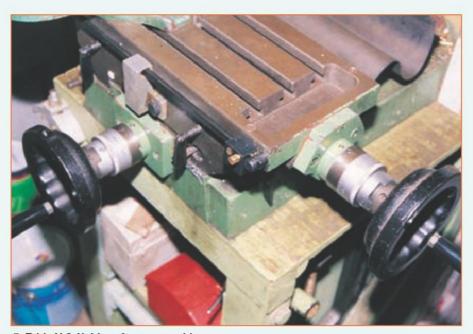
Down feed

In this case there is no axial movement to contend with as both operating handle and engraved ring are secured by socket setscrews bearing on a flat on the operating shaft. When the setscrew for the engraved scale is loosened that scale rotates freely on the shaft - in fact it is a bit on the loose side. There is not much room for means to achieve the required slip scale, but it was decided that if a hole was drilled right through the main shaft in a position clear of the existing flat it would be possible to fit two balls with a spring between them to provide the frictional restraint on the engraved scale.

In this case the available axial space for the spring was 5 mm. For wire diameter of 0.8 mm this would allow just over 6 turns before going solid when the balls were depressed to the surface of the shaft.

A simple drilling jig as shown in drawing 4 (c) and photo 6 was made which was held in axial and radial position by a socket setscrew engaging the shaft flat. Using a pistol drill a 3.2 mm diameter hole was drilled through the shaft using the back hole of the jig as a guide; then a 6.5 mm diameter hole was similarly drilled using the front jig hole.

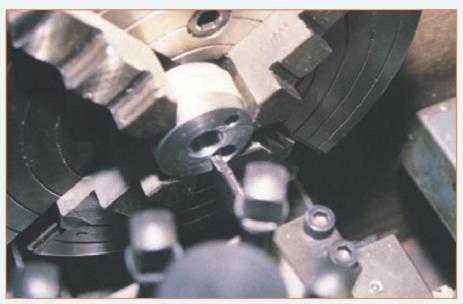
The two balls plus the spring had a free length of 20 mm. Compressing this combination to the 15 mm of the shaft diameter was fraught with difficulty. After several unsuccessful attempts including the loss of a ball and a spring, a tool was made as shown in drawing 4(d) and photo 6 which allowed the combination to be



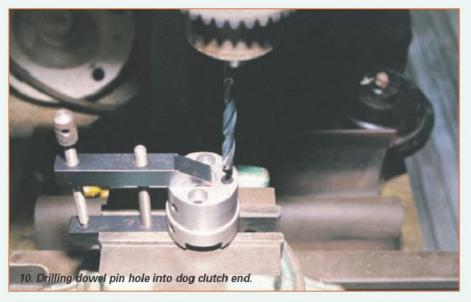
7. Table X & Y drive after reassembly.



8. Quill Z drive after reassembly.



9. Finishing counterbore to size.



Appendix 1

Sequence of Operations. Dismantling - X or Y Table Movement.

- By undoing 2 capscrews in the bracket housing and unwinding, unship the feed screw from the drill/mill.
- 2. Remove handle.
- Measure axial play and distances from end of shaft to dogs.
- Mark shaft end and dog end with file nicks for future orientation.
- Knock out roll pin using wooden support cradle - photo 2.
- Dismantle components, clean in kerosene and inspect.
- Position dog end on shaft with No. 10 drill through cross hole. Clamp handle to this axially and with its own setscrew to shaft.
- Remove No. 10 drill and open out progressively to %inch diameter.
- 9. Ream hole for No. 4 taper pin.

Preparation

- Measure shaft diameter (13.85 mm) and diameter of hole in scale/dog clutch (13.90mm).
- Hacksaw scale drum from dog clutch end.
- 3. Face both sawn surfaces with attention to faces being at right angles to axis.
- Measure resulting thicknesses of scale drum (21.74 mm) and dog clutch end (16.25mm).

Boss manufacture

- Cut billet (38 mm diameter) to length of two bosses (45 mm each) plus 50 mm for chucking - 140 mm total length.
- Face both ends in turn in 3 jaw chuck.
- Skim full length to make circular, half a length at a time.
- Groove 23 mm from end (i.e. about 1 mm wider than the scale drum).
- Turn to diameter 36.92 mm as far as groove.
- Mark centre on end.
- Layout end for holes and punch centres.
- Drill, bore and ream main hole 13.90 mm diameter.
- 9. Part off.
- 10. Face to length 21.82 mm (equals scale

- drum thickness plus 0.08 mm).
- 11. Mark off and centre punch side hole.
- Drill in side of mill/drill hole 6.5 mm diameter.
- 13. In 4 jaw chuck drill and ream dowel hole 6.35 mm diameter. Drill tapping size M6 (5.0 mm diameter) and counterbore 10 mm diameter 6.5 mm deep (2) initially with 9.5 mm diameter slot drill then opened out with mini boring bar - see photo 9.
- 14. Make stepped dummy shaft see drawing 4 (b).
- 15. Mount on stepped shaft with dog clutch end, clamp together, drill and ream (D-bit) dowel hole 7.5 mm deep and drill air relief hole 1.6 mm diameter - see photo 10.
- 16. Fit dowel.
- Drill tapping size M6 in dog clutch end
 5 mm deep. Remove boss and tap hole M6
- Open out holes in boss to clearance (6 mm) diameter.
- Assemble boss to dog clutch end with 6.35 mm diameter dowel and two M6 socket head capscrews 22 mm long.

Scale drum manufacture

- Drill and bore scale drum to diameter 37.00 mm using boss as gauge (as well as measuring with telescopic gauge and micrometer).
- Trial assembly on boss with spring and ball with dummy shaft in boss bore.

Stop collar manufacture

- Measure axial distance from shaft end to end of Acme thread.
- Assemble two bearings, bearing housing and boss/dog clutch end on shaft fixed with taper pin, and measure axial distance from end of shaft to inner face of inner bearing.
- Deduct 2 above from 1 above to compute collar thickness.
- For confirmation also measure this with gauge blocks – see photo 4.
- 5. Skim 25.4 mm diameter raw material to approx 25 mm but circular.
- 6. Drill inside diameter ½ inch (13.49 mm).
- Part off to dimension of gap plus 0.1 mm.

held in place while the engraved scale was moved axially over it. The operating handle was then fixed in position with a 0.1 mm feeler gauge arranged to define the axial gap.

Conclusion

The intended aim to equip the mill/drill with slip dials was achieved, and the amount of backlash reduced to what might be expected in an ordinary machine tool.

Photos 7 and 8 show the arrangements after modification; it is hard to detect any external change in appearance.

References

- 1. Machinery's Handbook Revised 21st Edition 1982.
- Model Engineers Handbook Tubal Cain 1981.
- Ream inside diameter to fit screw shaft (13.90 mm).
- Assemble parts to check for axial tightness or play.
- 10. Correct by filing or shim washers.

Reassembly

- When satisfied no axial play in bearings dismantle, and fit scale drum, spring and ball to boss with dummy shaft in boss bore.
- Coat both bearings and Acme screw with Molybdenum Disulphide grease.
- 3. Reassemble all parts taking care that the hole for the spring and ball is at right angles to the taper pin hole in the shaft. As the boss/dog clutch end is passed on to the main shaft, the dummy shaft is pushed out. When the spring and ball are beyond the taper pin hole the boss/dog clutch end can be turned until the taper pin can be fitted in its hole.
- The screw is wound back into its table nut and the housing bracket resecured with its two capscrews.

Operations For Z quill movement

- Undo two socket setscrews to remove handle and scale ring.
- Make drill jig to drawing 4 (c) and photo 6.
- Secure drill jig to shaft with socket setscrew engaging shaft, and jig end abutting machine casting.
- Using hand held pistol drill make pilot hole through shaft 3.2 mm diameter with rear jig hole as guide.
- Likewise open out hole to 6.5mm diameter using jig front hole as guide.
- 6. Make spring and ball assembly tool to drawing 4 (d) and photo 6.
- Insert spring and two balls in 6.5mm diameter hole and compress length from 20 mm to 15mm overall with tool.
- Move scale ring over the balls to abut the machine casting.
- Re-secure handle to shaft with socket setscrew using 0.1mm feeler gauge for axial gap.
- Plug hole in scale with shortened socket setscrew.

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- For sale: Moore and Wright internal micrometer in padded box, range 2in. to 8in. in very good condition. £30-00 please phone 01442 863 026 (West Herts).
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QUICK TIP

From Mr P Foyle of Basildon, Essex.

hen sharpening scissors, the scissors are opened wide and the edge of each blade in turn is held at the correct angle and slid up and down the oilstone. It can be difficult to apply enough pressure and to hold the narrow blade at the right angle consistently. My idea is to reverse the procedure, grasping the blade in a vice, and using the stone in the manner of a file. It is much easier to apply pressure this way, and to maintain the correct angle. Ensure that the stone is kept well oiled. A similar technique may be found useful on garden shears.



NEXT ISSUE

Coming up in Issue No. 91 will be



Milling Projects for Beginners

Harold Hall describes a fixture to sharpen end mills and slot drills.

Friction (and bearings)

Philip Amos considers the theory, use, and avoidance of friction.



Improving the Conquest Lathe

Alastair Sinclair outlines his modifications to this popular machine.

A New Approach to Form Relieved Gear Cutters

Eric Rumbo has devised a system for producing such cutters which avoids the usual complex "Backing off" machining process".

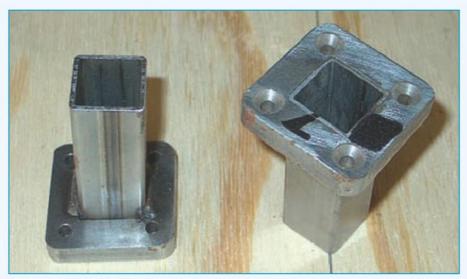


Issue on sale 20th June 2003

(Contents may be subject to change)



WORK BENCH ADDITIONS (2)



1. Sockets for bench clamps.

his second article follows on from the first with the detailed descriptions of the remaining parts. Safety minded readers should note that in several photographs, guards have been removed to give a better view.

Bench clamps (5)

I do not have an end vice and this system was made up to counter this omission. It consists of a series of Hollow Rectangular Sections (H.R.S) welded to steel flanges which are set at an angle of 5 degrees, (photo 1). These are then set flush in the bench, one end unit with its taper towards the right, and the remainder set at various distances on the left hand side and with the angle this time to the left. In this way the parts that fit into the H.R.S. will always seat themselves more firmly into the bench receptacles and not have a tendency to lift out under pressure.

The flange holes for the H.R.S. were first machined out at the correct angle before the tubes were fitted and then welded into position. (As a brief aside make sure that these parts are well supported on the underside by fitting them through a longitudinal stringer or other suitably reinforced part of the bench)

The clamp and end components are modified from a standard clamp system that originally would have been fitted to a timber beam. These, after modification, were bolted to specially made "Tooth stems" (photos 2 & 3). The system works well enough but I need some more fitted into the wings so that they would then be available for use with longer jobs. One end of the clamp can be seen in use in photo 4.

Elektra Beckum saw adaptation (6)

This saw is very good and comes complete with laser alignment. What I did not realise at the time of purchase was that it could not be used in a similar manner to a radial type saw, in that it it was not possible to lock the blade at a fixed height

3. Fixed clamp, commercial and home made parts.



Peter Rawlinson concludes his selection of woodworking aids.

I therefore came up with the additional two parts that give the saw extra versatility, and do not detract from any of its original uses.

The assembly consists firstly of a 10 x 16 mm steel bar bolted into place using a specially shaped gusset, (photo 5). The height has been set to allow 100mm. timbers to be slid underneath. The adjustment is achieved by means of a threaded arrangement consisting basically of a tapped bar working within a tube. A ball bearing is set into the end of the rod and runs freely on the steel bar. This can be seen close up in photo 6, and the adjuster is shown in use in photo 7. Approximately 60mm.of movement is available. The modification works well and does not get in the way of normal use.

Dust suction connector



I am given to understand that many hard woods and also M.D.F.(Medium Density Fibreboard) give off nasty chemicals, some of which are carcinogenic in nature. It is therefore best to try to prevent these dust particles getting into the air in the first place. Although wearing a mask will help, a dust extractor is clearly a more desirable solution to the problem.

Most of today's wood working tools are equipped with dust extraction outlets, in the main being 100mm or 4in. diameter male tubes or some close approximation to these sizes. However if a number of tools are available and space is limited then the fitting of each of these to a permanent dust extraction system is very costly and indeed is not feasible if the tools are to be moved around the workshop.

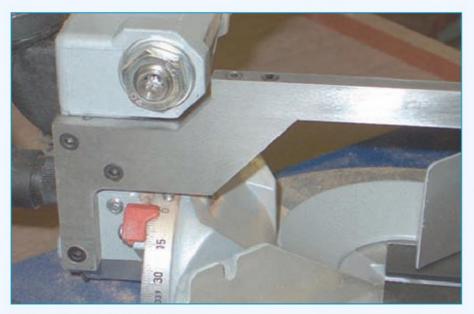
My answer to this is to have one dust extractor with a three or four metre flexible

4. Clamp in use.



2. Adjustable clamp.





5. Close up of bar and attachment.

hose and as we are only using (in general) one machine at a time we can transfer the hose as required between machines. This however is not as easy as it seems as the tube sections vary a little in size and can be either slightly tapered or parallel, so that the hose either fits too easily and then falls off, or is a struggle to put on.

I have made up from a piece of 115mm diameter cast nylon a tapered fitting that clamps on to the flexible hose (with 2 cable ties.) This is bored with a 6 degree inclusive taper and fits nicely on all of the six machines that I have. I also intend to add 100mm dia. outlets to my other machines as I have found that any restriction in suction hose diameter reduces the extractor efficiency considerably. The fitting has been equipped with a simple handle and if I find a problem in the future I can use an elasticated luggage strap to hold it in place. The connector and hose are shown in photo 8.

As an aside, the piece of nylon that I had was solid, and naturally I hated the idea of throwing away the central core as swarf. I found that I had a 90mm dia. hole saw which would cut in to a depth of 35mm. I therefore machined the length to

6. The adjuster unit.



70mm and used the hole saw from both ends. This now leaves me with a piece of nylon some 80mm diameter and 70mm long, potentially more useful than a bin full of swarf. This sounds simple but the operation required suds to be used continuously, and required repeated cuts of just a few thous at a time as the teeth clogged very quickly. Fortunately some time ago, my tailstock was modified, being fitted with a rack and pinion feed instead of the normal screw type arrangement. Even working this way, this it must have taken nearly an hour to remove the core.

Height setting gauge

These devices are, in fact, commercially available from at least one tool catalogue, but making one is a very quick and simple exercise, and therefore worthwhile. It consists of a steel centre section with brass strips top and bottom to give a reasonable foot print, so ensuring that it

will stand on its own with good stability. Mine is graduated at both ends, one for measuring up (table saw and router) and the other one down (for the radial saw and for setting a stop on the bench drill.) It is first fabricated then set up on the mill for making the step cuts. I chose two millimetre intervals using the D.R.O. for accuracy. In the absence of such gear, it can equally be done using either a clock gauge or by careful attention to the machine dials. The completed gauge is illustrated in photo 9.

Hold fast bosses (9)

My older bench features a couple of bosses for Stanley hold down units, and I wanted to incorporate these into the new bench. The commercial items are simple flanged bosses with a series of grooves cast inside. I found that I could replicate approximately by turning these features with a specially ground tool having a nose radius of 3.5 mm. Commercial and home made items are shown in **photo 10**. The bosses are incorporated in the top and in the legs of the bench, the latter for holding long pieces on edge.

Acrylic infill discs (10)

The end wing has a hole through it. This provides a route for the dust hose when the wing is in the lowered position. When the wing is raised for use, the hole is closed with a disc, (photo 11), and this stops the gremlins pushing the tools through it.

A second aperture occurs over the bobbin sander In normal use the bobbin is removed from the sander. There is then an open hole for the saw dust to drop through, and a second disc (photo 12) is fitted to save clearing this out

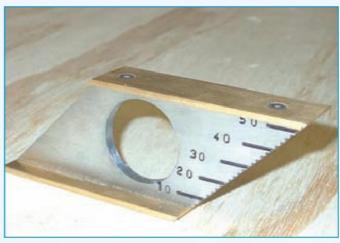
These discs are turned from acrylic (Perspex) 6mm thick. The manufacturing procedure was to first cut out oversize on the band saw, then drill the central hole for the handle. Then, using the central hole, they were then mounted on an arbor and turned (very carefully) to size.

7. Height adjuster set for half jointing.





8. Dust connector adapter, handle and hose.



9. Height gauge showing increments.



10. Commercial and home made collars.



11. Acrylic disc with handle up.

Tenon cutter guide (11)

This unit is used in conjunction with a table saw for guiding the long side cuts when making tenons. Again such things are available commercially, but at a price. I have made mine to be able to cut both vertically and also horizontally, because I had made some of the parts for an earlier abandoned project.

The base of the accessory consists of a pair of circular discs mounted together with a central pivot pin and radial slots with through bolts for locking the angle into position.

The lower disc has fitted to its underside, a bar that will fit into the mitre fence slot on the table. The fit should be free running with no play. The top disc with a slide (the same as a top slide on a lathe.) will give accurate adjustment for the tenon thickness. The vertical plate fitted to the front of the slide is fitted with



a clamp system to hold the timber that is to be cut. This description so far covers the basic machine and next we move on to my addition. This is a system for swinging the front plate to an angle of 45 degrees. I have therefore pivoted the plate at the bottom and fitted two shaped plates with curved slots to take clamping screws to hold it firmly in place. Photos 13 and 14 convey some of the detail aspects of the construction. The machining procedures and techniques are relatively straightforward and probably do not require detailing. The device can be seen in use in photo 15.

