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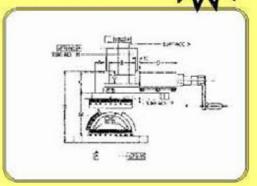
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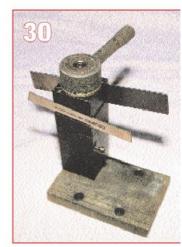


### Front Cover

The chuck fitted to this industrial dividing head is unusual in having both self-centring and T.E. Dominey describes his collection on page 46.













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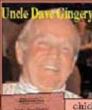
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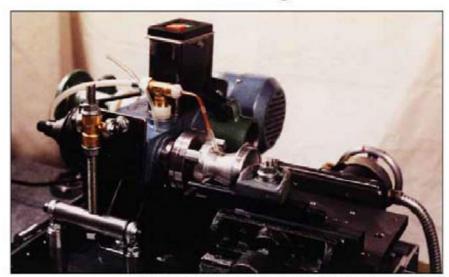
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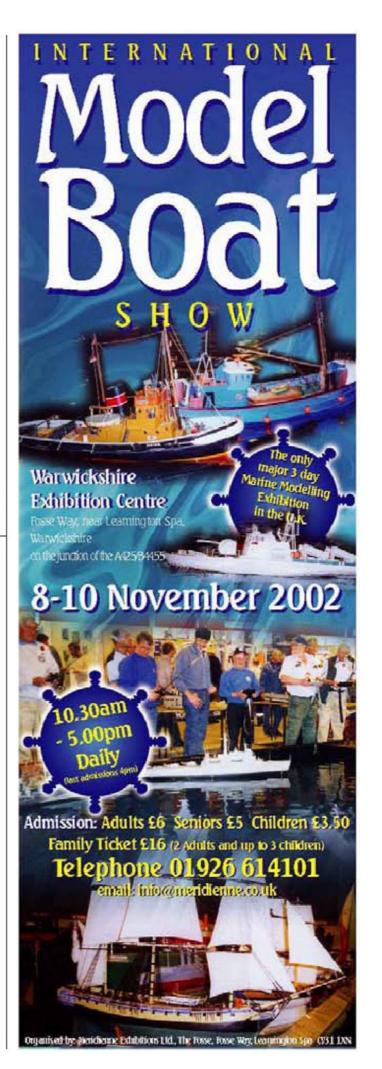
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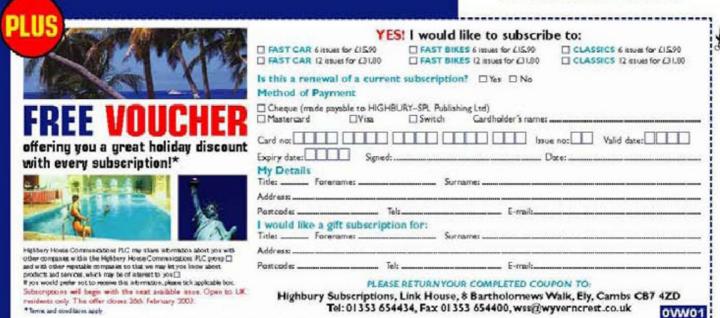
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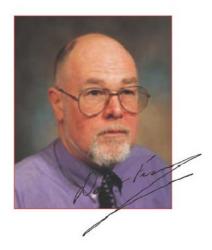
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## International Model Boat Show

Celebrating its fifth anniversary this established event (the only three day show aimed exclusively at marine modellers) promises to be even bigger and better for 2002. Two indoor pools will offer displays by exhibiting clubs, as well as free sailing. The larger pool extends to 1500 square feet, and includes a harbour and other skill testing features.

The exhibition will be held at the Warwickshire Exhibition Centre, conveniently located on the Fosse Way near Leamington Spa, just a few miles from the main motorway network in the Midlands. Ample free car parking, disabled access, and full restaurant facilities are available.

The event will be open from 10am to 5pm (last admissions 4pm Friday 8th to Sunday 10th November, and ticket prices are Adults - £6, Senior Citizens - £5, Children £3-50, Family (2 adults plus up to three children) £16. For further

### Out and about

"Farming Yesteryear" is organised by the Scottish Vintage Tractor and Engine Club and takes place in early September in the grounds of Scone Palace. Although the underlying theme is agricultural, the event is a forum for most historic things mechanical, including steam traction engines, tractors, farm and horticultural machinery, bicycles, motorcycles, cars, commercial vehicles, military vehicles, and stationary engines. On a "workshop" theme, the "portable" sawmill belt driven from a traction engine, produced its own

ON THE EDITOR'S BENCH

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### Variable Speed Drives

Elsewhere in this issue Dr Vassilii Zakharov describes a budget approach to motor speed control using washing machine parts. Inverter drives for three phase machinery are an accepted higher cost alternative, and it was noted in an earlier issue that government incentives aim to encourage the take up of such energy efficient equipment. Not many years ago the market was dominated by two or three names, however thumbing through the pages of one trade magazine revealed that around a dozen manufacturers are now competing in this area. It is to be hoped that this will make such equipment even more accessible since it provides an avenue to power cheap surplus industrial machines from the single phase domestic supply.

### In the workshop

Work on the trailer has moved forward, with the main structure being essentially complete, while the brake mechanism and suspension control are in progress. A 1200lb. hand winch has been obtained, which with its 65 feet of cable should be sufficient since this will allow doubling around a pulley block if ever necessary. It

small mountain of sawdust during demonstrations.

Historically, the weather has almost always been kind to this event, however this year was the exception, with a succession of sharp downpours conspiring to dampen spirits in between the bright intervals. Fortunately the forecast was accurate, and waterproofs had been donned. With something over a thousand individual exhibits, this event can probably challenge the Glamis Extravaganza for the premier title for this ype of event north of the border.



was noticeable that as fabrication work proceeded, the standard of welding improved visibly, a clear case of practice making, if not perfect, at least a few tentative steps in the general direction of the elusive perfection.

On a totally different topic, an acquaintance called by to raise the question of restoring a worn pre-war Wolseley king pin assembly. Examination and measurement showed slight wear on the hardened pin, and rather more on the bushes. At the time of writing he is attempting to track down new replacement parts, however if these prove unobtainable, then it may be a case of lightly grinding the pin diameter, either between centres, or using the Grind All, and then turning up undersize bushes to match.

### **DRO Developments**

This issue includes articles relating to the two extremes of capital spend on such devices. Having some years ago fitted a two axis system to my Beaver Mill, I am well aware of the usual advantages. In addition, my rotary table has become all but redundant except for milling curved surfaces. A number of years ago, Richard Bartlett introduced Compucut, making affordable CNC available to the amateur workshop. Now in conjunction with software developed by Alan Good, he has come up with an ultra low budget system for positional readout, using computer mouse internals.