Standardisation of "T" slots (12)

Since I had a number of different mitre squares which could not be interchanged between machines, I decided where possible, to standardise all the machine T" slots. After giving the problem some thought and taking measurements of the material wall thickness surrounding the existing "T" slots, I concluded that there would be sufficient material left for strength. In the main the better quality mitre gauges featured "T" slots which were %in. wide (19mm) and required an undercut of 23mm x 4mm deep, within an overall depth of 10mm. This rather drastic remedy would be applied to three machines, the bandsaw, the table saw, and the sander. The last would also benefit from a new slot at right angles to the face.

Band saw

This tool had been made with sufficient material for the final machined slots. It was set up on the milling machine using a sub table and an enlarger plate, then clamped in place using four machinists clamps which held the table with no problems. The existing slots were first opened out to 19mm wide x 10mm deep and a key seat cutter was then used to cut the "T". This cutter was 16mm dia. x 2.3mm thick so that two cuts were required for each side of the slot. This then gave the required 4mm deep cut.

Sander

The existing slot in the sander table was enlarged in the same way. However there was insufficient material to cut the new one that I planned. I therefore machined

13. Tenon guide showing angular adjustment features.

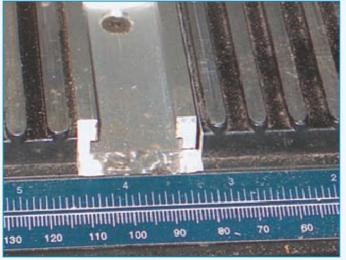




14. The slide adjustment handle was salvaged from a Boxford lathe.



15. The tenon guide in use.



16. New "T" slot inset fitted to table saw.



17. Adapter fitted to fence with featherboard.

the underside flat, screwed into place a 50mm x 10mm. steel stiffener, and proceeded to machine this in the same way as before.

Table saw

The worst case was the table saw which has a table of die cast aluminium approximately 5mm thick. I had already purchased a "T" slot extrusion which was ½in. deep, (12.7mm) x 32mm.wide. It was then found that standard routers can be used to machine aluminium, and thus could be used to cut the old slot out.

I therefore used my smaller T5 Router and fitted this with a standard ‰in. end mill and machined the old "T" slot out to a width of 32mm. This was cut out using a straight edge as a guide and was most

18. A rear view of the adapter.

successful, taking cuts of 2mm. Exact measurements were then taken and two pieces of 8mm square steel were then Screwed to the underside of the table and then machined such that the overall depth was 12.8.mm. A 50mm wide steel plate was then screwed to these and these then formed a groove 32mm.wide x 12.8mm deep. The "T" slot extrusion was then fitted and screwed into place, as can be seen in **photo 16**.

I have since found that the aluminium used for making the fence and other items, can be cut very successfully using the Elektra Beckum saw, when fitted with an 80 tooth tct blade. I have also started using my wood band saw on aluminium as well and have found no problems and as yet, no increased wear on the blades.

New saw fence (13)

The table saw when bought was not an expensive model, and the fence was not to my liking, so I decided to build a new one. As the saw was to be bolted in place on the bench it was not necessary to mount the new fence directly on the saw itself, as it could equally be fixed to the bench.

It consists of a sliding bar of 25mm diameter bright mild steel and uses two bronze bushes fitted into an aluminium housing which holds the fence, the measuring vernier, and the lock. The fence itself is made from a piece of 50mm x 25mm aluminium and is fitted with one

"T" slot on the top to take various adapters and a second one on the side which allows it to be mounted on to the slide housing. This allows the fence itself to be pulled back to avoid a "Nip" situation occuring on some operations. I have also made a short fence that can be fitted as an alternative.

Featherboard adapter (14)

This fits on to the top of the fence and gives the added height that is required to fit a vertical feather board. It is made in two pieces for the very good reason that my scrap box did not contain a single piece of aluminium large enough for the job. The fence and featherboard adapter are shown in **photos 17** and **18**.

I hope that my short foray into the woodworkers territory may in some small way be of help to some other readers. As usual I am always happy to be of help if possible but phone only please and I will not return calls for the obvious reason.

Peter Rawlinson, Charing, Kent 01233 712158.



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OXYACETYLENE: MU(JUST A WAY OF



1. A portable and versatile apparatus.

n earlier articles you were invited to consider a cheap MMA ("stick") welder, then introduced to the many virtues and values of the MIG welders, and later given an outline of the special benefits that can be derived from TIG welding in the home workshop. In this the general benefits and practice of oxyacetylene are outlined, with some particular areas of detail to be covered in a follow up.

Even in a well equipped versatile workshop, we may come to realise that we still lack some capabilities. The wish list could include methods for better brazing, softening and cutting metal, and releasing rusted parts. After a period of observation, we come to realise, if we are prepared to pay for it, that one item fulfils these needs and comes in the form of the torches, hoses, regulators, gas bottles etc. that make up an oxyfuel capability, with oxyacetylene (Fig 1) being the most familiar and most popular of such systems.

Why oxyacetylene?

What is so special about oxyacetylene compared with other mixtures? Why oxygen? What is the advantage of acetylene over, say, propane or butane, available as those gases are for immediate collection from the local hardware shop? The answer is, in short, that the combustion of oxygen and acetylene offers the combination of a very high flame temperature and very good heat

Trevor Marlow examines the good old fashioned gas welding process and the allied uses for the equipment.

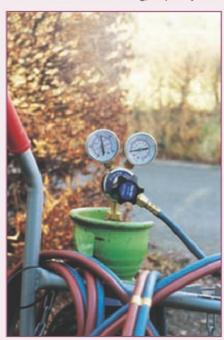
transfer, having better values than any other common combinations of gases. (MAPP gas is a close second, but isn't generally as popular or available as acetylene, it is not considered further in this article.)

Is the welding of thin steels difficult with oxyacetylene?

The answer is, in short, not at all. In everyday terms, it is an "absolute doddle". Provided you get reasonable equipment, look after it, and set it up properly, particularly re the delivery pressures, then the gas welding technique is incredibly easy. (Welding with oxyacetylene is often referred to simply as "gas welding").

When to gas weld and when not to gas weld

In industry and commerce, oxyacetylene welding is now less widely used because it is a slow process and not well suited to a lot of fabrication requirements. However, let there be no doubt about it, for thin carbon steel sheet or tubing, oxyacetylene



2. The ability to know feedline pressure, and to be able to accurately adjust the value, is critical to successful gas welding.

can be an excellent welding method. The fusion of the parent materials is quick and very controllable, allowing very high quality welds. However, when we need to weld greater thicknesses, getting all that material around the weld pool up to appropriate temperatures takes bigger jets, used at higher pressures, so it all becomes much slower, and it takes much more of those expensive gases. With the arc methods, on the other hand, on material above a certain thickness, the required rate of energy input is relatively insensitive to thickness. For thicker material arc methods are better.

And what about brazing?

What can one say? Superb, for starters. You can rocket up to temperature, with a controllable flame containing a spectrum of temperatures that protects from oxidation. It is particularly in brazing jobs that the range of flame types and sizes really comes into its own. For a teensy job, you could choose to utilise a cool, remote part of the outer flame. On bigger jobs there is the opportunity to choose bigger or special tips, and the heating can be made continuous or intermittent to suit your purpose. You will certainly not



3. Absolutely, totally necessary. Flashback arrestors in each supply line.

CH MORE THAN WELDING







4. A small, light torch is exactly right for welding sensible metal thickness, and for any brazing.

5. The torch is made up of valves, mixer unit, and tip.

struggle to raise the workpiece to the brazing temperature. You thus avoid the pitfalls of not quite reaching the proper temperature, or worse, when you do, having oxidised the job giving major nonwetting problems.

Rusted solid

Persons habitually working on vehicular antiquities (mine is C-reg!) know that the decision whether to even tackle a job will

6. One welding tip screws in to replace another.

rest on their pre-assessment of the rust-jacking problems that will be encountered. (Laboratory trials have shown that the rust bonding forces can be far higher than the strength of the metal parts). Fortunately, with an oxyacetylene capability, a serious rust jacking problem can usually solved in a matter of seconds. Just occasionally there will not be enough access to apply the flame, and there may be destruction of rubber bushes etc. – a small price to pay for an easy solution to an otherwise intractable problem.

Making the most of what we've got

Moving on, we may consider the next valuable asset of an oxyacetylene capability, that being the ability to rapidly and cleanly heat parts of components. You can for instance turn an ordinary spanner into a special (Fig 12) in a matter of seconds, without losing the temper of the jaws of the spanner. Similarly, with a bench vice, you can effortlessly put sharp bends in substantial bar, and with an anvil and hammers, you can locally heat strip, bar etc. and then forge it into almost any shape, sometimes making items that could

not be produced in any other way. Panel beating enthusiasts will be familiar with the problem that deformation of steel makes the material work harden and become highly elastic. After a time, you can make no further progress towards the repaired condition, until you do a local heating job with the oxyacetylene torch, up to a bright cherry red being sufficient. The heating takes only a few seconds, but the change to the material properties is truly miraculous. That which was highly elastic, and unworkable, becomes totally plastic. The lightest of hammer blows then causes permanent deformation, allowing you to proceed, quickly and easily, to a most satisfactory completion.

Will it work in a field?

With several metres of hose, you do not need, in the typical workshop, to move things about much. On a suitable trolley, or pick-up truck, the oxyacetylene set is easily moved about the workshop, or further afield. Note that cylinders should be kept upright.

Best for big jobs or small jobs?

One of the beauties of a typical oxyacetylene capability is that you can tackle astonishingly small and delicate jobs, then proceed right through the spectrum of tip sizes and flow rates up to what you might reasonably rate as "industrial". Typically, a torch will have a range of sizes of welding "tip". (It is worth mentioning, in passing, that the simplest of welding tips can be much more sophisticated than they look. If you use a straight bored tip you will get a short, fat flame. If you use a tip with an internal taper (narrowing towards the outlet), you will get a long, narrow, precise flame).

A cut above the rest ...

An oxycutting torch is an extremely





8. A small difference in appearance, a big difference in performance. The oxycutting jets.

valuable accessory on suitable welding sets. Typically it fits in place of the welding torch. The oxycutting torch frequently has a range of nozzles, sometimes including a special one for gouging.

Minimising the costs of possessing the oxyacetylene capability Getting equipped

To make a start you will need cylinders, regulators, hoses, flash back arrestors, and a welding (Figs 1 - 6) and perhaps cutting torch, (Figs 7& 8). Cylinders will usually be hired from one of the big two, BOC or Air Products. The remaining equipment will be purchased from your local or mail order welding supplier. Long hoses will allow you to chain your cylinders to a wall, short may be used with a cart. When choosing regulators (Fig 2) you may be offered one or two stage units. The former are cheaper but the latter give more precise and consistent pressure control, which in turn leads to better welds.

Flash back arrestors (**Fig 3**) are a non negotiable part of the kit. These must be permanently installed in each line and are one way of avoiding catastrophic explosive events.

Many texts suggest you should make your own welding cart as a first forming/brazing/ welding exercise. A fault with some commercial carts is that they will not quite pass through a domestic door, so a self-built item may indeed be a good idea. An added storage box will help avoid losing jets etc (Fig 9)

It is worth remembering that lightweight torches, besides tending to be least expensive, are the least tiring to use, and thus lead to the best performance from the operative. Also, it is the very small jobs that are difficult, and the small set will be the best choice of equipment for those jobs. If you are in any doubt, it is best to choose a small gas set and supplement it with an inexpensive arc welder.

As to ancillaries: buy bridged goggles with flip-up shades (Fig 10). They only cost about a fiver, they are fine over spectacles, and you do not get in the right old tangle that is so characteristic of the separate-lens models. Buy yourself some firebricks so that you can easily assemble working surfaces and hearths.

Cylinder size and rental deals are another area for decision making. Arguably, for the dedicated hobbyist, an oxygen bottle of the "half commercial" size must be about right, with the acetylene being somewhat smaller. (The cost of hiring cylinders of gas is more reasonable than it appears to a first glance, because of the statutory requirement for periodic proof testing. If you own the bottles you face that expense and the inconvenience of such testing. If you merely hire them, you are not subject to any inconvenience, and the cost is part of the hire charge).

Some gas welding sets on offer include the cutting capability, others do not. Since possession of the cutting capability is a must, take the trouble to learn to recognise the different tips, torches etc., before you go shopping. Observe that the most expensive sets often do not offer the widest capability, and can hardly therefore offer best value for money. The case for the expensive sets being of higher quality may well be true, but is by no means proven.

Hazards in using an oxyacetylene welding/brazing apparatus

The most obvious hazard comes from that devilish flame, a flame that is in a class of its own for the melting or incineration of anything that gets in its way. Fairly obviously we can have spectacular fires and explosions if that flame is allowed to be incident on almost anything other than the workpiece. In particular, you are unlikely to survive if the flame is allowed to play long on either of the bottles. You should always light up with a spark igniter, never with a naked flame of any kind, since if you happen to be oxygen-rich at the time, your source of ignition can turn into a spectacular and unpredictable firework. Always avoid ingesting any welding fumes, and remember that

simple masks can offer little, if any, protection, since they will not filter fumes. The noxious effects of such fumes are nasty and cumulative. In particular, those from zinc, cadmium and lead are known to cause serious nerve damage. (If you are working with galvanised material, life is much safer and easier if you locally remove the zinc with an acid, e.g. hydrochloric. Just brush it on and wash it off. You can rest assured that you are most unlikely to then be troubled with hydrogen embrittlement, as steels that have been galvanised are usually too soft to be susceptible to such embrittlement). Beware that some light alloy castings (e.g. carburettors and the like) may be plated with cadmium. As to the danger from lead fumes, while there is wide awareness that petrol tanks can only be repaired after rigorous procedures to prevent the risk of explosion, it is perhaps less well known that many petrol tanks are made of a material "terne plate", which is essentially steel with a lead coating. Always make sure that there is plenty of ventilation, either natural or machine induced, when you are welding with gas or by any other method.

Do not attempt to do any DIY mods to your gas supply systems, either acetylene or oxygen, as they are both unforgiving. Leave well alone and follow the instructions of the supplier to the letter. The total of risks is more subtle than we can imagine. It is for instance reported that acetylene can form explosive compounds with copper or copper-rich alloys. (What might you have made your DIY pipe work out of?) This "Safety First, leave it well alone" principle is the reason why acetylene generators, calcium carbide etc. are not mentioned in this article.

Watching where that flame goes is very necessary when using an oxyfuel torch. Parts of the flame can be reflected from or follow the work surfaces and go off in directions entirely different from those intended or anticipated. You can so easily incinerate nearby plastics or electrical wiring, perhaps leaving yourself with a BIG repair problem.





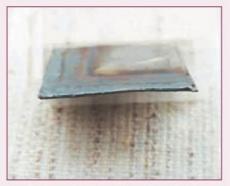
10. Super value for less than a fiver. Flipup goggles that fit over your spectacles and cannot tangle.

Lighting up time

Before starting, read the directions supplied with the kit, and assemble the regulators, flashback arrestors, hoses, and torch. Note the acetylene hose is coloured red, and its fittings have left hand threads. Set the regulators to deliver around 2 – 3 psi.

There are all sorts of ways to do the actual "lighting up". One popular way is to light with the acetylene torch valve turned on half a turn or so, and the oxygen off. Crack on a little oxygen and then get long white acetylene rich flame, (Fig 13) which is a good starting point for further adjustments. You will be aware that you could rapidly fill the room with smuts if you loiter at those settings, so you crack on a touch more oxygen, and while so doing, keep close watch on the changing flame. Any smutting will cease, and as you continue to increase the oxygen feed you will see that the long white flame becomes much diminished, (Fig 14) being replaced by a long, transparent, bluish-tinged flame. Such of the white flame as remains has meantime shrunk back to become a relatively teensy cone (hard edged, opaque, and by now intensely white) at the torch tip exit hole, with perhaps just occasional hints of a feathery whiteness extending a short way into the blue flame. You now are very near the wished-for and oft-used neutral condition. It will be explained later that the hottest part of the flame is just ahead of the white cone. Just a little less acetylene, or a little more oxygen, and you are there. Continue to fine tune the flame by variously increasing and decreasing the acetylene and the oxygen, continuing to examine the flame(s) critically and in detail all the while. At times when the acetylene is being turned up, you will observe that the edges of the intense white cone tend to revert to being feathery and less distinct, and the overall flame is bigger than at other times. You have then re-entered the carburising, reducing condition. Now observe what happens if you decrease the acetylene and/or increase the oxygen. After going through the neutral condition, the intense white cone shrinks and takes on hard edges, while at the same time the length of the overall (blue, transparent) flame shrinks to about half of what it was previously. The burning is noticeably noisier than previously. You then have reentered the distinctly oxidising condition. (Figs 15 & 16).

As said, for most of your jobs you will



11. Fusion where you want it and only where you want it. Trial welds along the edges of two very thin sheets.

want to use the neutral condition, which is the half way house between the reducing and oxidising conditions. It is best to approach from the acetylene rich condition, because the transition to neutral is sharp and obvious.

But here is a minor problem...

Having set up the flame correctly, it would be reasonable to hope that you could then press ahead with your welding or brazing without needing to make any more adjustments. Unfortunately, a number of factors come into play which alter the flame characteristic, and so you have to regularly readjust to the preferred condition. On the positive side, you will after the first few occasions make the readjustments without conscious effort or perhaps even realising that you have made them.

Easy exercises to develop your welding skills

Having correctly set up the flame, we can now proceed to a simple trio of welding tasks that will prepare you for almost anything that comes your way. For these exercises you will need some bits of straight sided steel strip, of thickness, say 2 or 3 mm, or thereabouts. Having lit the torch and adjusted to the neutral flame, play that hottest part of the flame on the middle of one of the flat surfaces of the steel. In a matter of seconds, you will see the local surface melt. (the liquid surface looks rather like dirty mercury). Now move the tip side to side slightly, or round and round in little circles, whichever you find easier, thus making the puddle just a little bit bigger. Now, move the puddle slowly along the plate, seeking to keep the puddle width as consistent as possible. Not too difficult, you will agree. Look at the back of the plate, and form an opinion of the degree to which the fusion has reached that far side.

Now put two pieces of the steel side by side, forming a butting edge. Run a puddle along that butting edge, perhaps prodding with a piece of filler wire to encourage the molten corners to merge into one pool. Deliberately seek poor penetration, by keeping that combined pool as small as possible, by making a quicker traverse and



12. Tools can be modified in a trice to reach into those near-impossible locations. (This one was for the nuts joining the carb to the manifold on a 20 VII)

with less transverse movement. When the workpiece has cooled, observe how easily such a one-sided, poor-penetration joint can be destroyed, perhaps even just by the strength in your fingers. Now make another identical butt joint, but this time seek better penetration, by making it more slowly, and making a wider pool. Then, turn the plate over and run another puddle down the join line. Now try to destroy that sample. You will probably find that your two sided weld is as strong or stronger than the parent material. Having made those simple welds in light material, you will be well on the way to competence for any thin-wall job that you are likely to tackle.

What about the thicker stuff?

Things would get much more difficult if we sought to gas weld thicker material, thicker than say 4 mm. Beyond that you will be far better served by connecting up to, say, an MMA or a MIG welder.

And the really thin stuff?

When butt welding really thin material, examine the benefit of putting a teensy 90°, turn-up on each butting edge, as in Sk1. At the same time notice how you can make a far better job of making those turnups (then getting better butting contact of the up-turned edges, and less distortion of the sheets) if you put a little saw cut every few inches, along the edge that you intend to turn up, extending the cut into the sheet just a smidgeon past the line of intended bending, rather like Sk 2. Note that you use a saw to make the cuts, not snips or shears. If you use anything that does not remove a bit of the line of bending, you do not materially improve matters. Flat thin sheet trial welds are shown in Fig 11.

Filler technique for steels

Having used the filler wire for that first time (if only to encourage the merger of two pools into one), you will have started to appreciate the several values of the filler. Continue to develop that left hand skill. When you choose to add filler, feed it



13. The starting point for fine adjustments to the flame. A long white cone of excess acetylene.

into the pool, rather than melting droplets off the end of the rod. Observe that the oft-desired pooling is usually achieved just by judicious prods at the junction of pools. There sometimes is benefit in warming the wire, sometimes not. Sometimes there is benefit in making significant volume additions, sometimes not. (The filler material for general jobs comes in the form of mild steel rods, usually copper coated, usually 36 inches long, usually 1.6, 2.4 or 3.2 mm diameter).

Some things are easy, some things are not

When gas welding, some problems may well be obvious before you ever start welding. For instance, for the fillets in a classic T weld, one piece of metal has twice the heat sink of the other. So don't direct the flame into the corner. Bias the flame so that there is greater incidence on the material with the double heat sink.

Because you are working with a flame, welding of protruding material is generally easy. The converse is equally true. Welding at sunken locations is generally difficult, because you so easily get excess heat where you do not want it, and a shortage of heat where you do. So, in those latter situations, beware poor fusion and poor penetration, and beware unwanted fusion at locations adjacent to the weld pool. Always remember where the flame hot spot is: just ahead of that intense white cone. For more heat, move that hot spot nearer to coincidence with the metal surface, or dwell for longer times. For less heat, increase that distance, or reduce the incidence time by diverting the flame. (The downside of the diversion method is that you also divert the protective atmosphere).

If things look as though they are going to overheat or you see the early signs of melt through, it can be found quicker to rotate the torch than lift it. Try to keep about 1/2 inch (3 mm) between the workpiece and the end of the intense white cone. For most jobs, this keeps the weld pool dimensions right. At a particular torch setting, on the particular workpiece, your primary control is via travel speed. By control of the weld pool dimension you control the penetration through the thickness. Some welds are made without filler, apart from a preliminary dab to bring two pools into one. With other welds there is frequent addition of filler, usually to bring the level of the weld pool up to the general level of the two surfaces. You will



14. The transition between carburising and neutral conditions. An occasional and transient hint of excess acetylene seen beyond the intense white cone.

find that it is easier to weave the flame than to keep it in an exact straight line. At the start or end of a weld you are heating less material, so at those locations, reduce the heat input, either via torch proximity or torch residence time. In oxyacetylene welding, in material thicknesses that make sense, vee prepping etc. is done to allow the heat transfer that will lead to full penetration. (Unlike the prepping for the arc techniques, where part of the purpose is to provide unimpeded access for the electrodes).

As in all welding, life is made much easier if you use the range of clamps and magnetic formers that are cheap and readily available. If the parent material has high thermal conductivity, and is of a shape that provides a good heat sink, you will almost certainly need to preheat, other situations may require slow cooling.

Identification of the parent materials as the basis for selection of fillers and fluxes

All weld jobs depend crucially on getting the right filler. Easy for mild steel jobs, but less so for more out of the way alloy compositions. Often, strips of the base material will provide good filler material. With mild and low alloy steels, the familiar copper-coated filler rods are usually quite sufficient. For any piece of parent material more sophisticated than a piece of mild steel, the less you know about the exact identity of your parent material, the less likely you must be to be using the correct filler rods, and the more likely you must be to make a hash of the job. There are many roads to ruination, for instance cracking, or inability to make a weld, or local loss of corrosion resistance. The message is: for anything over and above mild steel, you have to do your homework, before you can be reasonably confident of success.

To flux or not to flux, that is the question

One aspect of gas welding/brazing practice that can be a little confusing is: when are fluxes used, and when are they not used? That confusion is compounded by some occasional lack of clarity about whether a material is being welded or



15. Early stage of moving from neutral to oxidising conditions. The intense white cone is hard-edged.

brazed. (There is for instance the process of "braze welding", that has some distinct differences from both brazing (by not making much use of capillary flow) and from welding (by not melting the parent materials). A sensible policy is to simply follow the advice given in respected texts, and if a particular filler and/or flux is suggested, give it a try. A flux may be in the form of a powder or a paste or a coating on the rod, the latter often becoming very friable if you store your brazing rods in a damp workshop. A flux in gas welding/brazing serves variously to remove oxide, or prevent oxidation, both vital if you are to get good pooling/ wetting.

Cleanliness is next to Godliness

A lot of materials require special cleaning before welding, and a lot of jobs benefit from a furbishing after welding. For general purposes on mild steel etc., a twisted wire brush on a 115 mm angle grinder takes some beating. (But not on stainless please. It will subsequently develop rust stains! Buy a special brush with stainless wires). If you do a lot of jobs, you will soon break even on the cost of an angle grinder dedicated to that wire brush, by saving the time spent changing discs for brushes, and back again. Remember particularly with such brushes: look after your eyes! Cleaning up after welding is particularly important if you have been using an aggressive flux (e.g. on aluminium) otherwise it will continue to be aggressive, and large holes will appear in your workpiece!

Brazing and the oxyfuel torch... a marriage made in

heaven

An oxyacetylene unit is near perfect for all soldering and brazing. (As indeed are almost all oxyfuel systems, and the others may be better and cheaper. Oxyacetylene only retains the crown because of the other things that it does so well). If you braze or solder, you must do so with appropriate design at the contact points, which usually means making lap joints



16. Distinctly oxidising. The intense white cone is now very small and the secondary blue flame has shortened to about two-thirds of its previous length. A far noisier flame than previously.

instead of butt joints, the lap size being at least three times the thickness of the thinnest sheet. For capillary flow you need a gap at the joints, the ideal value being in the range .001 to .005 inches, dependant on the parent metals and the fillers. If you have to make a butt joint when soldering or brazing, try to use guile to ensure that there are other, lapping surfaces, if the design and circumstances allow. For example: a backing plate when brazing plates that have to butt or a liner tube when brazing tubes that have to butt (Sk 3).

Brazing is very handy when you want to join thick stuff to thin stuff. (because if you weld you might burn through the thin stuff), for delicate items (Fig 17), and for when the joint location is hidden from easy access or contact. (You don't have to see the capillary flow to know that it has happened, if you have set things up properly beforehand). You can braze many dissimilar metal combinations, combinations that you cannot weld because of the possibility of creating some god-awful alloy. Brazing is used to join some special steels, chosen as the only way to do so without significant loss of the strength of those parent metals.

A few cutting remarks

The start procedure for cutting is that an oxyacetylene (or other oxyfuel) mixture, fed by about 4 or 6 small nozzles, heats some part of the start region to incandescence The internal design of the cutting torch (Fig 7) is such that some of the oxygen is diverted to mix with the combustible gas, while the rest of the oxygen is available to provide the cutting jet, on demand, as a collimated stream. Jets are shown in Fig 8. The supply requirements for each gas are as you might expect, not a lot of fuel gas pressure (say 1 or 2 p.s.i) for acetylene, and a much

higher pressure (say 15 p.s.i) of oxygen, the higher oxygen pressure being necessary to feed the cutting stream. The feed of cutting oxygen is usually lever actuated on manual systems. The size of the cutting tip is increased with the thickness of metal to be cut. Maintenance of tip hole diameter and bore smoothness is absolutely vital, otherwise the flow characteristics may be changed, resulting in ragged cutting and reduction of thickness capability. The cutting attachments can be uniquely useful, for instance allowing easy cutting of far thicker material than is possible with most plasma cutters.

Destruction and distress

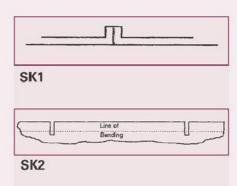
When using an oxyfuel cutter, one working instruction deserves carving on tablets of stone. Be very, very careful where the sparks and debris are going. The fire risk is obvious, but that is only one part of it. Even at a distance of several feet, the stream of debris particles will cut through many insulation, and blanket materials, and having done so, will then proceed to devastate anything else that then stands in its way.

Cutting to a pattern

As might be imagined, it is fairly easy to move from freehand manual cutting to various forms of guidance and automation. The opportunities are legion. so we can't go into them in this article. One thing introduces a slight complication into guidance by running the nozzle along simple straight edges and templates, and that is the need to make allowance for the offset distance between the side of the oxygen stream and the side of the cutting nozzle. An advantage of the oxyfuel cutting nozzle not being held in contact with the surface of the workpiece is that there are not the same slip-stick problems that can so detract from accurate and easy plasma cutting.

Keep in mind that...

There must always be a risk of fire with any oxyfuel operation. Always have several fire-fighting capabilities ready, immediately to hand, e.g. a couple of detergent bottles filled with water (to use first), a couple of powder extinguisher canisters (in case one is empty), and a garden hose (to really cool the situation). Many insurers (of house and contents) seem happy with oxygen and acetylene gas cylinders being held on domestic



premises provided you are only acting in a non commercial manner, but you must check with your own insurers. Remember that acetylene bottles should not be used in a horizontal position or if they have recently been in a horizontal position. (If you have to go and work in a field somewhere, transport the acetylene in a vertical position. The reason harks back to acetylene being a quirky gas that can, if over about 30 p.s.i, explode without necessity for oxygen or air to be present. So, the acetylene is supplied dissolved in acetone, which itself has been absorbed in a porous material. So, if you lay the bottle on its side you can get acetone coming out with your gas ...)

Ensure that the bottles cannot fall over. (After breakage at the neck, bottles have been known, as projectiles, to travel hundreds of yards and to go right through buildings).

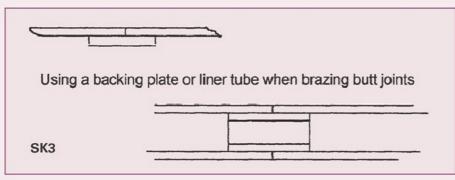
So the conclusion at the end of the day is?

You can now, in a leisurely fashion prepare to agonise over the decision whether to purchase or not to purchase. An angel will sit on one of your shoulders, loudly urging the restraints that "You don't *really* need it ... awfully expensive ... better to save the money...". On the other shoulder a little red devil will whisper the seductions "Go on ... treat yourself ... think how useful it would be ... think of the pleasure ... now is the time ... there aren't any pockets in a shroud ...".

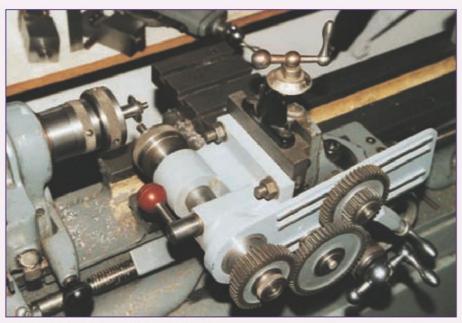
Since I am totally impartial, I cannot offer advice either way, except of course to point out the obvious: that the angel must have a quite miserable, stagnant existence, while the little red devil must have a lot of fun in a world where all is change and all change is for the better! Have fun, but remember, watch those sparks!



17. Prior to being re-cut, one broken key and one worn out key have been rescued by a teensy bit of silver braze. No need now to buy and fit new locks!



DIVIDING ON THE SUPER SEVEN (2)



1. The Sparey device, banjo clearly visible.

s I mentioned in my last article, my initial forays into the mysteries of dividing were confined to the most crude methods but, at this stage of my model engineering, it mattered little since I was only concerned with relatively simple jobs. I had already gathered that there were apparently two main approaches to indexed milling in the lathe, the first being by the method of driving the cutter from the lathe mandrel whilst holding and indexing the work by some means on the cross or top slide. The second was by adopting the technique, pioneered by the horological world, of using an auxiliary means of driving a cutter spindle whilst employing some method of indexing the

lathe mandrel. Since my mentor at the time was Lawrence Sparey with his new book 'The Amateurs Lathe', the chapter (including plans) on his own particular version of a dividing device persuaded me that this was the direction to take, and I determined to make one in spite of my lack of experience.

Alas, what do they say about fools rushing in? In spite of my pattern making being successful, the moulding and casting of the aluminium body proved a complete disaster. In the first place I had no moulding sand at my disposal, so I improvised with fine builders sand, using the same material in its driest form for parting powder. Unfortunately I knew practically nothing about the techniques of moulding so that, in

Having earlier dealt with simpler headstock methods, John Brittain now considers other further variations on the theme.

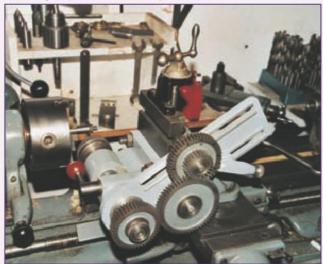
spite of managing to produce an actual mould, all the resultant castings (and there must have been at least six attempts) were deficient in some aspect -usually a large sinkage being the culprit, as I recall. My 'furnace', by the way, was an old iron saucepan set up on an open coke fire which, in itself was fairly satisfactory, but having no knowledge of such details as venting the mould and de-gassing the molten metal, the likelihood of success operating under these conditions was, in retrospect, rather slender. Nevertheless, In spite of these initial setbacks, I conjured up the impudence to have a go at the banjo piece and, wonder of wonders, it emerged from the sand in a nigh-perfect state. (To this day I can never understand why!) However, in spite of my machining this component successfully, I found that the momentum had been lost and I shelved the project in favour of other ideas. Years later, during which time I had acquired the necessary know-how for moulding and casting, I finally finished constructing the device, more as an entertaining project than a much-needed one, since by then I possessed a milling machine anyway.

The Sparey dividing device

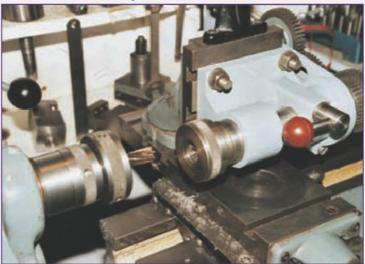
For those unfamiliar with the late Mr. Sparey's dividing device, a word of explanation: it consists of a main casting

2. The Sparey device located by two bolts.

36

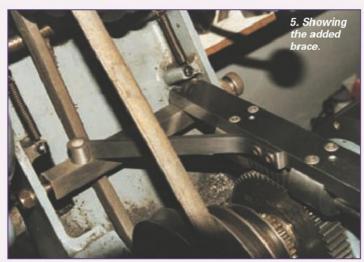


3. The same unit here set parallel to the lathe bed.



Model Engineers' Workshop





carrying a mandrel. On the rear end of the casting is attached a 'banjo' piece. This banjo carries a train of changewheels which can be arranged to gear the mandrel up or down whilst being indexed by a plunger detent. (see photo 1) Thus, for example, a 35 tooth wheel located directly on the end of the mandrel and indexed every 5th tooth would obviously give 7 divisions of the headstock, if geared down 2 to 1,14 divisions and if geared down 3 to 1, 21 divisions etc. By using this method and utilising the complete range of lathe changewheels, it is possible to obtain a very large number of divisions but with one important proviso; the gear on the end of the spindle must contain a submultiple (always the prime number if one is involved) of the required division number - in the above case this number being 7. The mandrel nose is screwed to accept a Myford chuck and bored to accept collets of Mr. Sparey's design.)

In practice, I have found the device to be of a most workmanlike and sturdy design, but with certain limitations. With the vertical slide in the its lowest possible position and with the device fixed centrally on it; the difference between its centre height and the lathe's is only about one inch, thus severely restricting the size of work which can be accommodated. The illustration in Mr. Sparey's book showing it

in use indicates that he has fixed it by utilising the centre tee slot of the vertical slide, which means that the device is being held by using its two upper bolt-holes only (see photo 2). This, of course makes for a less-than-perfect situation though, in fairness, the resulting setup is reasonably rigid. Furthermore, the cross-slide needs to be retracted rather a long way in order for the work to be positioned beneath the cutter - unless, of course, one chooses to use the cross-slide tee-slot at the extreme end nearest the handle, in which case the reverse applies and the cross-slide needs to be wound forward for nearly all of its travel. . (Forgive the three jaw appearance in the photo but the situation is simulated to illustrate this problem of working space. Where possible, I favour mounting the cutter on a stout mandrel held in the fourjaw chuck for maximum rigidity).