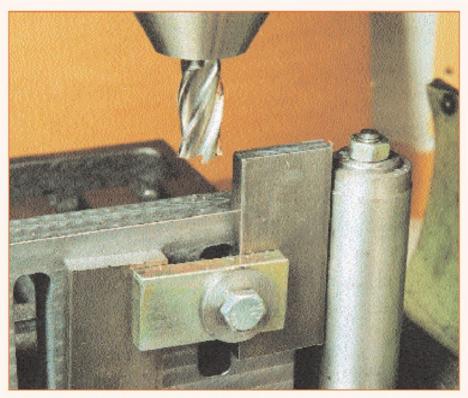
The recent arrival of relatively low cost readout scales of oriental origin has added a further mid range budget twist to matters. Fitted to a typical mill as supplied, they are less than totally convenient, in that one needs to almost prostrate oneself before the machine in order to peer at the smallish figures in awkward places (notably y axis). For additional cost, they can be connected to a remote repeater for more convenient reading.

Also using these scales, one of our local club members, John Curtis, has achieved a similar easy to read result by feeding the outputs of up to four such scales via a multiplexing board to a PC, giving large on screen digits. If scales are fitted to both quill and knee, then a corrected Z figure can be shown. Given that computers are now so cheap, this promises to add convenience to such a setup at relatively little cost

It is hoped to feature an article on John's system, in the not too distant future, however prospective builders will require the production of a programmed chip (this being outwith most amateur capabilities), and as yet, no commercial arrangements have been made for this.

November 2002

# MILLING PROJECTS FOR BEGINNERS (3)



 Machining the first end of the clamp, do machine towards the cylindrical square for added security.

or this the third part of the series we are producing two very simple items, one essential for use on the milling machine, the other almost equally so. The items are clamp bars and parallels.

### The Clamp Bars

It would be tempting in the case of the clamps to cut a few short lengths of steel, drill a hole for the clamp stud, debur, and call it a day. We are in this though for the experience so will aim at a more professional finish and useful result. The dimensions on the drawing are for guidance only as size of machine, may dictate the size made. Do though ensure they are sufficiently robust, if in doubt be cautious and use a thicker material. Eight millimetres thick would seem a sensible minimum for use on all but the lightest milling machine. The slot and hole will of course have to suit the clamping stud size. I have suggested a set of dimensions in Sk.1.

First decide how many are to be made and cut off this number from the bar of material adding 1 to 2mm for final machining. As to quantity I would suggest 6 minimum. This may seem more than is likely to be used at any one time but as we shall see shortly other uses than direct

clamping do frequently occur.

Mount the angle plate and one of the cylindrical squares (as covered in the previous article) and first clamp as in Photo 1, you will need to make a simple clamp with a single hole if you do not have one. Use one of the other clamp pieces as packing for the clamp though it is best practice for the clamp packing to be just higher than the part being held. This I normally achieve by placing a thin piece of card under the part being used as packing. Machine the top face of the part and unless you have a large diameter cutter two passes will be necessary. In all milling operations it is highly desirable to machine towards the supporting items, in this case the cylindrical square. If machining was away from the square, that is from right to left in the photograph, the single clamp may not adequately hold the part. Eagle eyed readers may observe that the clamp stud could be higher in the angle plate slot, ensuring that the clamp held the part nearer the edge being machined for improved security. This though is not the case as I find that using a Tee nut in the slot enables nuts to be tightened without the need for a second spanner, and often a third hand. The T nut does though prevent the screw from being close to the slot end, and I intend to make some special nuts as shown in Sk 2 for use in this way.

In section three of the series, Harold Hall focuses on two simple but essential accessories.

### T nuts, other uses

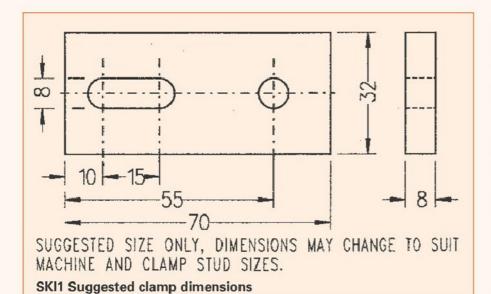
Having trimmed the first end of all the clamps, machine the second in a similar manner, Photo 2. At first this may appear identical to photo 1 but closer examination shows that the part is being supported by a screw screwed into a T nut, illustrating a point made earlier that there are uses for T nuts other than pure clamping. When fitting, turn the screw until it contacts the bottom of the T slot and very lightly tighten. This then supports each part as they are fitted onto the angle plate so that each new part can easily be machined to the same length without recourse to measurement or reading leadscrew dials. A real time saving benefit when a number of identical parts are being made.

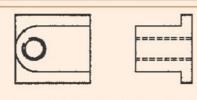
### Secure clamping

Next mark out the parts for drilling the holes and just one with the width and length extremities of the slot to be made. Drill the single hole in each one and use this for securing them to the machine table as in Photo 3. I cannot stress too much to err very much on the safe side when it comes to securing parts for machining, one too many a clamp is very much better than one to few. With that in mind, placing support pieces, which do not actually grip the part, but prevent sideways movement, will give added security, often in places when an additional direct clamp cannot be applied, as will be seen through the series. They may also function as positioning stops when multiple components are being handled.

In this case a single screw fixing would probably suffice, especially as it is a slot being produced that will not tend to place any side load on the item. The support pieces in the photo do though perform a very important additional function. Mount first the clamp that had the slot positions marked onto it and position it using an engineers square of the front face of the machine table. Clamp it in place using the single screw then add the two support pieces as shown in the photograph. As you become more involved in milling machine activities such additional aids to completing the task will become necessary, so do make a habit of keeping these bits and pieces handy for possible future use. Of course the clamps now being made could perform this task for future operations, hence my comment

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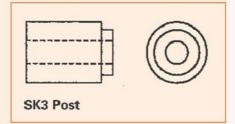


WHEN USING A T NUT WITH THE FACE PLATE OR ANGLE PLATE, NUTS MADE AS PER THE ABOVE FORM WILL ENABLE BETTER USE OF THE SLOTS TO BE MADE

SK2 Modified T nut

regarding making a sufficient number.