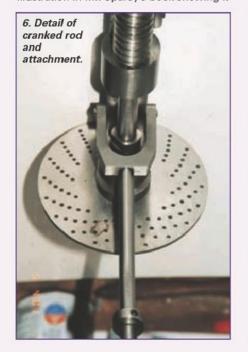
When the device is located with its axis parallel with the lathe bed, (see photo 3) it seemingly presents a better set-up, but unfortunately there are few machining applications which suggest themselves when in this position. Notwithstanding the above remarks, the device works well when diameters are not too large and is especially useful when the milling of steel components such as clock pinions is attempted. Ironically enough I have found it to be an excellent tool when used on my

milling machine, where the extra space available enables it to become a most useful appliance.

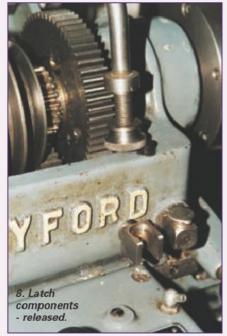
Were I to contemplate re-making this device, I think I would re-design the main casting by offsetting the cylindrical mandrel housing in relation to the base in order to gain more working height whilst, at the same time, being able to fix it centrally to the vertical slide. I feel also that the whole thing could be shortened by up to one inch so that the cross-slide would not require retracting so far. I doubt whether I shall ever do this but some intrepid enthusiast may like to try it and reveal any advantages (or otherwise) which may ensue.

The Radford approach

Meantime, to return to the ongoing saga, as the years went by my dividing requirements gradually became more demanding and I realised that it would be desirable to make the other type of device mentioned earlier - i.e. one which indexed the lathe mandrel. During my student days at Loughborough Training College, I had completed a wall clock case and intended at some time to design and make the works for it. Therefore in 1968 when the late Mr. J. Radford's indexing attachment appeared in the 'Model Engineer' I

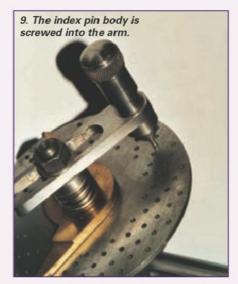






guessed that this would suit my requirements admirably. - and what a truly elegant design it proved to be. As I write this I have the very magazine in which it featured in front of me and note that is dated January, 1968, volume 134 number 3336. Again, for the benefit of those who can obtain the plans and might be interested in making it, I offer a brief description:

The device is designed specifically for the Super 7 and consists of a main arm carrying a shaft, part of which is screwcut to engage with the 60 tooth bullwheel, (see photo 4). The arm is arranged to be supported at one end by a cross member located between the sides of the belt guard, and by a cranked rod at the other. This last is held in position by an adjustable nut engaging with a fixture attached to the front of the headstock casting. The upper end of the shaft carries

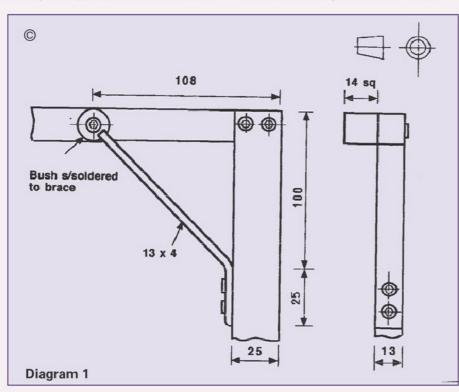


a division plate, detent and fingers and the whole thing operates in much the same manner as the usual form of dividing device used on milling machines.

One of the most impressive characteristics of the tool is the ease and speed with which it can be fitted and removed from the lathe, a few seconds being all that is required. Of course, the principle of applying this type of dividing device for use on lathes is not new but this particular design represents an extremely neat solution to the problem, albeit for a particular machine. Those, by the way, whose machines are not suited to this form of device could do worse than consult Ian Bradley's book 'The Amateur's Workshop', where they will find a design of similar principle which can be applied to most lathes.

Modifications

Mr. Radford's design as it stands is perfectly sound but, like most of us, I like to make alterations if I think I can see any benefit from doing so, and in this case I

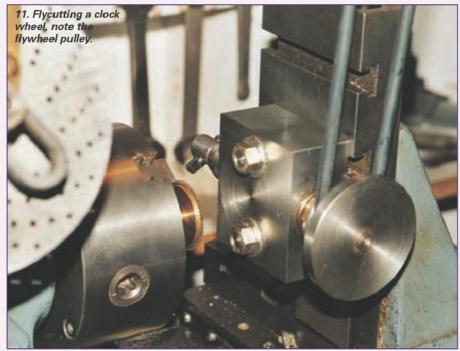




felt that I could modify it to suit my particular eccentricities without compromising its efficiency. Since I hate applying heat to any job where it can possibly be avoided, my first thought was to join the supporting cross-member to the arm by means other than brazing. Accordingly, I began by drilling the end of the arm to receive two cap screws (see Diagram 1) and fastened it to the cross member by one of them. Placing the components in position on the lathe I then adjusted them until the threaded portion of the shaft engaged correctly with the bullwheel before tightening the cap screw. I then removed the assembly from the lathe, spotted the second cap screw position, took the two pieces apart and tapped the second hole. When these components were re-assembled, I set about fitting a diagonal brace to the two pieces in order to ensure complete rigidity. Incidentally, I feel also that the aesthetic aspect of the tool is improved by the addition of this brace(see photo 5).

I have always thought that both the 'U' shaped bracket and its cranked rod (swinging latch) were a little on the light side so I increased the rod to % diameter and re-styled the bracket as in photo. The original design allows for quick disassembly of the two main components but since I never intended to take them apart anyway I opted for a hinge pin passing through bracket and arm as shown in diagram 2. This pin can be tapped out any time I change my mind and decide to take the thing apart, but meantime, when not in use, the assembled device sits on a shelf above the lathe ready for instant action!

I suppose my main departure from the original is found in the 'latch' design, where I considered that the various components used to anchor the cranked rod to the headstock casting somewhat fussier than necessary. Accordingly I redesigned them as shown in diagrams 2 and 3 (photos 6,7 and 8) and can assure anyone who may contemplate making the appliance that the alteration works perfectly well and, in my view, represents



far less trouble to produce.

A further minor alteration concerns the indexing components where, rather than braze the index pin body to its arm, I formed a semicircular end to the arm, drilled, bored and screwcut it and screwcut the body to suit (see photo 9) - again avoiding brazing and the need for cleaning up!

Very probably, the item which could cause the biggest headache for some is the approach needed to cut the 16 D.P. worm on the shaft. For those therefore who need a little guidance on this, I will explain:

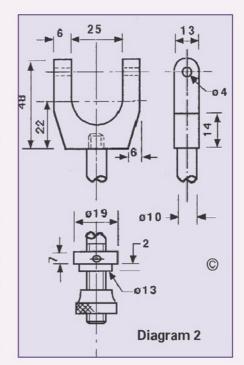
D.P. stands for Diametral Pitch and refers to the number of teeth on a gear per inch of diameter. In this particular case, we need to cut a 16 D.P. worm matching the teeth of a gear which, if of one inch diameter would have sixteen teeth. Now if we imagine that the diameter of this gear is divided into sixteen parts, then it follows that the distance between each tooth (i.e. centre to centre or 'pitch') will be times one sixteenth of an inch. We need therefore to introduce in our gear train once we have imagined setting up for 16 t.p.i. and the way of doing this is as follows:

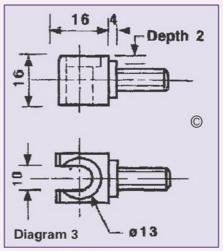
22/7 can be represented by 220 and 70 tooth gears except that we don't have a 220 changewheel - or, for that matter, a 110 wheel! If, however, we first cancel

down to 110/35 and then we halve the 110, thus obtaining 55/35 and, at the same time set the lathe to cut 8 t.p.i. the end result will be the same i.e. 110/35 x 1/16 gives the same answer as 55/35 x 1/2 Having stated this, I must now confess that I did not carry out the job on my Myford lathe simply because I also own a Harrison L5 and the procedure on this machine needs to be slightly different. In this case a 55 tooth gear is paired with a 70 tooth gear and the lathe set up to cut 4 t.p.i., again, 110/35 x 1/6 works out to be the same as 55/70 x 1/4 (see photo 10) You will, of course, find the actual changewheel set-up in your Myford handbook but without the above explanation!

One point which must be noted; it is imperative that the half-nuts remain engaged during the whole process, so the procedure is to run the lathe backwards after each pass - which, in turn, calls for a reversing switch. It is possible to turn the lathe backwards by hand but the job then becomes a very tedious chore and I would recommend that you take the easier way out and fit that reversing switch if your lathe is without one. Sooner or later It will come in handy when you are faced with the need for cutting one of the less usual threads, and I'd like to bet that it's sooner!

Finally, the last three photos show some of the many uses to which the Radford





device has been put:

Photo 11 shows a clock wheel being formed with a flycutter (Note the flywheel pulley)

Photo 12 shows a straight sided cam being formed using a filing device.

Photo 13 shows the finish- profiling of the cam. Some will no doubt question the use of a drill chuck for milling. It does not offer high rigidity and positive axial location, however for light duties, I find it a satisfactory solution.





TRADE COUNTER

Please note that, unless otherwise stated, Trade Counter items have not necessarily been tested. We give news of products and services which have been brought to our attention and which we consider may be of interest to our readers.

New grease from Enginewise

CP (Corrosion Preventing) Grease is a new product from Enginewise. It contains active corrosion inhibitors which make it uniquely appropriate for a wide range of model and full size applications.

'Standard' greases provide only barrier protection and conventional water repelling greases tend to emulsify. CP Grease does not emulsify and it has other useful characteristics:

 A high melting point (above 200 deg C).

 It is thixotropic – flows easily when shaken/agitated or is subjected to shear forces and gels when such activities cease.

3. It does not contain silicone.

These properties make CP grease particularly suitable for lubricating and protecting cables of all kinds. It is effective at preventing ingress of water based coolants on machine tools and can be used on steam models of all sizes to lubricate and protect valve gear and bearings. Other applications might be found on cars, motor and pedal cycles, boats, light aircraft and horticultural machinery. CP Grease is available in

250gm plastic pots at £9-00 plus p&p.
The company has also announced two further additions to the range. Al-Clean is described as having an acidic dissolving action, very effective in removing

oxidation from aluminium and alloy castings, and components. The

formulation consists of a mix of organic and inorganic acids with a corrosion inhibitor, and may be applied by brush, spray, or dip. Treated surfaces should be flushed off with clean water before the Al-Clean dies, to provide a surface ready for primer or paint.

XMPX is a higher performance version of the established XMP, having a higher solids content, giving a thicker but still clear film.

Possible applications for XMPX might include under bonnet components, plated brightwork and wire wheels on vehicles shipped by sea, and polished steel and cast iron parts on traction engines and steam launches.

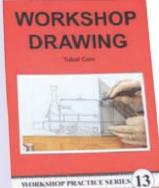
These and many other specialist corrosion control products are available direct from Enginewise, tel: 01472 347 400, www.enginewise.co.uk.

Fireside Reading

Now back in print under the Special Interest Model Books banner, Workshop Drawing by Tubal Cain will be welcomed by beginners to the amateur workshop hobby, and seasoned experts alike. Prior to achieving an enviable reputation as a writer and modelmaker, the author's earlier career included work as an engineering designer, and as a teacher of engineering drawing. This practical "hands on" experience results in a clear and concise book which is very much easier to read and digest than some rather bulkier titles which were aimed at the engineering training market.

The book extends to 114 pages, in eleven sections with two appendices, one of which sets out very clearly the layout of, and differences between, first and third angle projection. The introduction gives a brief history of the use of drawings for communication and recording, noting that the invention of

the blue print process in 1840 then allowed multiple copies of identical drawings to be distributed to a number of workers The following eleven sections then cover: The Rules and 'Grammar' of Drawing: The Conventions of



'Projection'; Hidden Details and Sections; Dimensioning; Conventional Representation; Tolerances; Machining Marks; Making Drawings and Sketches; Reading Drawings; Developments and Intersections; Metric and Imperial Drawings.

Some might try to question, in these days of CAD systems, the relevance of such a work, however, even the very best computerised package is still a GIGO (garbage in – garbage out) system. Without a clear understanding of drawing fundamentals, it is all too easy produce unintelligible graphical nonsense. Tubal Cain provides a short course which will allow the tyro draughtsman to convey design ideas clearly, also to correctly interpret older drawings. It may in addition, refresh the memory of many an older, seasoned practitioner.

Workshop Drawing (ISBN 1-85486-182-4) is published by Special Interest Model Books and may be obtained from all good booksellers or from Highbury Nexus Customer Services 01322 616 300

The right tool for the job

Having found a little spare time I had settled down in the workshop to complete a few more operations on the Bentley BR2 nosepiece. The external features include a tapered section between two flanges with fillet radii. Having taken a few trial cuts with slightly modified part off tools, I had stopped, to await the opportunity to grind up a "proper tool". Later, while thumbing the pages of Model Engineer, I chanced on the Greenwood Tools advert showing their SRDCN button tool. Knowing that a fellow club member had reported excellent results with a part off tool from the same source, I had no qualms about parting with £31-65 including p&p. The tool duly arrived the following day. The carbide tooltip is a 5mm diameter round button which allows you to cut in almost any direction. The round shape also allows the tip to be rotated when the edge wears.



The splined end of the nosepiece which carries the prop. and prop. driver had been completed during earlier sessions, leaving the rear end to be dealt with. It was felt that the internal features would be easier to inspect for size, so these were attended to first, using drills and then boring bar, having set over the top slide to the appropriate angle. The external taper section and corner radii were then formed with the new tool, taking measurements with a ball ended micrometer to check wall thickness. Certainly a little care is needed deep in the acute angle corner since the length of edge cutting then extends around more than 90degrees of the tooltip, and the loading will test most small machines. My technique here was to make repeated approaches from alternate directions into the corner. The finish straight off the tool was found to be quite impressive, with no need to reach for the emery. Readers who have studied the Blackmore drawings for the Bentley will know that a corner radius of 2mm is shown on this part. I think I may be able to live with 2.5mm. Other uses for this type of tool might include operations such as profiling locomotive wheels, and those beautiful but tricky rods typical of Victorian beam engines.

Greenwood can be contacted on 01527 877 576 or www.greenwood-tools.co.uk

40 Model Engineers' Workshop

DRILL GRINDING WITH THE QUORN

Bill Morris outlines ways and means of using the ever popular Quorn tool and cutter grinder for more mundane but perhaps more frequently required drill sharpening.

ext to sharpening lathe tools, the amateur machinist's most pressing need is for some sort of device to sharpen drills. Lathe tools can be sharpened after a fashion offhand, but not so Mr Morse's twist drills except perhaps the larger sizes and at that only after much practice. When I built my Quorn tool and cutter grinder over twenty years ago, I was looking forward to being able to sharpen every cutter type under the sun and was disappointed to find that it would not do what all of us wish to do: sharpen drills; unless one was also the owner of collets, one size for each size of drill. So I carried on making do with a diecast drill grinding jig for larger sizes and accumulating a box of blunt drills in the smaller sizes against the day when someone would publish an article about how to sharpen them in the Quorn. Very small drills of course can be sharpened using a simple honing jig such as the one described by John Wilding in ME numbers 4136 and 4138; and I can vouch for the usefulness of such a jig. Eventually, with my earnings from writing an article in MEW I bought a drill grinding machine from the USA, complete with two multi-size collet chucks. I had better not identify it, as it seems to be a matter of complete luck whether the drill lips end up with positive or negative clearances and it now lies unused in a dark corner of my workshop.

Philip Amos's articles "Compendium of the Quorn" (MEW 62 and 63) were, I am sure, welcomed by all of the many owners of this machine and they contain much useful information, but very little on drill grinding except to refer to I. Strugnell's Model Engineer article of 7 July 1978. This article describes how to attach a "Duplex" drill grinding jig to the Quorn, using the angular settings and the movements of the Quorn itself rather than of the jig. I had a partially completed Duplex jig in a box, abandoned when I could not complete it for want of a complete series of constructional articles, so recently I did a bit of hard thinking to fill in the missing bits. Soon I had a Duplex jig that, set up on my surface grinder, quickly sharpened the box of blunt drills and those that were sharp but with clearance angles going the wrong way. Ian Strugnell's approach seems unnecessarily complicated and in



any case, he built his jig with marriage to the Quorn in mind. Those of us who built the jig to the originally published drawings need a simpler approach to marrying the jig to the Quorn.

Drills larger than 12 mm do not sit happily in the Duplex jig, so I designed and built a jig that will accommodate drills up to 25 mm in diameter. Drills under about 4mm in diameter are hard to hold in any sort of jig that uses vee blocks, so I also adapted an unused 6 mm Jacobs chuck to hold drills between 4 mm and those tiny ones that can be honed with a Wilding-type jig.