Fit a slot drill of a size that will cut the slot at one pass. If however a sufficiently wide slot drill is not available, then widen the slot with a second pass. (For this, I prefer to use an end mill rather than a slot drill, as I feel that the former may be more robust when cutting on one side only.) With the machine stationary lower the cutter so it is almost touching the workpiece. Then, with the cutting edges in line with the cross travel use the cross



feed to align the cutter with the marks on the workpiece, lock the cross feed in this position. Now rotate the cutter ninety degrees and traverse the table until the cutting edge lines up with the end mark and set the first table stop (bottom photograph 3) at this point. Knowing the cutter, set the second table stop with the gap required, and traverse the table to check against the other end mark on the

useful for setting the second stop, distance gauges, a drill or bar of suitable diameter, each of which may be augmented by feeler gauges for fine adjustment. In each case check with micrometer.

Start the machine and plunge the cutter into the workpiece, say by 1mm, (or more if yours is a heavier machine), and make the first cut. Slot drills can be used in either direction, so plunge the cutter by a further 1mm and take a cut in the reverse direction. Continue until the slot breaks through on the other side. As the slot aligns with the T slot there is no danger of the cutter damaging the table surface. The positioning pieces on the table, and the end stops having been set, will make the repeat machining of the remaining clamps very straight forward.

You may consider that the single hole in the clamp is purely for this machining operation but we shall see later in the series that it has a very important role to play. Generously debur all edges and the clamps are complete.

### **Parallels**

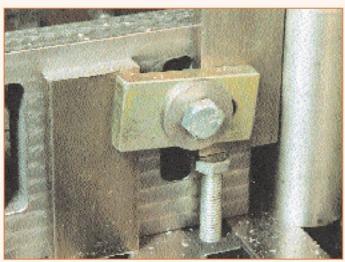
Almost as essential as the clamps above are a set of parallels for use during milling operations. These could be commercially made items, ones made by the user, or, as so often is the case, just off-cuts from mild steel bar. Whilst in many cases the latter may be adequate, especially when used as a single parallel, two pieces of bar, especially if taken from different bars, may not be sufficiently identical. On the other hand the hardened and ground commercial variety will be of an accuracy rarely required and be a little on the expensive side. Of more significance though with these is that they will not be available in a sufficiently wide range of heights, especially if the cost is a consideration. Making your own is therefore a worthwhile option as the cost will be minimal and a wide range of sizes will present no problem.

### Parallel, How?

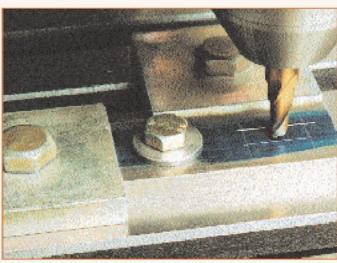
The aim will be to create parallels in pairs that are both parallel along their length and of exactly the same height, at least within good home workshop standards,

length of the slot, and the diameter of the clamp. Various techniques may be found

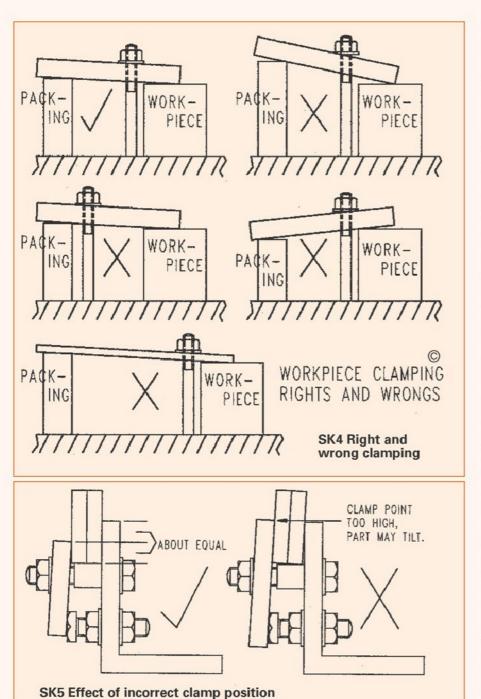
2. The positioning screw below the clamp piece enables all the clamps to be easily machined to the same length when machining the second end.



3. With the clamp having been marked with the position of the slot, setting the table stops for machining the slot in the first and remaining clamps is easy.



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4. Posts fitted to the angle plate and lightly machined on top enable parallels to be positioned and machined to a fair degree of accuracy.

say within 0.02mm. At first sight this may appear a standard that is too close to be achieved, especially with regard to being parallel. How, after machining the first side, is the parallel positioned accurately enough for the second to be machined parallel to the first? This is the secret behind the method proposed.

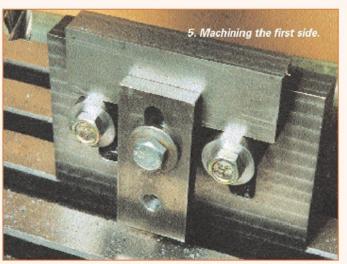
The heights of the parallels are not critical providing each pair are accurately the same, I would suggest nominal values of 10mm, 15mm, 20mm, 30mm, 40mm and 50mm. and say 8mm thick and 100mm long. Having cut your lengths of material, in various widths, machine the ends using the same setup as illustrated in photo 1 and generously debur the ends. Also remove any blemishes along the long faces and edges that affect the mounting of the pieces for machining.

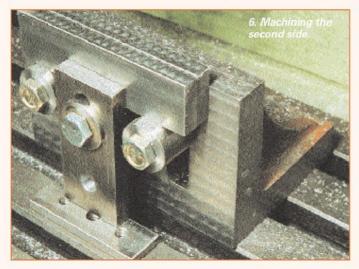
Make two posts as Sk. 3, as you will see

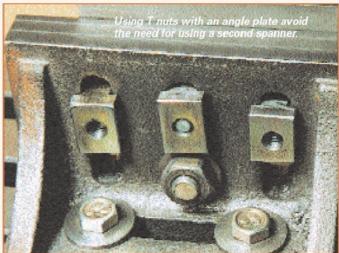
the dimensions are not that critical, and mount these onto the angle plate at approximately the same height, see Photo 4. Machine very lightly over the top surface of the posts to give two locating faces for the parallels to sit on. The small reduced end to the post avoids having to machine too close to the angle plate face. It will be necessary to mount the posts nearer the top of the angle plate for the smaller sizes, say 10,15 and 20, then remount lower down and re-machine them for the larger ones. The screw seen in the centre slot acts as packing for the clamp when holding the parallels as in Photo 5. This should be set at a height just greater than the thickness of the two parallels, say plus 0.5mm. This would seem to be a good time to examine good practice in terms of clamping and rather than go into lengthy verbal description, Sk.4 should largely illustrate the do's and don'ts. Note that in this case, if the clamp is not positioned suitably the parallels may tilt as shown in Sk. 5. with obvious consequences on height accuracy.

With the first pair of parallels mounted machine the first side, remove and very lightly debur edges and ends. Turn over, and once more fit in place making sure that the mounting surfaces are scrupulously clean. Machine the second side, **Photo 6**, the piece of packing seen added below the clamp holds this at just the right height. Finally, remove, debur, and the first pair of parallels are finished.









**Photo 7** shows the use of T nuts with the angle plate as mentioned earlier. This avoids the need to use two spanners and frees a hand to help elsewhere.

These parallels not being hard will be susceptible to damage on their edges, though if treated accordingly this should easily be avoided, a small wooden tray with separators would help at the storage stage. In any case any damage is likely to be local and can easily be removed with a file without effecting their overall accuracy. Of course if you have access to more advanced facilities, you may be able to have your parallels case hardened and then trued up on a surface grinder. However that falls outwith the scope of the present discussion.

This now completes the basic kit shown in Photo 8 and as the series progresses it will be seen to be adequate for completing some sizeable projects without further equipment. In the next section, we commence the construction of a boring head, the first of three substantial projects that bring the series to a conclusion. Even though the projects are quite sizeable the individual machining operations are mostly no more complex than those already met. The projects should therefore not present any major problem, even for the novice, but provide sufficient milling involvement to ensure that the newcomer would be well at home with the machine by the time the series is complete.



8. With the basic kit now complete we are ready for some advanced projects.

# INK UP

Would readers wishing to make use of this facility please note that the maximum total value of items accepted for a 'For Sale' entry is £50.

To advertise goods of a greater value, please contact our Classified Advertisement Department. Please indicate clearly if an item is intended for Link Up.

### FOR SALE

- MEM electric motor starter, for use on single phase, 240 volt coil and No Volt release. Reversing switch with wiring diagram. Both suitable for Myford or Boxford lathes or similar machinery. £30-00 the pair plus carriage, would split. Please contact Mr. J. E. Fletcher on 01723 362 537
- For Sale Picador Pulleys 4in, and 10in, with two S/A BB Plummer Blocks with bolts, collars, and washers £20-00 Please phone Mr G. R. Hughes on 02392 737 365 (Hants)
- For Sale Hemingway Knurling Tool kit £25-00. Dremel 210 drill stand (928 series tool) £10-00. Please phone Mr D. Pickup on 01373 832 681

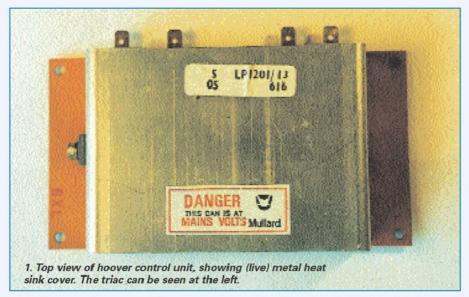
### WANTED

- Wanted instructions for construction and use of Dore Westbury Milling Machine Kit by Model Engineering Services. Will reimburse all costs. Also wanted, Acorn/ Ajax vice for Acorn/ Ajax 7in. shaping machine. Please phone Mr D. Pickup on 01373 832 681
- Wanted a mains electric motor not less than one sixth H.P. with an integral reduction gear -OR - a pair of spur gears to make a 10:1 reduction gear (similar to Myford gears) Please Phone Mr P.A. Twist on 01962 880 475
- Wanted copy of manual for Adcock and shipley Milling Machine model OEG. Please contact Warren Green, 15 McDonald Road Papatoetoe 1701, New Zealand, or e-mail greenest@ihug.co.nz All expenses reimbursed.
- Wanted help. I have recently purchased a small bench filing machine made by the Oliver Instrument Co.

- Adrian, Michigan, U.S.A. Several parts are missing. Any information, manuals etc would be most helpful. Costs of photocopying etc will be gladly reimbursed. Please contact Stephen Tresidder, 17 Station Rd, Carnhell Green, Cambourne, Cornwall, TR14 0LY
- Wanted Information. Does anyone recognise the homebuilt lathe (see photo). I bought it from a friend a couple of years ago, and he had purchased it at a workshop clear out. I'd like to know who designed it. Please contact Kevin Quiney email: kcqup2u@ukf.net



# MOTOR SPEED CONTROL

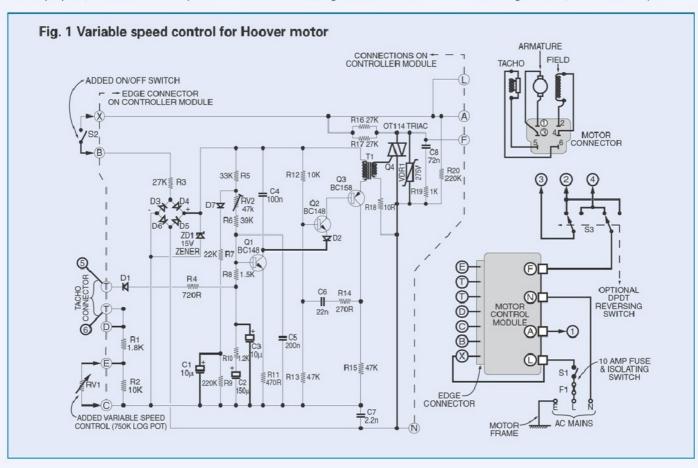


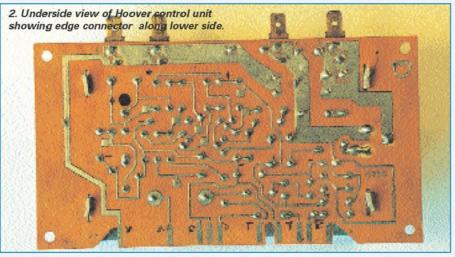
n the correspondence of the Aug./Sept. 1997 edition of MEW, the question of speed control of AC motors was discussed, and a particularly helpful suggestion was made to use discarded washing machine motors for the purpose, with an electronic speed

control based on the TDA 2086A phasecontrol chip. Unfortunately, with the cessation of Plessey semiconductor production (a very sad event indeed) this chip is no longer available at any reasonable price. On the other hand, the basic idea of using a series-wound Vasilii Zakharov suggests a low cost approach to variable speed control which can be applied to many typical amateur size workshop machines.

washing machine motor for driving a small lathe or other machinery requiring say 1-2 HP is still an excellent one, because the incorporation in the motor units of a tachometer allows electronic control of speed over a very wide range indeed (without gearing, 100 to 10,000 rpm is typical) with only marginal loss of torque over the whole range, and with tolerably good speed stability for varying loads. Moreover, such motors are usually very inexpensive, or even available at no cost at all, and they run off single-phase AC mains.

The purpose of this brief article is to suggest that a simple, even trivial, solution exists to the problem of electronic control, even less expensive than the original TDA 2086A option. This is to use not only the motor but also the control unit from the washing machine, and then modify it





appropriately. The modifications are simply to add a rotary potentiometer with on/off switch, a reversing switch, if needed, housing the electronics and switches in a tough (preferably plastic) box, and making the necessary interconnections.