Marriage of Duplex to Quorn

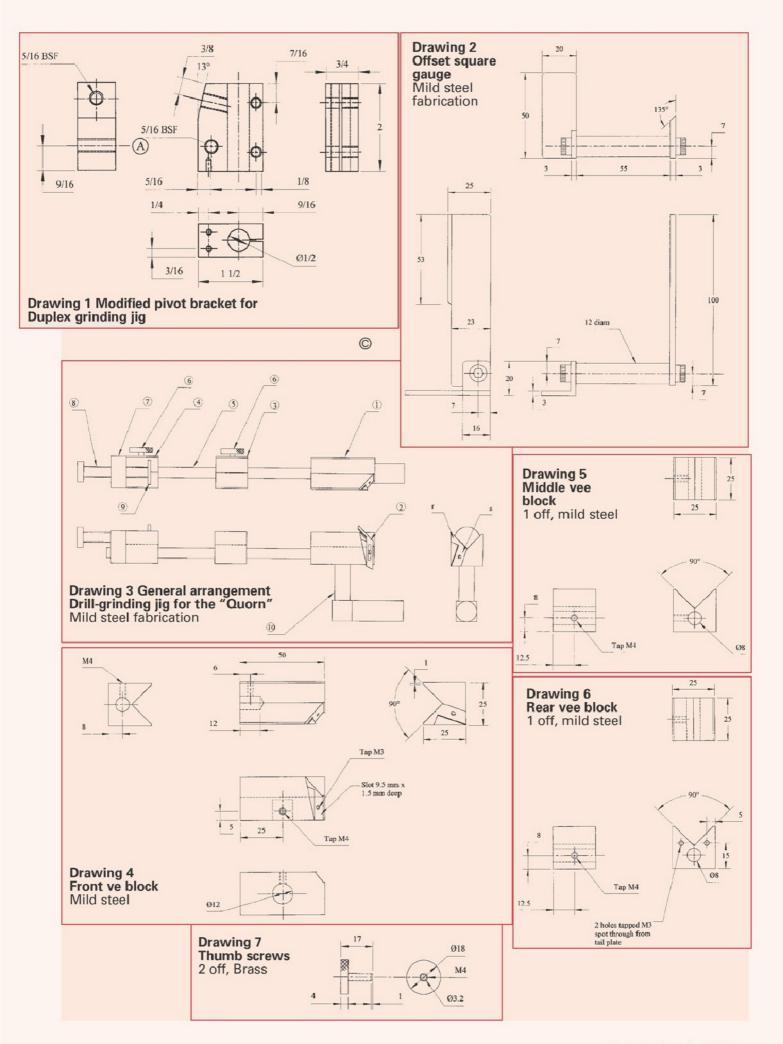
The Duplex jig can be attached simply to the top of the Quorn rotating base by means of a simple peg with either two spanner flats or a tommy bar hole so that it can be tightened securely in the sloping face of the Duplex pivot bracket (Photo 1). Attached this way, the rotating base and the tilting bracket of the Quorn are set to zero and the whole jig brought up to the face of a cup wheel as shown in the photo. This is fine so long as there is plenty of length left in your cup wheel, but as it wears, and for small diameter drills, you run out of Quorn bed to the left. This can be got around by relocating the peg in the back face of the Duplex pivot bracket using the tapped hole shown as "A" in my Drawing 1, and rotating the Quorn rotating base 90 degrees clockwise. Located this way, the Duplex pivot bracket has to be rotated about the peg until the 13 degree inclined face is vertical and then fixed in

this position on the rotating base (**Photo 2**). The inclined face is only about 18 mm long and there is no convenient datum from which to set it vertical. However, the front edge of the by-now-unused stop arm is a useful length and is parallel to the inclined face of the pivot bracket, so all we need is a usable datum to set it at right angles to the top of the Quorn's rotating base

The Quorn rotating base is a substantial casting and it is the work of a few minutes to seat it squarely in a machine vice and mill a datum surface on its top (Photo 3). Then, by using a gauge that, for want of a better term I have called an "offset square" (Drawing 2), the front edge of the stop arm can be set at right angles to the top of the rotating base. If the Quorn tilting bracket is set at zero, the edge of the stop arm will then be parallel to the face of the cup wheel. Photos 4 and 5 show front and rear views of the offset square in use.

Jig for four-facet drill grinding

The Duplex jig is by no means easy to construct (though once constructed it is a pleasure to use) so I set out to design a simple jig that could be used in the Quorn with the minimum of fuss and using basic machining techniques of turning and milling or shaping. This led to a jig that will sharpen drills between about 3 or 4 mm and 25 mm in diameter by the four facet method. To use the late Professor Chaddock's words, "Instead of one continuous conical back-off angle the cutting edge is ground with a primary and secondary clearance angle just like an end



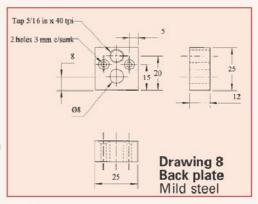


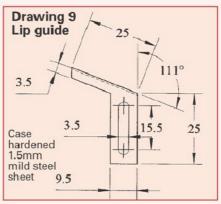
mill in fact. The important difference is, however, that the secondary clearance is taken just so far that the back edge of the primary clearance on both lips of the drill forms an exact straight line across the

diameter of the drill. The result of this is that the chisel point...is itself pointed...which gives the drill its selfstarting and true-running properties." (Photo 6)

I designed the jig in my head as I went along. The drawings came later from the finished item and, lacking the necessary drafting skills to work out how to calculate and draw the complex angles at the nose of the jig, readers should regard the GA drawing (**Drawing 3**) and the front vee block drawing in particular simply as illustrations rather than an accurate guide to construction. For the latter it is necessary to read the text.

A front vee block (1) has on its front a facet produced by rotating the vee 31 degrees in the horizontal plane and 10 degrees in the vertical plane passing through the axis of the vee. The facet passes through the vertex of the vee. A seat (s) is machined in this facet for the lip guide (2) to slide in and there is relief (r) machined to allow the transverse part of the guide to be lowered to accommodate small drills. An intermediate vee block(3) and a tailstock vee block(4) slide along a





round bar bed (5) and are held in position by knurled thumbscrews (6). A backplate (7) is attached to the rear of the tailstock vee by screws and is threaded for an adjusting screw (8) and pressure pad (9), held in place in the screw by means of a helical spring passing through the central hole. The assembly is attached to the rotating base of the Quorn by means of a fabricated support leg (10).

The sharpening process

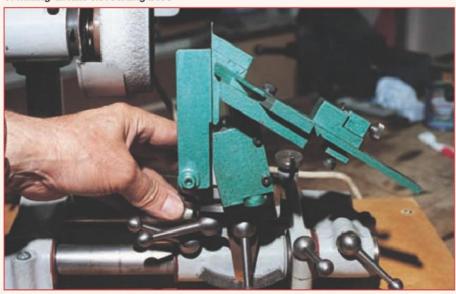
This is perhaps a good point to introduce the actual sharpening process to encourage others to try it, but again to echo Professor Chaddock, "Like most grinding jobs, it is easier to demonstrate than to describe it."

In use, the three vees are aligned by holding the drill firmly in the front vee with the fingers and sliding the other vees along into alignment, locking them in place with the thumb screws. For smaller drills the intermediate vee block can be omitted but for larger drills it is necessary to use it, to ensure that the drill rests on its lands in at least three points or more to prevent rocking (Photo 7). The drill and lip guide are adjusted so that the lip being ground projects a few millimetres beyond the guide while being approximately parallel to the base of the block (Photo 6); and then the tail stock is brought up so that the end of the drill is located by the pad. Advancing the tail stock screw rotates the drill clockwise and so does lowering the lip gauge. You can think of them as being fine and coarse adjustment respectively. Once set, the lip gauge is not disturbed and fine adjustment is made later, during the process of grinding, by means of the adjusting screw.

Although Professor Chaddock and others describe the use of the setting pin



3. Milling datum on rotating base



4. Front view of offset square use



5. Rear view of offset square use





7. Jig accommodates large drills

or other devices to set the lip being ground horizontal, I find that the Mark I Eyeball, combined with adjustments as the drill is being ground, gives satisfactory results.

Set the rotating base of the Quorn at 31 degrees anticlockwise to give the usual point angle of 118 degrees (118 + 31 + 31 = 180) and the tilting bracket at 10 to 12 degrees anticlockwise(i.e. nose down) to give the primary lip clearance angle. Then slide the workhead base along to bring the

drill up to the face of the cup wheel and lock it in place on the front bar. Cut is put on by the Quorn micrometer screw. The drill is held in the front vee with the fingers applying a gentle pressure to keep the end of the drill against the tailstock pad and the lip located against the gauge (Photo 8). The workhead base and front bar are then rotated so the drill passes across the wheel and the first facet is ground. It is quite easy to see as it is being ground whether the rear edge of

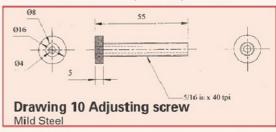
the facet is parallel to the cutting lip and, if it is not, to make minor adjustments by means of the tail stock screw. Once the rear edge of the facet has passed beyond the centre point of the chisel edge, swing the jig clear of the wheel, set the micrometer thimble to zero, rotate the drill through 180 degrees, relocate it in the jig and grind the primary angle on the other lip until the micrometer again reads zero.

The tilting bracket is then reset for the secondary clearance angle of 20 to 25 degrees (Photo 9) and the secondary facets ground until their front edges reach the centre of the chisel edge. The junctions between the primary and secondary clearance facets should then form a straight line as shown in Photo 6. This is the procedure for regrinding a drill that has been ground conventionally, but to sharpen a drill that already has four facets, it is usually quicker to touch up the secondary facets first and then the primary facets need no more than a few kisses from the wheel to produce the straight line across the chisel edge.

Construction

The vee blocks (parts 1, 3 and 4) and thumb screws(parts 6)

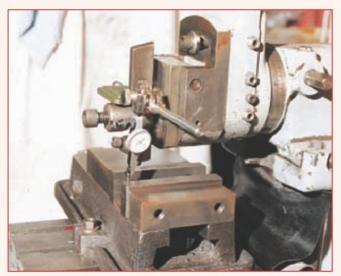
As I have a shaping machine, I found it easiest to make the vees as one piece and cut them up afterwards into three, but those dependent on a vertical slide may have to make the vees in two hits. Start by squaring the ends of a piece of 25 mm square cold rolled mild steel bar and then mark out and lightly emphasise the lines with a fine prick punch. In the shaping machine, the next task is to set the fixed jaw of the machine vice parallel to the movement of the ram (Photo 10). The work







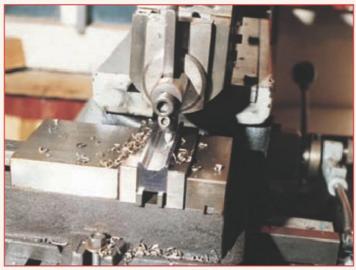
Model Engineers' Workshop



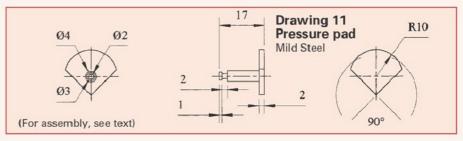
10. Setting fixed jaw parallel to ram movement

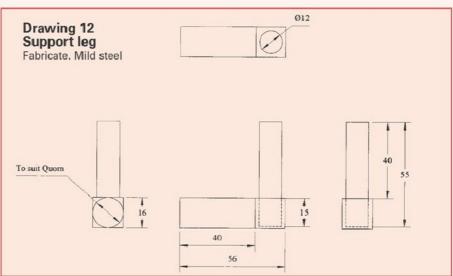
piece is then tapped down firmly on to a pair of parallels and the vee roughed out using a 60 degree vee tool with a rounded nose (Photo 11). The tool slide is set vertical for this part and I work from right to left, using the self-act until almost to the bottom of the rough vee. The tool slide is then swung through 45 degrees and the clapper box set over in the opposite direction so that the tool lifts away from the machined surface on the return stroke. The tool is of the shape shown in the photo and you of course need one of each hand. The tool can be fed downwards while doing further roughing almost to the marked line and the finishing cut made by feeding the tool upwards. Photo 12 shows this process being completed on the left hand side of the vee.

End milling a vee of this size with amateur equipment is quite a substantial undertaking and good finish of the wall of the vee cut with the side of the end mill is very much dependent on having a sharp cutter, well centred in whatever chuck you may have. If you have an angle vice, start by setting the fixed jaw parallel to the movement of the longitudinal slide and set the work piece down on parallels. Then rotate the vice through 45 degrees in the vertical plane to do the machining, necessarily in small steps with the light machinery available to most amateurs. If you don't have an angle vice, things get problematical. You could hold the blank



11. Roughing a vee











work piece, rotated 45 degrees on its axis, in a normal machine vice, but the grip and alignment are likely to be uncertain unless the vice is in good condition so that the moving jaw doesn't lift.

Once a long vee has been produced, two quarters can be sawn off and their ends squared and marked out ready for drilling the holes for the bar bed. Obviously these have to be well-aligned and once one had been drilled in the lathe, I used it as a drilling jig, the two parts held in a vee block as shown in Photo 13 to spot through to the next. If the drill wanders a little, it doesn't matter too much for the intermediate and rear vees, but if the hole in the front vee is not parallel with the vee itself, then the longer the drill, the worse the misalignment of the other two vees. My drill did wander and so I pegged the hole in order to be able set up the front vee in the four-jaw chuck with the misdrilled hole centred (Photo 14). I then bored out the hole, glued in a plug and drilled and bored out a new hole in the lathe (Photo 15). The flat-bottomed hole for the support leg is best bored in the lathe. Cross drill and tap the holes for grub screws in the front vee and knurled thumb screws (Part 6) for the other two. While you have the dust cover off the lathe this might be a good point at which to make

the latter which are simple knurling and turning exercises.

It is undoubtedly easier to form the facet on the nose of the front vee using a vertical milling machine rather than a shaping machine, but it can be done on the latter, with a certain amount of effort. In either case, a tilting vice is almost indispensable, indeed, without using a complex jig, I cannot think how else it could be done. My approach was to set over the vee at 10 degrees to the top of the vice jaw and then to tilt the vice 31 degrees. I then milled the facet until it reached the point of the vee. Without the 10 degree angle, the edge of the facet would drop vertically downwards from the apex of the vee and machining the seat for the lip guide would be much simpler, but the 10 degree angle is needed so that the edge of the lip guide leans backwards away from the face of the wheel. Some readers may be able to calculate how much to rotate the vice on the machine table to mill the seat for the lip guide. As my trigonometry stops at a fairly elementary stage, I chose a cut-and-look method, using a narrow end mill and widened the seat once I had the alignment of the vice correct (Photo 16).

Back plate (part 7)

This is simple sawing filing drilling and

tapping, followed by spotting through to the rear vee for the tapped fixing holes in the latter. I had a tap 1/16 in x 40 tpi so I used this because it is finer than the metric series that I usually use. A 0 B.A. size would do just as well.

Lip guide (part 2)

Those who are keen to see things take shape will probably choose this point to make the lip guide. This means a return to basic marking out, sawing and filing to a line on a fairly small scale, something that will be well within the capability of most model engineers. I was not able to calculate the angle of the top lip and measured it from the finished article. It just has to be approximately parallel to the edge of the vee. It is after all simply a fixed resting place for the land of the drill. I did not have any suitable gauge plate so I made mine out of mild steel sheet and milled the slot before cutting out the rest of the guide, then filing it to a very snug fit in its seat.. Note that the bevel is on the back of the guide, facing the tail. I casehardened the lip of mine and left it glasshard, something that you cannot do with gauge plate, for fear of it cracking. I would suggest tempering gauge plate to a pale straw colour.

Adjusting screw and pad (parts 8 and 9)

The screw can be threaded using a die, but it must not be a drunken thread, so the die will have to be held in a tailstock dieholder. Drilling right through for the pad and its retaining spring (an idea that I copied from Duplex) has to be taken in easy stages as the hole is classified as "very deep". The knurled bit is simply a stub that is knurled, drilled, tapped and glued on to the end of the screw.

The pressure pad is simple turning. A piece of 20 mm diameter mild steel is turned down to 4 mm to fit snugly in the central hole in the feed screw and then further reduced and grooved as shown to fit whatever tension spring you may have on hand. After parting off, the vee shape is then filed to fit the rear vee block. The two are married together on assembly by snapping the end of the spring into the groove, opening up a loop greater than 4 mm diameter in the other end of the spring and dragging it through the screw on a hook of wire until the pad is held firmly in

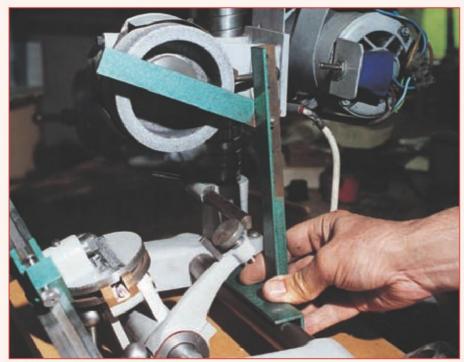
15. Re-boring plugged hole



16. Milling lip guide seat on facet



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17. Rough and ready wheel setting

place while still being able to rotate.

Support leg (part 10)

This is fabricated from a piece of 16 mm square bar and a piece of 12 mm round. The square piece is centred in the four jaw chuck, centre drilled and the tail centre brought up for support to turn down the square to 16 mm diameter. The square end is then drilled 12 mm and the piece of round bar glued in.

Bed (part 5)

This is simply a 220 mm length of 8 mm diameter cold rolled bar. I did consider using square bar or machining a flat on the round bar and using the thumb screws to locate the vees, but this is a very poor way of ensuring angular alignment. One could of course use square holes, but this would require broaching, a process that is beyond most amateurs reach, including my own.



18. Setting offset square

Offset squares

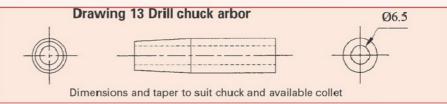
I give drawings for only one of these, for setting up the Duplex jig on the Quorn, but Photo 16 shows another simple offset square in use, made from three lengths of 25 x 25 x 3 mm cold rolled steel angle screwed and bolted together. I use it to set the face of cup wheels square to the

rear(and front) bed of the Quorn when no great precision is needed. Readers are welcome to copy it though I imagine most will already have devised something similar. The Duplex setting square is a simple sawing, filing and drilling exercise, following by facing, drilling and tapping the 12 mm bar M8 or similar for two cap headed Allen screws. Once assembled, it is set square off a surface plate as shown in Photo 18 and the screws tightened. A coat or two of Hammerite paint should then lock things in place as long as you don't drop it. The purist may prefer something more elaborate with dowel pins, but I was in a hurry and it is easy enough to reset it if need be.