The author has in fact implemented speed-controlled motor drives based on parts from two different washing machines, Hotpoint and Hoover. It was discovered that the motors, connectors and tachos differed only in minor detail and construction, and so also for the control units; for example, the particular Hotpoint circuit seemed to be marginally superior in having a 'slow-start' feature, while the Hoover motor was the more substantial. The motor mounting arrangement and pulley were also remarkably similar. There is no reason to suppose that other washing machines have anything much different in them by way of motor drive.

Just as an illustration, Fig. 1 shows the circuit of the (simpler) Hoover control unit, together with the added speed-control potentiometer, on/off switch, and reversing switch. All the letter and numeral symbols at terminal points are as original (e.g. the tacho is connected to terminals (5) and (6) on the motor connector). The reversing switch simply reverses the polarity of the field winding in relation to the armature brushes. It is MOST important that the reversing switch is not operated whilst the motor is powered on, so a mechanical or electronic safety interlock is essential. The

usual warning about reverse running of lathes etc. of course applies. The on/off switch can obviously be quite separate from the speed-control potentiometer, but having a rotary potentiometer with a combined switch does have the added advantage that switching on or off then occurs at minimum speed.

For anyone searching for the control box in such a washing machine, just follow the wiring from the motor connector to the (nearby) control unit. In the author's example, this was a unit with edge connector (convenient!) about 10 x 8 x3 cm.. Be careful: the metal cooling cover acts as a heat-sink for the Triac switch, and this not only gets hot during operation, but is LIVE to the AC mains. Hence the advice to house the control electronics in a plastic box, and also, incidentally, to leave some holes for ventilation. Photos 1 and 2 show the control box, from above and below, the edge connector being clearly visible in the latter.

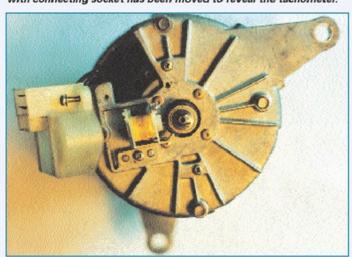
Concerning the tachometer, the Hoover version of which is shown in **Photo 3**, the actual physical construction does vary from one machine to another, as does the number of poles and the magnet arrangement. So, although by no means impossible, it is not advised to use a motor from one machine with a control unit from another. Do not alter the tacho setting unless you know what you are doing!

It is possible in principle to build a control circuit for any of these motors by using ordinary electronic components available from suppliers and copying the circuit I have shown, rather than using the washing machine control unit. But care should then be taken to include the various safety features and measures to minimise electrical interference, for example the 'snubber' network. Whatever the control circuit, it is strongly recommended to use an EMC filter between the AC mains and the control unit with motor; this is what the washing-machine makers do anyway. Otherwise there will be electrical interference from the unit to other electrical equipment (such as radios and TV sets) along the mains wiring. Notice that, in addition to the on/off switch on the control unit, I have also shown a separate mains isolating switch and 10 Amp. fuse. This is a standard wall-mounted unit, and is usual practice.

It was not intended here to go into any detail about circuit operation and so forth. Rather the purpose was to describe an easily copied and practical 'black-box' solution to the problem of speed control for readily available motors, and a solution particularly for those who are perhaps not well versed in electronics. For those readers who are interested, I can perhaps mention that the basic scheme used for control is with closed servo feedback loop. The tacho generates a signal proportional to actual motor speed, and this is converted to a voltage which is compared with a reference voltage representing the desired speed. The difference between the two determines the fraction of each half cycle of the AC mains during which the triac is switched on (the socalled firing angle). The circuit operates so as to keep the speed constant regardless of load, although change in speed by changing the setting of the control potentiometer does take a few seconds because of the timeconstants of various circuit elements. When first switching on, there is some intentional delay in coming up to speed.

It took some time to go through the tedious work of tracing out the control circuits, and understanding how all the circuit features work. But all this is now done, and the end result has been most rewarding. For no cost at all to the author (except time!) he has several motors whose speed can be controlled from 10 to 1000 rpm (when using 10:1 reduction gearing) at the turn of a single knob. Moreover, the necessity of designing and making a printed circuit board has been entirely avoided. It is to be hoped that other readers will gain the same benefit. After all, there are plenty of scrap washing machines about!

3. End view of Hoover motor showing tachometer. The plastic cover with connecting socket has been moved to reveal the tachometer.



4. Hotpoint motor, clearly showing the tachometer mounted at the end of the spindle, and also the connecting socket.



# SIMPLE TOOLS -SIMPLE METHODS or Hand tools for beginners



1. A selection of small chisels.

ust lately I have had to re-think my model engineering activities, not just re-think but finish. Since moving to a small flat our furnishings and belongings have had to shrink. Having thought long and hard about possibilities, I have decided to stop. It is a question of room: the sitting room and bedroom are non starters for obvious reasons. So is the kitchen, Pauline has hardly enough room to cook. That leaves the bathroom and I toyed with the idea of a board over the bath which I could put the Unimat on. Having thought through all the implications, I abandoned that idea.

During a conversation with our editor,

he suggested that I ought to make myself useful by writing something aimed at beginners. I thought that a look at some of the simple hand tools we use would be a good start, as the basic cutting tools are often undervalued and overlooked. If you do not have access to a heavy duty machine shop, then much metal removal can be accomplished quite efficiently by the thoughtful application of hand tools.

### Chisels

You cannot get more basic than a chisel. You may choose to think of it as the foundation upon which most metal cutting technology has been built. The shape of the cutting edge and the arrangement of rake and clearance angles are common to most other cutting tools. In a sense, a turning tool is little more than a stationary chisel, presented accurately to a moving workpiece, a flycutter may be thought of as a sort of rotating chisel, and a multi-tooth cutter just a series of chisels. What comes to mind when chisels are mentioned is not always too accurate. The immediate mental picture is of a lump of hardened steel which has to be clouted with a big hammer. This is certainly not always the case, two of my most useful ones are quite small and only need a 4oz. hammer. Consider also the precision work undertaken by master gunsmiths chiselling out fine decoration. Photo 1. shows some I use, from left to right, a home-made one from an old file, a very light duty one ground from a %in. tool bit, my favourite one, 4in. long with a 1/4in. blade width and the last one, bought for me by my son, a Japanese one with a cutting angle rather on the acute side, useful for soft materials and with a lovely comfy handle. Photos 2,3, and 4 show the favourite one being

Bob Loader describes some very basic techniques, - oft forgotten but nevertheless extremely useful.

used. Photos 2 and 3 show it at its most useful, where there is an amount of metal to remove which would be very hard work with a file, but too little to saw off, just that awkward size. Making hacksaw cuts to the depth needed, leaving a little for finishing, will let the chisel do all the hard work.

The best metals for chiselling are the brittle ones, like cast iron, cast bronze, cast aluminium alloys and hard brass. Most steels will chisel reasonably well but the tougher ones will need a bigger hammer. Thinner metals can be cut nicely in a vice as in Photo. 4. where the flat area of the vice jaw acts as a guide and keeps the cut level. Large jobs in thin materials can be done by putting the work over a piece of wood and following a marked line, leaving a bit for finishing. Keep the edges sharp by grinding them to an angle of about 60 -70 degrees with a slight radius. Keep the head chamfered, it should never look like a bunch of flowers. There are different shapes of chisel for special jobs but for model engineering, flat ones are the most

## Safety considerations when using a chisel

There are three main sources of danger when using chisels. Always wear goggles or safety spectacles. Small chips will fly about and using Vaseline as in photo.3. is

2. Chiselling the waste off a broad surface



3. Chiselling off a narrow surface, a smear of Vaseline helps stop the bits flying about.



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4. Using a chisel against the vice jaw to cut a thin metal. Photo by Pauline Loader.



5. Preparing the job in photo.3. by hacksawing grooves ready for chiselling.



6. Blades for three different saws.

not always the answer. A much used chisel will gradually develop a mushroom head with split edges. Pieces of these can fracture away at high velocity, so keep the head of the chisel neatly chamfered by filing or grinding when it starts to spread. Use a chisel guard if you have to do a lot. It is a circular piece of hard rubber which can be squeezed on to the chisel shank. When you miss the chisel head, it saves you from clouting your fingers. If there is the slightest chance of anyone else being hit by bits of metal, rig up a guard or curtain to keep them safe.

### Saws

### Hacksaw

As well as the normal jobs which need sawing, there are some which a hacksaw is specially good at. It can be a very good roughing out tool and also a short cut in many jobs. For instance, the piece of cast iron being sawn in **photo.5**. is being prepared for the chiselling shown in photo.3. It saves time and trouble.

A hacksaw frame with several blades of different pitches will cover most of the cutting you will need to do.

In photo.6 the top blade is one for a hacksaw and is suitable for most cutting jobs. Look for the magic words, 'high speed steel' or the letters HSS, it may not be flexible but if it is used correctly, that is not too important, I've shown this blade because it shows the number of teeth per inch and also the direction of cut, the big black arrow. What S D means I have no idea. You should have another two blades, one with 24 teeth and one with 32 teeth. then you can follow the rule, - soft and thick materials - coarse blade, - hard and thin ones - fine blade. You will not go far wrong if you remember this. The other blades are one for a junior saw and the bottom one for a coping saw, more about those later.

A useful addition to the hacksawing tackle is a few tension files like those in **photo.7**. The two in the middle fit in the saw frame with the clips shown. The one with the spring clip is the easiest to fit, the other one is a bit of a fiddle. The files are coded, red for coarse, yellow for medium and the coloured bit goes to the handle end. Better still is the one on the left, it is a tungsten carbide one which is unidirectional, no clips, no fiddle and according to the label, will cut anything. It is called a rod saw and I bought it in

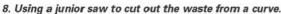


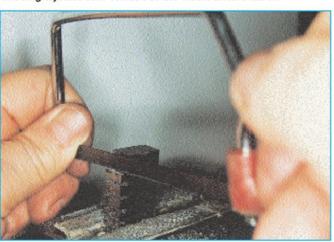
A rod saw and two tension files with the clips used in the hacksaw frame.

America, if it is available in this country, buy one, it is excellent.

### Junior saw

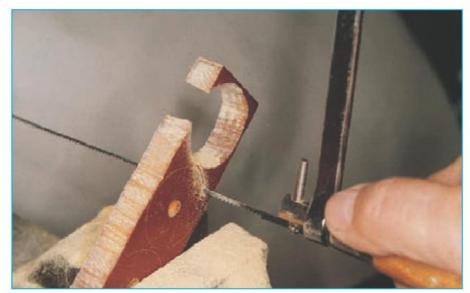
As the name suggests, it is a smaller version of a hacksaw with a finer pitch blade which is hard only on the teeth, so it is easier to bend and wears out quicker. There is a variety of frames, from the simplest- a piece of ½ in. mild steel bent to shape, to some more special ones which are more comfortable to use. Photos. 8 and 9 show one of each type. They are very good at cutting shallow curves, photo.8. because the blade will follow the



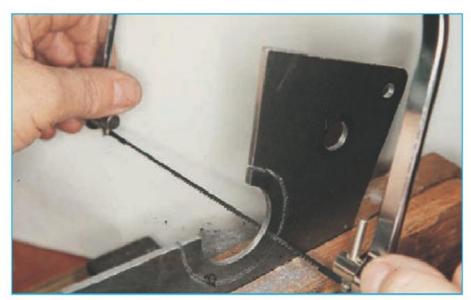


9. A junior saw used for accuracy.





10. A typical use for a coping saw. Photo.by Pauline Loader.



11. The thinnest material a coping saw will manage because of the tooth pitch.

curve, especially if the work has been cut down to the marked line first, leaving the bits in between to be cut. Another use, photo.9. is where the cutting must be very carefully done. The job was to rough out the slots in a four jawed chuck body. The 'feel' is better than a hacksaw and there is less chance of the blade jumping about. So the junior saw is good for accurate work and the smaller jobs.

## Points to remember when sawing

- 1. Keep the sawing speed down, for most materials about 60 to 80 strokes per minute is right, the timing of the radio time signal is a guide.
- 2. The man who made the saw blade put teeth all the way along, use all of them.
- 3. Cutting pressure should be only enough to make the teeth cut and they cut going forward.
- 4. If you use the saw like a scrubbing brush, you will break a lot of teeth and the blade will not last and one day it will be the last blade in your box, but you will only find out when you have broken it.
- 5. When starting a hacksaw cut, file a small nick for the blade to drop in. It will save your fingers and finger nails having lumps cut out of them
- 6. When sawing to a line, especially on thin materials, cut along the widest side as in **photo.13**. it will let you sight along the line and make sure that there are more than 3 or 4 teeth in contact.
- 7. Do not cut thin materials vertically, it will encourage the saw to wander and perhaps break teeth.
- 8. When putting a blade in the saw frame, take up the slack and give the adjusting nut another three full turns, that should be enough tension.
- 9. The same applies to tension files. Be careful not to saw too quickly with them, they get hot very quickly; for the same reason avoid too much pressure.