Chuck adapter

I have a set of three Clare collets and have made an adaptor so that they can be used in the Quorn to hold end mills. It occurred to me that I could make a hollow parallel arbor so that a small Jacobs chuck could be held in one of the collets and, if drilled through, used to hold drills down to 0.5 mm in size (readers of MEW No 59 will know it is safe to drill through a drill chuck). The idea is almost too simple to merit a drawing, but I include one for completeness and Photo 19 shows the finished idea. A hand lens is needed to check that the facets are correct, but once one has been correctly set, the other one can be ground after simply rotating the chuck through 180 degrees.

I hope that my explorations will be of use to frustrated Quorn users and as usual I will be happy to hear suggestions and criticisms via the Editor or by e-mail at engineer@clear.net.nz.





19. Chuck adapted for small drill grinding

SOME IDEAS ON QUICK CHANGE TOOLING



was very interested to read Philip Amos's account of his quick-change tool system in M.E.W. No.81, as I had arrived at a similar system by a different route. I believe some of my devices could also be used with his system, and may be of general interest, as I find them to be very convenient and time-saving. It would be nice to claim that all the items I will describe were the result of purposeful design, but the fact is that many of them more or less turned up as incidental benefits while other targets were being pursued.

I had better begin at the beginning: forty years ago I bought an old Logan lathe of 5½ in. centre height. It is an American

machine, and similar to a South Bend. On to this I grafted a Myford long cross-slide to enable me to do some small milling jobs. Soon I learned the hard way that the tee-slots in the Myford slide are not very robust and are easily damaged. Resolve: make up some long well-fitting tee nuts (to spread the load) and try to attach things to the cross-slide by clamping flat surfaces directly onto the slide. Next I realised that I had only very occasional use for the rotating top-slide, and I achieved greater rigidity by mounting a steel block on the cross-slide to carry the four-way tool-post, as others have also done. This has now evolved into the arrangement shown in Photos 1 and 2, a piece of 12 mm steel

Amhlaoibh Hennessy summarises his toolholding accessories which have evolved over a number of years.

plate is fixed to the cross-slide by four short % in. B.S.F. capscrews which engage in 1in, long tee-nuts. The plate carries an array of holes tapped 16 in. B S.F. Six of these allow the steel block to be mounted in two different positions (for normal and very large jobs): all are available to hold milling jobs by means of studs of various lengths. The work can be very securely held without any danger of damage to the cross-slide. The holes are protected from swarf by a sheet steel cover when not required. For convenience, a hex key for the mounting block screws has been lengthened to clear the stud, Photo 3. The Myford cross-slide can be wound off and can be replaced by the original cross-and top-slides in a few moments if tapers are needed. The mounting block on the Myford slide comes to exactly the same level as the top of the original top-slide, so that tool-posts with tools set to centre height will be correct on either.

An excellent four-way indexing toolpost came with the lathe, but I soon found that four tools were seldom enough, and there were problems when left and right hand tools had to be accommodated. Then I saw the late Dave Lammas's article on his three-way tool-post in M.E.W. No.27, which offered a solution to many of these problems so I proceeded to make up a few toolposts to his design. I made mine the hard way: the top and bottom plates were



2. Baseplate and Block mounted on cross slide.



3. Extended hex. key.

hacksawed (very good for the soul) from 12 mm steel, with a triangular centre piece from 1in, thick aluminium. Photo 4 shows one in position, and also the sheet steel cover for the base plate. It also shows the clamping nut, which by accident not by design, turned out to be a great success. It is about 2 in. long, and made from 1% in. diameter stock, and threaded (½ in. B.S.W.) for a length of % in. at the top end. The result is that a few flicks of a finger spins it all the way up or down, making tool-post changes very quick. About 20 seconds brings another set of tools into action. A short ring spanner is used for the final tightening via the hex at the top. The same spanner fits the tailstock locking nut where it normally resides, very convenient to hand, as can be seen in Photo 4.

Base plate and block assembly

Fig. 1 shows details of the base plate, and Fig. 2 the mounting block, stud, and nut. The bottom of the base plate should be quite flat. My plate was pretty good as it stood so after removing the mill scale I tried it on a surface plate and a little scraping soon brought it to a satisfactory condition. The holes for the capscrews have to be counterbored. Having no suitable counterbore I used a twist drill. Purists may be shocked but I find it works. The holes marked B and the corresponding holes in the mounting block must be set out and drilled accurately if the block is to fit in both its positions. The other holes are indicated by crosses to avoid confusion, as their positions are entirely optional. There is plenty of room for more if they are ever required.

The height shown for the mounting block is only approximate. It should bring the top of the block to the same level as the topslide when that is fitted, so that toolposts can be used on either without having to alter tool packing I did this by chucking a piece of silver steel and measuring from its upper surface to the top of the topslide using a vernier height gauge. Repeat the exercise to the top of the base plate (without rotating the chuck) and the difference gives the required height for the mounting block.

The long stud is a legacy from the original four-way toolpost that came with the lathe. Had I decided at the start (as I did later) to retire this toolpost I would have had a shorter stud and an ordinary nut, which would not have had the flywheel effect of the heavy nut. As well as the rapid action already described, the nut and stud I arrived at will also clamp items of a wide range of thickness without additional packing washers.

Lammas style toolposts

Photo 5 shows my basic left and right hand Lammas toolposts, and Fig 3 gives their dimensions. The first thing to decide is the size of tool to be used: I decided on ¾ in. square as standard, but with the capacity to take ½ in high tools. The height of the tool, plus an allowance for packing, will decide the allowable thickness range of the bottom plate,

A BRIEF ASIDE ON USING THE HACKSAW

Most readers seem to have bandsaws these days, but the hacksaw is a very useful tool when you get the knack of it. Here are a number of points I find helpful when there is much hacksawing to be done.

Select your frame carefully: it should be comfortable, rigid, and with a little bit of weight: many are too light.

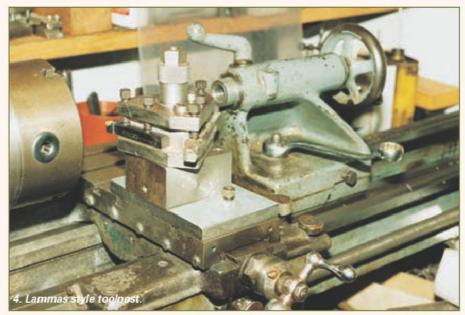
Use all-hard H.S.S. blades of good quality; the bimetal ones have their uses but with prolonged use the backing metal will stretch and the blade will no longer cut straight.

Do not allow the blade to touch the hardened vice jaws: if it does it will also refuse to cut straight.

Set up the work securely in the vice, if possible so that it can be attacked with the forearms horizontal. When cutting plate, the cut should be at about 25 degrees to the surface. This makes it easier to follow a straight line. If the plate cannot be set up at this angle, and there is much sawing to be done, consider standing on something, which of course must be secure, which will raise your feet by eight or nine inches.

Now of course all-hard blades are also all-brittle, and if you wobble in your stroke you will now have two half-blades to add to your sundry stock. But it is well worth while to learn a smooth, even stroke, and enjoy the resulting long blade life and straight cutting.

Finally, never continue cutting until your arms are tiring: you will be certain to wobble and snap the blade. I count the strokes and work in spells of 50 to 70 strokes, depending on how I feel. A few moments rest and I do another spell. It may be relevant here that I am 75 years of age. After about 6 spells I do something else for a while before returning for another session If you can leave the job set up in the vice you can do a few spells whenever you pass by. It is encouraging to put a pencil mark at the end of the cut after each spell, and it will also give warning when the blade finally begins to get blunt.



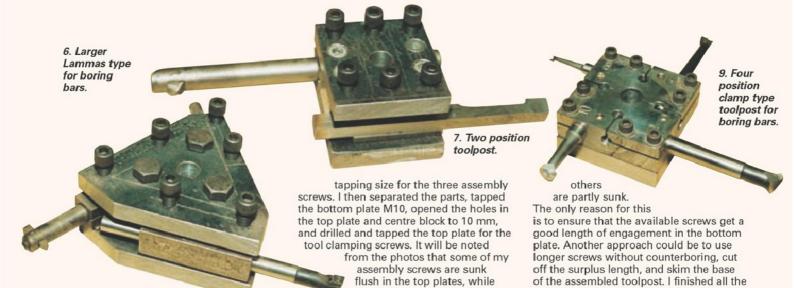
and also the height of the centre block My centre blocks are cut from a 2½ in. by 1 in. aluminium bar. I cut these with a 6in.

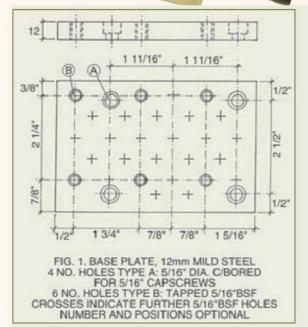
nium bar. I cut these with a 6in.
slitting saw mounted on a

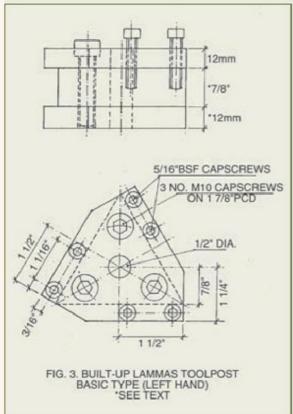


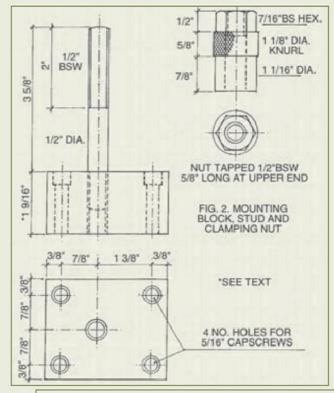
straightforward. I marked out the holes in the top plate, drilled the centre holes in all three parts, mounted them on a closefitting bolt in their correct alignment,

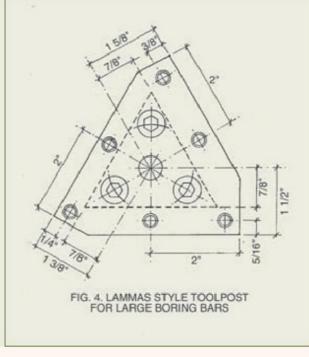
marked them for reassembly, and drilled right through M10

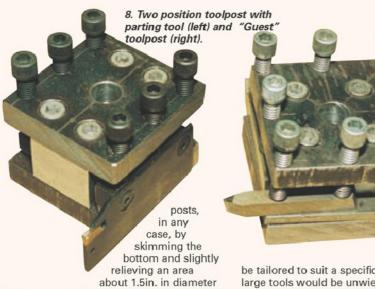












to give secure clamping. All my three-way posts have three assembly screws, either MI0 or ¾in. B.S.F., while my two-way and four-way posts have four ¾in. B.S.F. screws. These have smaller heads than M8 screws. Photo 6 shows a larger three-way post to accommodate boring bars: Fig.4 gives its dimensions. Though I have shown capscrews in Fig. 4 it will be noticed from the photo that I have used hex setscrews for assembly as there is plenty of room on this post.

Larger Tools and Parting Tools

Photo 7 and Fig. 5 show how a toolpost

be tailored to suit a specific tool. These large tools would be unwieldy on any but a two-way post. **Photo 8** shows another two-way post for parting tools, and, on the right, what I call my guest toolpost, which is available for the odd tool that may be required from time to time. **Fig. 6** gives its dimensions. I have provided two toolseats % in. wide and two % in. wide. Two-way and four-way posts, if flat stock of suitable width and thickness is available, will involve much less hacksawing than the three-way ones, and are quite easy to make.

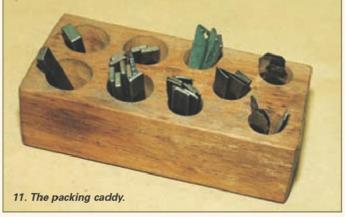
Photo 9 and Fig. 7 show a toolpost to hold small boring tools. It holds three Orkan H.S.S. tools, two with 10 mm shanks one with 8mm, as well as one tool with a ½ in. shank. As these tools have their cutting edge at the level of the centre

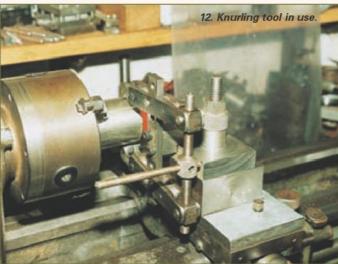
of the shank, the sockets can be bored from the lathe spindle with the embryo toolpost clamped on the mounting block. The form of tool clamping shown is very secure provided that the tool shank is a very close fit in its socket. I suppose the sockets should be finished with D-bits but I enlarged the holes in very gradual stages and finished them with drills which I had freshly sharpened as carefully as I could on my Reliance drill grinding jig. (An excellent tool, incidentally. I have not seen it advertised recently: is it still in production? Mine is the 1/4 - 1/2 in. model, but I have persuaded it to handle drills up to 1in.) The tool sockets are drilled to the centreline, where they are met by two ¼ in. holes, one from the top and one from the front The slots were cut with a small slitting saw. It would simplify this operation if the ¼ in. holes were a little bigger. There was a small residue in some of the slots beyond the reach of the sitting saw which had to be fiddled out with a piece of hacksaw blade. The photo shows that my toolpost is made up of two pieces. This was dictated by the stock situation.

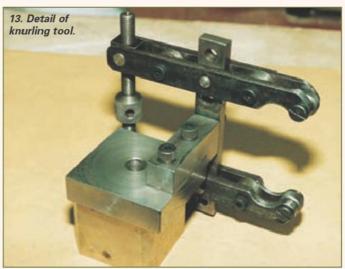
Tool Height Gauge

Photo 10 shows the centre height gauge I made to go with the new toolposts. It consists of a heavy base, made from 2½ in. by 1 in. channel ‰ in. thick, cut to sit level and without rocking on the lathe bed. To this a vertical post is fixed, carrying a short cross-arm which carries a short vertical rod. Grubscrews fix the cross-arm to the post and rod. I set the base of the rod accurately at centre height as follows: I









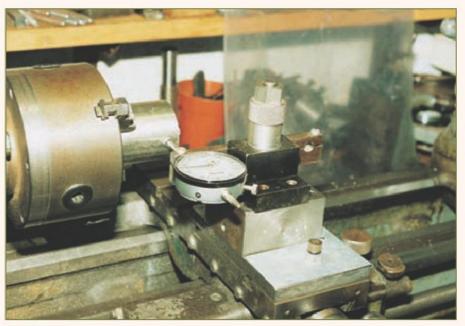


14. DTI and mounting arrangement.

faced both ends of the short rod carefully and finished them with a rub on an oilstone, and I also gave the upper surface of the cross-arm a smooth finish I then chucked a piece of ¼in. round silver steel and verified with a DTI that it was truly centred. I set the short rod with the top end exactly 0.125in. above the top surface of the cross-arm using a step micrometer and clamped it lightly. I then set the gauge on the lathe bed and lowered the crossarm until the short rod rested on the top of the rod in the chuck. I clamped the crossarm at this position and then lowered the short rod until its upper surface was flush with the top of the cross-arm, and clamped it there. Of course you have to see that the rod will finish up where tools can be presented to it as shown in the photo. Photo 11 shows my packing caddy. The result of this, after years of fumbling and making shift, is the joy of pipless facing every time.

Other Accessories

I now had a range of tools which could be brought into use at a moment's notice, each perfectly set to centre height, but there were still the items like the knurling tool and DTI holder which had formerly involved evicting a tool from the tool-post.



15. DTI in use.

The answer was simple: provide each with its own mounting base to be clamped to the mounting block or top-slide, whichever is in position.

Photo 12 shows my knurling tool in position, and Photo 13 shows a little more detail of it. The tool is a reworked version of one I made over thirty years ago. It can deal with jobs up to 3½ in. diameter. The design took this shape because I wanted to find a use for some left hand taps and dies I had acquired, but it turned out to be good because of the short projection of the knurls from the pivots about which the arms rotate.

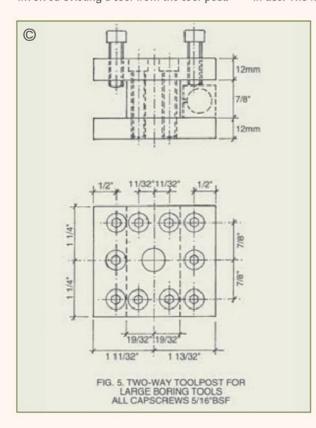
Photo 14 shows the DTI mounting. The DTI can be fitted at the other end to deal with larger workpieces. Photo 15 shows it in use. The mounting base is as it came

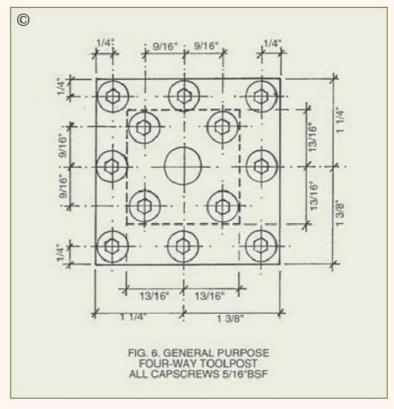
from the scrap-box.

Photo 16 shows a mounting to take a Baty DTI set, and alongside, a forcing bar for starting drills true when drilling from the tailstock.

Photo 17 shows a Myford plain vertical slide securely mounted. This involved drilling a ½ in. hole in the base (is this a sacrilege?) in a position which allows the slide to pass down beyond the face of the mounting block.

There are many other tools which could be mounted using this system. I have a hand turning rest on the programme, but ball-turning tools, milling spindles, and others also come to mind. This system does not allow for indexing, but I have never felt a need for it. Depends on the kind of work you do, I suppose.







16. Forcing bar (left) and mounting for Baty DTI.



18. Swivelling base for vertical slide.



19. Components of swivelling base.

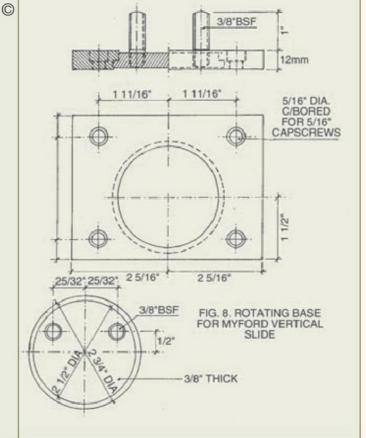


17. Mounting arrangement for Myford vertical slide.

Finally, Photo 18 shows a device which allows the plain Myford vertical slide to be rotated about a vertical axis. It consists of a plate which replaces the plate shown in Photo 1, being fixed to the long cross-slide by the same fixings, together with a circular inset plate which carries two %in. B.S.F. studs. These match the holes in the base of the Myford plain vertical slide, which thus can be rotated in a horizontal plane. Photo 19 shows the rotating piece and the underside of the plate: it has been lightly scraped to give a good seating on the long cross-slide. The extra holes in the round plate serve no purpose, except to record an error in calculation. Fig. 8 shows details of this item. The round plate is best made first so that it can then be used as a gauge when the hole in the plate is being bored.

I have not given detailed working instructions on the basis of an Irish proverb which translates as "A hint is enough for the knowled geable", and in any case, anybody wishing to do something similar would have to work out dimensions and other matters to suit his or her own requirements.

TO SUIT BORING TOOL 1/4" DIA M5x20 CAPSCREWS LATHE CENTRE HEIGHT .8/4. 9/16" 1 1/4" 1 1/4" 1/4" DIA SLOTS 1/16" APPROX. 1/2" DIA. 9/16 1.1/4" 1 1/4 FIG. 7. TOOLPOST TO HOLD FOUR ROUND-SHANK BORING TOOLS
*THIS DIMESION TO BRING TOOL LSOCKET TO LATHE CENTRE HEIGHT



SCRIBE A LINE

Mr. John Wilson, of Harlow, Essex, writes:

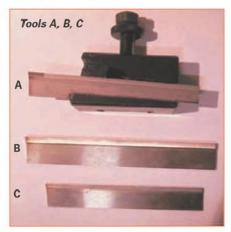
I have been reading with interest Philip Amos's article on Parting Tool Techniques and having worked as a Maintenance Engineer (serving my apprenticeship with a company that manufactured printing machines, then moving on to maintenance in the wine trade and finishing up the last 10 years, before taking early retirement, in the turned parts trade) I am curious as to why lathes for model engineering are invariably supplied with parting tool holders that are set with several degrees of top rake.

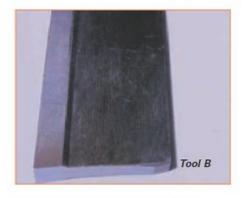
At no time in my 43 years of engineering, have I seen top rake used for parting tools. In the turned parts trade using Swiss automatics & 6 spindle automatics, tool holders such as "A" in the accompanying photo 1 would be impractical, as each time you had to sharpen or change a tool, you would have to reset the tool centre height. Now given that both the smaller Swiss automatics (or sliding head machines) and their bigger brothers the 6 spindle automatics are used to turn any material from plastic, stainless steel cast iron, copper, brass, aluminium & steel in all grades & shapes, to very high finishes & tolerances, one has to conclude that top rake is perhaps unnecessary.

Another interesting point about parting off in the turned parts trade, is that the tool is often a form tool making chamfers or more complicated shape. The photo of tool D shows an 8 mm parting tool that chamfers both edges of the bar as it parts off. This tool is typical of the type used on Swiss automatics.

Tools "B & C" are typical of the parting blades used on the bigger multi spindle machines and were made by J.J. Churchill Ltd of Market Bosworth. They are marked Emprite PM5, and have a hollow ground top face. The tipped blade "A" has been ground away to fit the parting tool holder on my lathe, but I will be making a rear tool post in due course, so that I can mount my parting blades without any rake. The tipped blade is made by Empire tool Co. Memphis and is a P3N C6 TC.

For those not familiar with Swiss automatics or Multi spindle machines, the Swiss autos that I was involved with were sliding head single spindle lathes and,

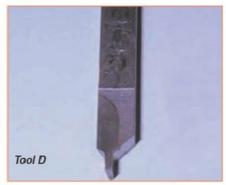




unlike a conventional lathe, the bar is carried along by the sliding headstock past the tool to turn the appropriate diameter. The tool or tools would rock back and forwards to form various diameters and forms on the bar as it was fed along by the sliding head. The machines we had, could handle material up to 12 mm dia., though bigger machines are made.

The Multi Spindle machines come in various sizes, and ours ranged from 5/8in to 1 3/4in. (the sizes denoting the largest bar the machine can hold). Each had six spindles and a possible fourteen machining operations taking place at some point in the machines cycle. (from a bar being fed out to its stop, fully machined & parted off, which is one full revolution of the drum carrying the six spindles). Unlike the Swiss autos, the multi's feed the bar out a predetermined distance and then the diameters are machined using form tools and/or tools mounted on slides, which move in a similar way to the saddle on a conventional lathe, but with very limited travel. Both the Swiss machines & the Multi's took bars in lengths up to 10ft. long. I hope this is of interest?

On a totally different topic, oh how I agree with the sentiments expressed in "On the Editor's Bench, Real World Engineering". Harlow, where I live and worked for many years used to have a major industrial base, with companies like International Distillers & Vintners (IDV) with their large wine and spirit bottling plant, Shreibers manufacturing furniture, Johnson Mathey had a large manufacturing site making things like catalytic converters, Press Bodies making body panels for Fords, ITT making electronic components, Cossors also in the electronics and defence business. Then there were the numerous small engineering companies making components for bigger companies like Fords



Now all that is left are a few companies like Cossors who have changed name and shrunk to a fraction of their original size. IDV had two large sites, one is now a Supermarket, the other a warehouse. Johnson Mathey's site is a Supermarket, Press Bodies site is now taken with two car showrooms & a small retail park. Shreibers site is car parking & Tyre & Exhaust repairs.

Successive governments have ignored the situation or dismiss the decline as unimportant, with the result that there are no real jobs left.

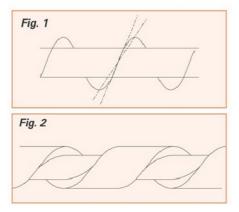
I served my apprenticeship with a company in Bow, East London, building printing machines for six years, I then worked as a Maintenance Fitter for IDV for 25 years and for a small Hertford based engineering company for 10 years, all good paid jobs. All three companies are now gone and the chances of our children getting well paid and interesting jobs, where they can take early retirement (at 58 in my case) have long gone. It seems the best they can hope for is shelf filling at a supermarket or cleaning on minimum wages. God help our youngsters, because there is no future for them in industry.

Comment from Dave Fenner

My guess is that Mr Wilson's experience of zero rake tools stems in part from the need to compromise on several counts. First as he says, many different materials were encountered, and if one tool can be used satisfactorily, then why have more. Secondly, before replaceable tips gained popularity, resharpening implied resetting. Thirdly, if a tool such as "D" is used, then it is cutting at more than one diameter, and it will not be possible to set the tool cutting edges on centre unless it is set with zero rake. I understand that the latest tipped part off blades have multiple top grooves and some positive rake. With turning tools in general, much work has been done in the past to determine optimum angles for high speed tools cutting various materials. Using the optimum should give good finish, machining time, tool life and tool loading. This last factor assumes some importance in the amateur context where machine rigidity and spindle power may somewhat lower than in an industrial

Mr M. Connelly writes by email:

I read the letter in issue 88 from Mr H. Lord and the reply by Bob Loader regarding screw threads and helix angles. I understand the mistake made by Mr Lord and also agree with Mr Loader's calculation of helix angle. I would like to point out that the origin of Mr Lord's mistake is probably the fact that when drawing a thread people tend to draw a saw-tooth pattern when the true form of a thread in plan view is a sine wave. This true form is impossible to see on the



majority of threads using the human eye and when drawn correctly sometimes looks wrong.

If the thread is drawn with a stretched axis (Fig1) that makes it look like it has a long pitch it is possible to draw the line Mr Lord found the angle of, and also the correct helix angle as calculated by Mr Loader. The source of the error becomes obvious, see figure. With this knowledge of the plan view of the thread it should be possible for Mr Lord to find the best way to machine his chuck jaws to suit the thread he has produced. I know from looking at the thread on my own chuck jaws that the sides are not flat but are lenticular and so must be made to suit this sine curve in some manner. If the thread is drawn completely with a CAD program, (Fig 2) the root of the thread can be seen to be significant as far as the final shape is concerned, the lenticular shape on the jaws seems to match this drawing. I hope this helps in some way.

Mike Thurgood of Milnerton, South Africa, writes:

I entirely agree with what you say in your editorial, Drawings, Standards and Attitude - MEW No.87, December 2002/January 2003. For someone to complain about missing dimensions when clear notes are made on drawings which indicate which parts are intended to fit together is either demonstrating an unfortunate inflexible attitude, or they had a bad business dinner the previous evening! I haven't seen the drawing of the Plans Service Drawing WE 19, but your comments make the situation quite clear. Where exact dimensions are concerned, again I entirely agree with your remarks. It would be unusual for a typical model engineer to go into mass production, which would then certainly require the correct replication of parts when off the shelf replacements are required.

When I construct hot air engines from pre-prepared drawings, a particular dimension may be given for the bore of a cast iron power cylinder, with that of its piston to match. But if the bore of the cylinder is, say, 35 mm and there is plenty of wall thickness I may not bother to bore even to the nearest millimetre: I would most likely go for a slightly larger diameter on the basis that it might provide just a little more power output, whether or not the theorists would entirely agree with this philosophy. What is essential is that the

bore is parallel and honed smooth. Also, of course, that the piston is turned to suit the bore, the right fit being shown by closing the cylinder at its lower end and placing the piston into the bore, when it should just very slowly slide down the cylinder.

But then I am apt to change dimensions or other features on drawings if I think that something doesn't look quite right to me. One such change is the number of attachment screws of a cylinder head to the body. You often see them attached with as few as four or six screws. Although this may be perfectly adequate, it never looks right to me. I will increase the number from nine to twelve, depending on the diameter, but possibly go down one BA size in the process.

Another example: loco wheels. Although the drivers all need to be the exactly the same diameter, at least to start out, they gradually wear in use, but scale locos still manage to run very successfully. However, the crank distances on each wheel must be identical otherwise there would indeed be great problems with the driving links. Therefore whatever dimension is given on the drawing doesn't need to be adhered to, to the nearest +/-0.1 mm, as long as they are all the same. Even loco cylinder bores don't have to be identical to some tiny dimensional tolerance - there's quite a wide latitude. but the pistons do need to be a good fit.

And, no, I am not suggesting that dimensional differences of 10 mm are tolerable, but a millimetre difference in 50 mm diameter for a cylinder bore is generally of no consequence.

Likewise for axles and bearings, providing the one is a good matching fit to the other.

My comments all relate to small dimensional differences, of course. But it's really only when you get to commercial scale work, with thousands of repeat components, that reproducibility becomes essential. As, for example, replacing the tailstock barrel on my mid-1960's Myford Super 7 lathe in 2000. The new barrel was a perfect fit - certainly nothing less to be expected from Myford's.

Arthur Owens of Claverdon writes:

Mike Haughton's' article On the Internet is interesting and I would also encourage doubters to take the plunge. Some comments.

Get a virus checker. Products from MacAfee, Sophos, Symantec or F-Prot are well regarded (I use FProt - usual disclaimer). They can be downloaded or in many cases bought on CD. Prices are not that high around £36 inclusive of VAT for the Symantec Norton AntiVirus 2003.

The Internet is not a library. In many respects it is the antithesis of a library. A library is an organised collection of material with controlled indexing and careful arrangement of its collection. Everything is set out in a logical fashion, and its operators have exercised a degree of quality control. (Well that is the theory, anyway!) The Internet is none of those things - which is why search engine results must be interpreted with care. As Mike

says - think about why someone has put content on the Internet (actually usually the Web - which is a subset of the Internet). It isn't necessarily there for altruistic reasons! Furthermore not everything is available free on the Web. Many valuable indexing and full text services are out there and password controlled - you can subscribe to them, but your friendly local University Library will be paying many thousands of pounds a year to access just a single service. You are unlikely to have access at all unless you happen to have similar funds to spare.

Not all colleges and universities will be able to allow Web/Internet access to the public, even for a fee. There is a whole minefield of copyright, contractual and other restrictions which explain this, so don't assume your local college can help. Check in advance. However, recent Government initiatives mean that more and more public libraries offer access for comparatively modest fees.

All sounds a bit negative but (this is the up bit) I used the Web a few years ago when deciding what lathe to buy. No engineer, I bought a Sherline lathe partly because of the speedy response of the British agents (Millhill Supplies - again usual disclaimer), but also because the makers clearly understand that many of their customers are like me, first time buyers and users of small machine tools. Their website is not just an advertisement All the kit represented comes with full and helpful guidance, which makes few assumptions about previous knowledge and at the time everyone else seemed to want to sell me something - and that was it.

I have recently been making parts for a REMAP project (lots or references to REMAP in ME and MEW) including machining plastics about which I knew nothing - searches on the Web produced quantities of helpful information. Given my job (a librarian at Coventry University) it is probable I could have found the information at work - although even then it could well have been by doing what I did in Google from home.

Finally, drawings for the same REMAP project have been transmitted to me as email attachments. Wonderfully convenient and flexible.

I could go on! I spend quite a lot of time teaching students how to use the Internet. I make no claim to infallibility, but like Mike, if anyone wants to contact me I am Arthur@arthurowens.demon.co.uk and am happy to take questions or just continue the discussion.

Mr Bernard Langley of Stoke-on Trent writes:

As Chairman of a small family engineering business I have long been a keen reader of your magazine. I do this partly because of my personal practical interests but also because yours is one of the few periodicals to deal with the sort of operations that we actually DO.

One gets the impression that most of the new generation of engineers want to sit in front of a VDU while someone else, or more probably a CNC device runs the actual operation. I think one reason why

model engineering affairs are so well attended by older engineers is that they are bored to death with their daytime occupation of form filling and box ticking and seek release in the evenings at their own lathes..

I have written to you on this topic before but I am driven to say the same thing again by your perceptive leader on p11 of the February/March issue of your admirable journal. From my own observation I would not be at all surprised if more folk attended a model engineering event than came to a "grown up" one.

Like you I am not entirely clear by what is meant by the "knowledge based economy". It seems to mean not getting your hands dirty. I realise that the service industries can contribute to the national cash flow while not "making" anything but my latest figures show that service industries made an export/import surplus of £13Bn but that manufactured goods overall lost £34Bn.

Perhaps some of the folk who are so good with their Myfords in the evenings could do a bit more for us in their day jobs to revive engineering manufacture.

Mr. G K Bartlett of Selly Oak, Birmingham writes:

Just a couple of quickies first. Trust Ray McMahon to come up with such a simple solution to the lack of a clutch on the excellent B600 type lathe or similar. I had tried to work something out for a couple of years on and off.

Second, why do people seem to need a DTI to set work in a four jaw chuck. I am not boasting but rarely use a DTI for this purpose unless it is really critical. It takes a fraction of the time to first use ref points on the jaws or setting rings then wind a non-cutting edge of the tool a little way from the work surface and judge by eye the run out. Finally, wind the tool closer almost touching the surface and move the chuck in reverse. In fact you can usually let the tool just slightly mark the work surface. This method takes all of a couple of minutes and I have checked it many times with a DTI and not been able to improve on it. A similar method can be used for square work pieces and also for checks on straightness of grip in the chuck.

More importantly ref. Vasillii Zacharov's excellent speed control articles. He has been very careful in the wording to say treat the complete motor and control as a unit and leave as is; i.e. do not try mods unless you are versed in electronics. Please heed this if for no other reason than the lack of transformer isolation in these devices. They fall into my don't-liketo-work-on-category as I would not consider any point on the cct board safe to touch while switched on. The neutral line should be at or very close to earth potential but don't bet on it. I am not over cautious by any means and have little time for the HSE but have received my fair share of electrical shocks in my working life and didn't like any of them. My phobia about non isolation dates back to my few years in TV servicing in the 1950's and believe me TVs in those days

were horrendously dangerous to work on due to the AC/DC Live chassis construction used then.

Imagine the scenario working in domestic property probably crouched with your back against exposed gas or water pipes on a TV with more than likely a two pin mains plug and a fifty-fifty chance of a 240V live metalwork to work on, not to mention connecting earthed test gear to same. Obviously polarity was the first check but the neutral line was not necessarily truly neutral. I soon moved into professional Scientific and Instrumentation Electronic and Mechanical work and was much happier working on equipment which often had quite complex Electronic control ccts floated up at maybe 10kV or more above Earth and often had to float the test gear up with it but you didn't touch it ,curtains if you did.

I also learned the first lesson with large industrial X ray equipment 400 kV or more that you never removed the EHT cables on a switched off rig without discharging the cables. The first time you discharged the cables meant you never forgot to do it in future, a great beefy spark several inches long. The cables have quite a large capacitance and hold a charge for a surprising time as the insulation has to be very good.

I have one or two pieces of workshop equipment with DC motors and home built controllers but all but one 12volt and completely isolated. The one mains powered unit is transformer isolated right up to the TRIAC and snubber components. This means that I might curse and swear if a fault appears (as I have little interest in electronics since retirement) but at least I can work on them with safety.