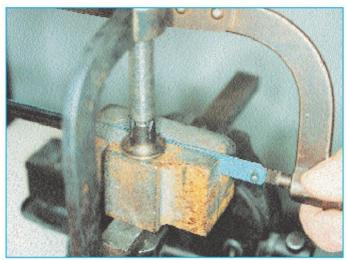
13. Sawing along a line instead of vertically is best for thin work.

12. The thin blade of a coping saw will get into awkward places.



14. Hacksawing a large block can be hard work.





15. Changing the sawing direction several times will make the job easier, note that when the work is too big for the vice there is a remedy.



16. Roughing out a large turning workpiece with a hacksaw.

### Coping saw

This one has a deep frame and a narrow blade which can be set to any angle. They are very good for jobs like the one in **photo.10** where several discs are being cut from a tufnol blank. They will cut most materials and are better on the thicker ones because of the coarse teeth, the work in **photo.11** is about the limit for thin work. With the blade angled as in **photo.12** it is a good tool for getting into restricted spaces.

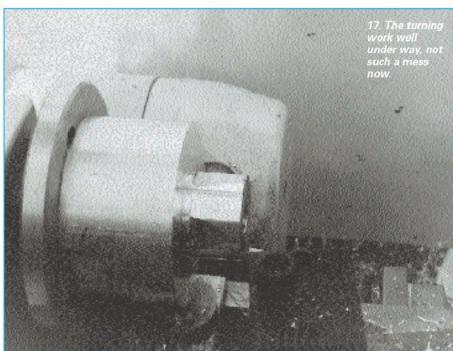
### **Short cuts**

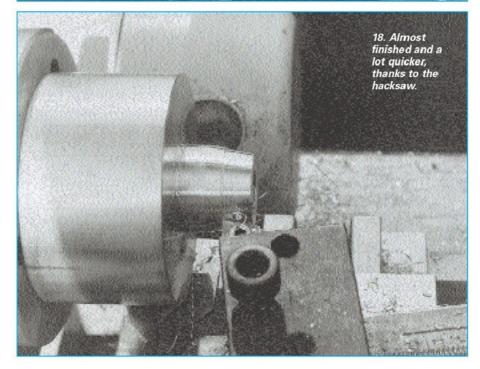
A hacksaw is ideal for shifting a lot of material fairly quickly. If, like me, your machining equipment is limited, a lot of roughing out can be made easier by hacksawing as in **photo**. 14 where a cast iron block is being reduced to a manageable size. The technique is to cut down to about the blade depth, then move it 90deg. and do the same again. Keep moving it and you will always be cutting along a manageable length. To use a small vice which will not open enough to hold the block end wise, put a bar into the vice and clamp the block to the bar, **photo**.15. It is a solution I have had to use for larger work.

The same sort of roughing out can be used for some turning work where a lot of material must be machined off. Using a hacksaw can be quicker than turning for the roughing out, although it does not look too clever, photo.16. But by the time it has been turned a bit, photo.17 it looks a bit better and when almost finished, photo.18, it has cleaned up a treat and looks as if it could have been turned from the start. In this case the method adopted saved a lot of time and machining, to say nothing of swarf.

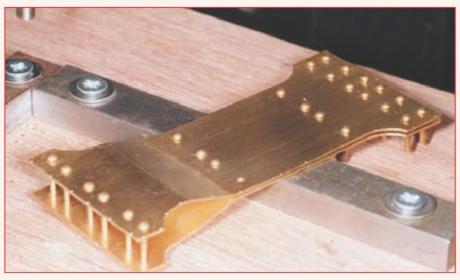
### Next issue

In the second part, I shall offer a few words on the subject of files, again simple tools, again frequently undervalued and overlooked.





# A TALE OF TWO READ-OUTS (2)



1. Repeatability of positioning is proved by the insertion of rivets in these loco. step parts

### Minor Limitations

Although I chose the Newall system as best suited to my requirements, there are many others out there vying for your attention and pocket money, and you might have bigger machines than mine, without the space restrictions. Which would extend your choice of system considerably, of course, and you might well decide on another variety. Whatever the actual system you choose, what it can do remains pretty much the same as long as we stay in the realms of the "professional" equipment. Almost pretty much the same, though you do need to check each one out in some detail before stumping up the monies. As an example, the Newall system that I have has to my mind two limitations - it won't take an input from an electrical edge finder, and it doesn't remember it's position when powered down. This hasn't actually caused me any problems, but they may be important to you. The power-off could be a nuisance, as I live in a sort of rural area fed by overhead lines, so power failures are by no means unknown. In fact we had one whilst I was writing this, and the mill DRO's lights went out. It was set up for a part-completed job, but disaster didn't follow since

a) it would be relatively simple if a trifle inconvenient to re-locate the reference point on the workpiece, but b) whenever the DRO is aligned for a locate the locate the sides to the

job I always return the slides to the reference (0,0) position when I pack up - that way I only have to press two zero buttons to set it up again. Anyway, back to the job in hand - how does it perform, and what will it do?

To answer the second question first – nothing that you can't do with the feedscrew dials, and in one particular case a lot of calculation. What it will do is do the same thing but do it more conveniently, more quickly, more accurately and more repeatably. If they don't matter to you, don't waste your money. If they do, then you have my permission to start drooling!

It goes without saying that having got the systems up and running, I was somewhat impatient to cut metal and find out exactly what I'd spent my money on. And if it had been worth it!

### **Initial Efforts**

The mill system was up and running first, so the natural thing was to use that to make the mounting components for the lathe system, eight in total, plus some precision drilling of the cross slide. You'll have to believe me on that for the time being, the drawings are in the next part of the article. Suffice it to say that a lot of holes had to be drilled, some accurate milling was required, and it all had to fit together and on to the lathe. OK, so some of it could have been less accurately done, but I wanted to test out the system. So I went for accuracy, and didn't resort to clamping things together to drill aligning holes, each component was drilled and milled individually. And it all fitted together to perfection. Very impressive indeed, and if that wasn't enough, it was easy to achieve. Yup, it was worth it. Definitely.

Even more impressive was the manufacture of the rear footsteps for my locomotive. These are shown in **photo 1**, and each was drilled individually with 28

## Barry Harrison continues by examining the operation and advantages of DRO systems.

- %6" diameter holes for the rivets – no marking out for the holes, nothing, just location on the mill table against the two bars on the table, each clocked true to the respective mill axis. The DRO was zeroed in using the edge finder visible in the photograph, a George Thomas design most kindly made and given to me by Alan Hopwood of the York Society.