Peter J King of Christchurch, New Zealand writes:

With reference to the letter from Mr Bill Brading MEW 88, February/March 2003. I own or have owned various different drill sharpening jigs, only one sharpens drills as near as makes no difference exactly as per the original sharpening and down to 0.0625in. dia. This is an old "Reliance" No1 size jig that I bought new from Tyzack's shop in Bishopsgate, city of London. about 37 years ago The "Reliance" (which was horrendously expensive) has apparently disappeared from the market and Tyzack's little 'City' shop is probably history by now. Also when the 'Reliance' is used exactly as per instructions, a very, very light cut with the grinder tends to touch evenly over the whole factory finished 'back off' surface of the drill. Thus obviously replicating the original profile. No other drill jig of my experience will do the same. I have been tempted in the past by various jigs and devices, clearly of the same type as Mr Brading has used, with multiple adjustments etc, none stood up to that standard. I wish that some manufacturer made replicas of these "Reliance" jigs, although there would be little call for the size three model that I also own (0.5 to 2in.) -it looks like it takes two men to lift it The difference between these and the more

recent arid cheaper jigs appears to be a subtle combination of angles, with the pivot angle to the vertical and the drill trough angled to but not intersecting this

I would recommend that Mr Brading tries to get a second-hand jig of this make. All three sizes are useful and all have the same subtle design.

Mr Ian Burton of Queensland, Australia, writes:

I read with great interest the article by Vasillii Zakharov, regarding electronic speed control using washing machine components, (issue 86). I wonder if such a motor would remove the vibrations inherent in single phase motors?. I'll try it and see.

My lathe, of Taiwanese make, is 40in. between centres, and 8in. swing over saddle. It is over 10 years old, but still accurate. When purchased, the motor (approx 2hp) was D.O.L. start with forward, stop, reverse on the saddle levers. Making any quantity of parts was sure to blow the fuse in the box, (10 A) and if this was uprated, blew the house fuse also. Even without cutting metal, the motor would cause the circuit breaker (1500w) in my multi-box to trip after 1-2 minutes. The Chinese motor, being very heavy, also took ages to stop, very annoying in a production run.

Eventually it stopped working and was replaced with an Aussie made motor, -very much better and doesn't trip the multi-box. When fitting the new motor, I did some thinking, and when the sketches were finished, had clutch start, and brake stop. I fitted an automotive air conditioner clutch on the headstock input spindle, and another driven from it, to the machine. A bit of fiddling with switches from the local auto store "Supercheap", and a cheap battery charger gives me: handle down—lathe start; handle centre—lathe coast, motor running; handle up—brake on, lathe stop.

What a difference! In the higher gears, there is just enough clutch slip for a "soft" start, same for braking. Brake is by vee belt, and "ferocity" can be controlled by adjusting belt tension. When working hard, I can stall the motor but the clutch won't slip. The machine never pops the 1500w circuit breaker, and the cheap battery charger is still going after 18 months hard (semi-commercial) use.

Thread cutting still takes some thinking about; stop lathe, withdraw tool, stop motor, wait until centrifugal start kicks in, reverse motor, start lathe, etc. I usually write myself a sequence to follow until I get in the groove. In over 36 years as a fitter/turner I have rarely found it worthwhile to disengage the feed nut when screwcutting, certainly never on metric threads. Also many modern commercial lathes reverse at 1.5 to 2 times the forward speed, just for this reason, I think.

Should others wish to pursue the air con clutch idea, one came from an Aussie 1978 Ford Fairlane, and the other from a Swedish Saab. The original cover still fits over the changewheels. Workplace Health and Safety rules.



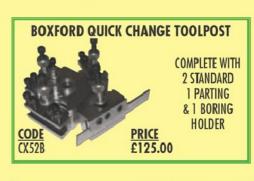




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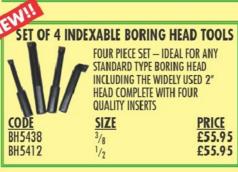




























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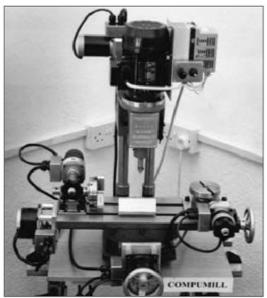
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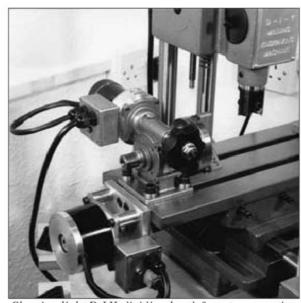




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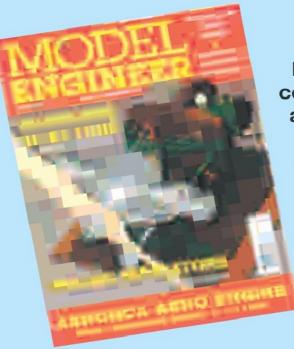
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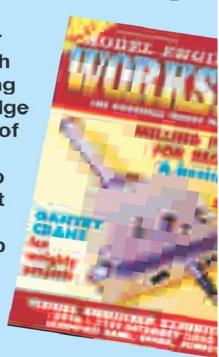
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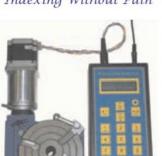
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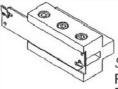
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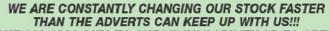
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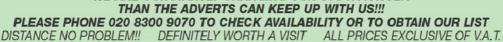
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BOXFORD VM30 vertical bethead 2 speed (short motor) head, R8 powered head, gearbox table, BRIDGEPORT vertical bethead 2 speed (short motor) head, R8 powered head, gearbox table, 42" x 9" table
BOXFORD VM30 vertical bethead 2 speed (short motor) head, R8 powered head, gearbox table, BRIDGEPORT vertical bethead 2 speed (short motor) head, R8 powered head, gearbox table, 42" x 9" table
BOXFORD VM30 vertical variable speed 7 30 INT head, table 211/2 x 6" + Abwood vice and chuck. 21,500 BRIDGEPORT vertical belt head 2 speed (short motor) head, R8 powered head, gearbox table, 42" x 9" table
BOXFORD VM30 vertical variable speed 7 30 INT head, table 211/2 x 6" + Abwood vice and chuck. 21,500 BRIDGEPORT vertical belt head 2 speed (short motor) head, R8 powered head, gearbox table, 42" x 9" table
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BOXFORD VM30 vertical variable speed 7 30 INT head, table 211/2 x 6" + Abwood vice and chuck
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BOXFORD VM30 vertical variable speed 7 30 INT head, table 211/2 x 6" + Abwood vice and chuck. 21,500 BRIDGEPORT vertical bet head 2 speed (short motor) head, R8 powered head, gearbox table, 42" x 9" table

_	urcular – A205	years
	MISCELLANEOUS / FABRICATION MACHINERY	
	HARE MODEL 51T complete with hydraulic indexable table EMI-MEC SPRINT spindles and collets beans 48 direct spares.	smart and brown
	lever compound slides + lever collets, hardinge finger feed coll	letsJust in
	GEORGE ALEXANDER 4MT collet adapter and two collets SWEENEY AND BLOCKAGE NO.2 flypress complete with ball	
	MARLCO notch broaching fixture + notch broach	£425
	CLARKSON drill point grinding attachment for CLARKSON MK1 HARCOS universal head for tool and cutter grinder	& MK 11 grinder
	MYFORD vertical slides just in	£95 / £155
	MYFORD VM-D milling attachment for ML7 and Super 7 lathes BCA 12" horizontal / vertical rotary table	
	QUANTITY of slips, height gauges, squares, straight edges, micr	nometers,cubes, angle plates and
	miscellaeous measuring tools	Just in
	TONGS (a varied selection)	
	FLAMEFAST DS 130 ceramic chip forge	£345
	FLAMEFAST DS 100 hearth MARLCO Broaching Press	
	JONES AIND SHIPMAN 4" x 24" bench centres	very nice example £245
	TOM SENIOR slotting head	£450 ed bandsaw). £950
	DIAMOND fret saw, variable speed	£345
	RJH BT 125 Fretsaw, variable speed SMART AND BROWN / CLARKSON H3-H5 toggle presses	
	ARRAND 2MT long milling spindle	As new £75
	VERDICT CLOCKS, Long/Short Metric and Imperial models FLAMEFAST LD300 Soldering Iron Stove	
	GRANITE 18" x 12" Surface Plate	£140
	VIBIROSHEAR Nibbler	
	TRIUMPH face plate D14	570
	JONES AND SHIPMAN Broaching Press + Stand	Nowe We have just
	ABB Inverter & 1/2 hp motor, wired up	had some Adcock and Shipley New 9750
	WELLSAW hacksaw DUPLEX D29 toolpost grinder BOXFORD (imperial only) thread dial indicator. ABWOOD 6" swivel/tilt machine vice.	2E horizontal mills inAs Is £145
	DUPLEX D29 toolpost grinder	good condition at only
	ABWOOD 6" swivel/tilt machine vice	£295 each + VATEach £345
	VANCO, 1" linisher / vertical + extractor	£495
	BURNERD, LO lever collet chuck + collets	
	VERTEX Dividing head	
	MYFORD ML7 / Super 7 rear tool post	
	MYFORD 254S rear tool post	New £40
	MYFORD Vertical slide / fixed type (copy)	guality equipment New 940
	LOCKWOOD QUAD HEADED 3mt Die Holder	quality equipment New £40
	LOCKWOOD Test Bar / 2mt Boxed	quality equipment New £39
	MAGNETIC chuck - 18" x 6" fine pole	Never used £325
	TOM SENIOR Model E pedestal stand	
	50 INT Tooling; Selection	
	STARTRITE 352 woodworking band saw	
	ALCOSA GF 080/1 Rapid Melting Furnace	
	MYFORD Burnerd Griptru 3 Jaw Chucks	Boxed £225
	COLCHESTER D13 Burnerd 4 Jaw 8" light body independent ch RJH 4" Linisher / Vertical complete with built in extraction	\$625
	MICROMETERS and associated measuring tools	Still packaged as new
	POTTERY WHEELS, kilns and associated equipment	Just In Cheap
	HARRISON L6 metric gearbox	As is £250
	HARRISON L6 tailstock NEW FROM NEW ZEALAND:- Machine vice, 55mm. Jaws pre	£245
	vertical slides and smaller milling machines such as BCA	now with the swivel base£134
	Vice on own	
	Swivel base on own) As new £375
	MITUTOYO grade A set of slips	£245
	F.J. EDWARDS 24" hole cutter	£525
	LINK 1.5 ton vehicle crane + top hat	£625
	MITUTOYO 103-913 metric set micrometers	
	A.IAX 6" hacksaw	9425
	SURFACE plates from 12" x 12" to 36" x 36" WEBER 1 1/2 ton mobil e garage crane, late blue colour	Very nice from £30
	ELLIOTT 1250 STURDIMILL vertical head	One off (rare) £525
	RJH linisher 4" wide belt, pedestal	£345
	STEEL STOCK different stock rolling in almost daily ELLIOT U1 / U2 Slotting Head	
	SWAGE BLOCKS	£125 / £145
	J & S Universal grinding vice	
	SLIPS / GAUGES Metric / Imperial. New Sets: 87 / 81 piece	£215 / £145
	HORIZONTAL METAL BANDSAW 6" x 41/2" capacity COLCHESTER STUDIENT / MASTER Round head, face-plates,	New £170
	QUALTERS AND SMITH 6" Hacksaw	£345
	BORING HEADS 2 / 3 Morse, R8 Taper, Max. Capacity 41/2" rour	nd barNew, each £90
	ODONI Machine Bed Clamps (pair)	Special £24.50
	ELLIOTT 10M Shaper, 10" stroke	£325
	TRANSWAVE 3HP Converter.	
	TRANSWAVE 5.5HP Converter	New £385
	TRANSWAVE MT & RT rotary converters	wford Super 7 Type motor
		Trock Super 7 Type motor
e i	IOINO OUD STOOK EASTED	













2-Axis DRO from

£615

- Made in the UK
- 5 year No-Fault Warranty
- 10 micron Accuracy

Conquest Lathe

NOW INCLUDES TEST CERTIFICATE



VARIABLE SPEED

STANDARD ACCESSORIES

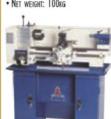
& Delivery

. Q.C.T.P. WITH 3 TOOL HOLDERS



920 Lathe Deluxe

- . SWING OVER BED: 229MM
- · SWING OVER CROSS SLIDE: 133MM
- . DISTANCE RETWEEN CENTERS: 500MM
- . SPINDLE BORE: 19MM
- . TAPER IN SPINDLE NOSE: MT3
- · Motor: 3/HP
- 6 SPEED: 100-1800RPM
- . NET WEIGHT: 100kg



STANDARD EQUIPMENT: • 4" 3-IAW CHUCK

- WITH 2 SETS OF JAWS
- 7" 4-JAW CHUCK WITH REVERSIBLE JAWS
- . STEADY REST . FOLLOW REST
- MT2 DEAD CENTRE • MT3 DEAD CENTRE
- . 4-WAY TOOL POST
- · FACE PLATE
- . Tool Box & Tool Kit
- TRAY & SPLASH GUARD



& Delivery

Model B-Super

- · SWING OVER BED: 420MM
- . DISTANCE BETWEEN CENTERS: 500MM
- . MILL DRILL SPINDLE TAPER: 19MM . TAILSTOCK BARREL TRAVEL: 80MM
- 7 SPEEDS 160-1360RPM
- SWING OVER CROSS SLIDE: 160MM
- SPINDLE TAPER: MT3
- . Draw BAR: MI2
- . CROSS SLIDE TRAVEL: 180MM
- Motor: 3/JHP
- NET WEIGHT: 155KG STANDARD EQUIPMENT
- 4" 3- AW CHUCK
- 2 DEAD CENTRES
- 1/2 DRILL CHUCK



Centurion

- . SWING OVER BED: 420MM - DRAW BAR: MI2 - CROSS SLIDE TRAVEL: 200MM
- . DISTANCE BETWEEN CENTERS: 520MM . MILL DRILL SPINDLE TAPER: MT3
- . TAILSTOCK BARREL TRAVEL: 80MM
- 7 SPEEDS 160-1360RPM
- . Swing over SAIDDLE: 160mm
- SPINDLE TAPER: MT3
- 4" 3-JAW CHUCK • 2 DEAD CENTERS
 - 1/2 DRILL CHUCK
 - CHANGE GEARS

Motor: 2 x ³/.HP

. NET WEIGHT: 230kg

STANDARD EQUIPMENT

- MT3 CHUCK ARBOR

. HIGH/LOW GEARBOX



Champion Mill

- Drilling Capacity: 20mm
 Face Mill Capacity: 25mm
 Face Mill Capacity: 65mm
 Table Size: 150x630mm
 Number of Speeds: 4
 Speed Range: 400-1640rpm
 Spindle Taper: MT3
 Tilting Head: 90° Left & Right



STANDARD **ACCESSORIES**

. I-13mm Drill Chuck & Arbor

Eagle 25 Mill/Drill

- . MILL/DRILL CAPACITY: 25mm TABLE SIZE 190 x 585mm
- . FINE FEED
- . NUMBER OF SPEEDS: 12
- SPEED RANGE: 100-2150RP
- · SPINDLE TAPER: MT3



Price includes VAT & Delivery*



. SPINDLE TRAVEL: 100mm

· MOTOR: THE

STANDARD ACCESSORIES

• 1-13mm Drill Chuck & MT3 Drill Chuck Arbor • Eagle Face MILL CUTTER • T3 TILTING VICE • M12 DRAWBAR • NVR SWITCH GEAR . INTERLOCKED CHUCK GUARD . MANUAL AND PARTS LIST

Eagle 30 Mill/Drill · MOTOR: THP

- . MILL/DRILL CAPACITY: 32MM
- TABLE SIZE 210 x 740mm
- . FINE FEED
- . NUMBER OF SPEEDS: 10
- SPEED RANGE: 80-2300RPM
- . SPINDLE TAPER: MT3
- . SPINDLE TRAVEL: 130MM
- · TILTING HEAD



£899

Price includes VAT & Delivery

STANDARD ACCESSORIES

• 1-13mm Drill Chuck & MT3 Drill Chuck Arbor • Eagle Face MILL CUTTER • VIOO MACHINE VICE • MI2 DRAWBAR • NVR SWITCH GEAR . INTERLOCKED CHUCK GUARD . MANUAL AND PARTS

626 Turret Mill

- . MILLING CAPACITY: 25MM
- . DRILLING CAPACITY: 32MM
- TABLE SIZE 152 x 740mm
- . FINE FEED . NUMBER OF SPEEDS: 9
- SPEED RANGE: 190-2100RPM
- · SPINDLE TAPER: MT3 OR R8
- . TILTING HEAD



& Delivery STANDARD ACCESSORIES

- . DRAWBAR . MANUAL AND PARTS LIST

Craftsman Gap Bed Lathe

- . SPINDLE BORE: 36MM . SPINDLE NOSE TAPER: MTS
- Motor: 11/2 нр
- Netweight 398kg
- STANDARD E OUIPMENT:
- 6" 3-jaw chuck with 2 sets of jaws
- 8" 4-JAW CHUCK . STEADY REST
- FOLLOW REST
- · SPLASH GUARD . THREADING DIAL
- 4-WAY TURRET TOOL POST . 3MT DEAD CENTERS
- T-SLOTTED CROSS SLIDE . HALOGEN WORK LIGHT



£1550

Super LUX Mill

- . MILLING CAPACITY: 25 MM
- . DRILLING CAPACITY: 32MM • TARLE SLITE 240 x 800mm
- . FINE FEED
- . NUMBER OF SPEEDS: 6
- . SPEED RANGE: 95-1600RPM
- . SPINDLE TAPER: MT3 . TILTING HEAD





Price includes VAT & Delivery*

STANDARD FEATURES

- POWERED HEAD ELEVATION
 CAST IRON STAND
- · ANGLE TILTING HEAD · MANUAL AND PARTS LIST

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