After drilling the first plate the DRO was 'scrambled' and re-aligned with the bars using the edge finder, the second plate then being drilled. When the plates had been drilled and were still in the flat, 27 rivets could be pushed through the back-to-back plates, and the one that couldn't was because I'd become careless and had suffered a wandering drill. Mea culpa, and it serves well to illustrate the point that the performance of these systems cannot exceed that of the operator. There are 20 rivets through the plates in the photograph.

Still on drilling holes, the case mentioned above requiring calculation involves the positioning of any number of holes on a particular and exact pitch circle diameter. Want a prime number division plate way outside the range of the ones you already have? No problem, although some makes of readout place a fairly low limit on the number of holes. Locate the spindle at some convenient point on the job, of known dimension from the centre of the pitch circle. Press a few buttons to tell the DRO where it is and where you want to start drilling, press another to select the bolt hole circle option, and a few more to tell it how many holes you want to drill. Press another button to tell it you're going for hole 1, and the display changes to apparently random numbers. But wind the feedscrews until the both axes read zero and you'll be in position for hole 1. Then press for hole 2, move the slides until both axes again read zero, and you're in position for the second hole. Ad infinitum ad nauseum, until you've drilled all the required holes. It's as simple as that, and accurate and repeatable. So you can confidently drill say the holes in the two ends of each of two cylinders, then drill the four covers. and they'll be totally interchangeable as long as you didn't let the drill wander when starting, of course, and do the original location relative to the bore accurately enough. No marking out, no drilling two together, no spotting through, just perfectly positioned holes.

A most useful facility is the ability to locate anything relative to anything else. If you want to dimension say a set of holes from an edge of the job, that's ok. If you want them located relative to centre line, that's ok as well, just zero the DRO at the relevant position. Most systems offer several ways of doing this, the most obvious is as described above for the footstep backplates. In fact, they were located from the centre lines of the plates. With the DRO zeroed against one of the bars (it could equally have been against an edge of the work piece) simply measure the width of the job, divide by two and enter this value as an offset into the read out with a few keystrokes, wind to zero and you're there, on centre line. Alternatively, if you don't know, or can't measure, the width of the job, use an edge finder on one side of the job, zero, move to the other side and again use the edge finder to locate that one. Then tell the DRO you want to go mid-way between the two, and it'll take you there, probably to greater accuracy than you could have achieved by measuring the width of the job.

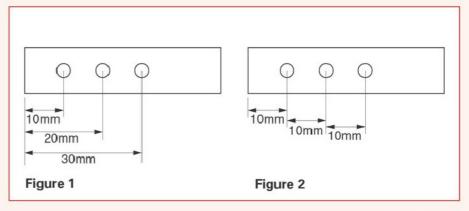
Or the diameter of the job, if you're drilling cross holes through a round bar. No need for drilling jigs and bushes to suit the many work and drill diameters you might want to use, so there's an enormous saving in time if you need to do much of this sort of thing, and every hole will come out on centre line, as long as you exercise a bit of care in starting the drill. And for the rare (!) occasions where you want a hole deliberately off centre by an exact distance, a DRO system can sort that for you as well... as long as you can get the drill to start drilling, of course!

The foregoing examples should serve to illustrate the uses of a DRO on a vertical milling machine, and even though I've only looked at drilling holes it should be apparent how they can be used when milling. Or a combination of milling and drilling, the DRO doesn't care what you're up to, or what tool's in the chuck, it just knows exactly where the spindle centre line is relative to where you zeroed it. So you can cut a slot a precise distance from an edge and an exact depth from the top surface, do any other milling you might need, then drill holes anywhere you like. In the exact centre of the slot, offset to one side, somewhere else. It doesn't matter, the DRO will guide you to the right position, and do it without need for any addition/subtraction on your part.

### Absolute or incremental

Which brings us to another useful feature, the ability to work in either absolute or incremental dimensions, or both simultaneously. I suppose that should really be alternately, but you'll see what I mean. The 'normal' operating mode is absolute dimensioning, as shown in the first simple (one axis) drawing (Figure 1) – all dimensions are taken from the left hand edge.

Figure 2 the same component, but



dimensioned incrementally – each hole is dimensioned from the adjacent edge or hole.

As we all know, many engineering drawings that we work to use a mixture of absolute and incremental dimensioning, and we also know that it can be a real pain to convert dimensions on the drawing to dimensions on the job, with much addition and subtraction being needed, each one bringing with it the possibility of mental error – or digit difficulty if you're using one of those new fangled electronic calculator things.

Most DRO systems can work with either system, and you can jump around from one to t'other without any difficulty. Take for example drilling loco frames. The pattern of holes for the horn blocks might be repeated at axle centre spacing. If the holes are dimensioned relative to a pattern reference point, then it becomes very easy to move to the new absolute reference point, switch to incremental, and proceed with the pattern.

So you work alternately in absolute and incremental dimensions, but the DRO does it simultaneously, always remembering where the zero point for the absolute measurement is located. This is most convenient.

### And so to the lathe

So here I am, absolutely (or should that be incrementally?) delighted with the mill system, what about the one for the lathe? Would you believe instant disappointment? Naturally the first thing that I checked on the lathe was how well the DRO agreed with the feedscrew dials. Great along the bed, unbelievably out for the cross slide movement. Damned idiot, Harrison, you forget to switch to radius mode! One needs to remember that the feedscrew dials on the Myford (but not necessarily on other machines) effectively read radius; if you move the dial by ten thou, that's ten thou off radius, twenty thou off diameter. The Newall DRO defaults to diameter mode unless you tell it otherwise, so it was reading twice the movement indicated by the dial - for my ten thou dial movement it was telling me that the diameter would reduce by twenty thou. Right, that's sorted, and a lesson learnt: When all else fails, READ INSTRUCTION BOOK!

The second trial was to turn repeatedly to 0.750in. from some 0.875in. round bar. The theory goes like this: take a cut along the bar to some diameter above finished diameter, and

measure the resulting work: say this comes out at 0.781in. You now make a few keystrokes and punch 0.781in. into the read out, so it now knows that the tooltip was at 0.3905in. from the lathe centre line, cutting a diameter of 0.781in.. Don't forget the plus/minus sign, though, or you'll both get confused! Now move the cross slide until the DRO reads 0.750in., take the cut and that's what you'll end up with, 0.750in.. Fat chance, no matter how many times I tried it, the finished size was wrong. Sometimes not much wrong, less than a thou but readily detectable, sometimes by several thou. And to add to the confusion and disappointment, the error could be either way, up or down on diameter. So, instant disappointment, and I packed up to go away and sulk, muttering awful things about Mr. Newall.

Whilst sulking and muttering I began to recall that this wasn't actually the first time I'd had this problem, and I'm sure it must ring a bell with others who have for example zeroed the cross slide dial at finished diameter, then worked to that setting for further components, only to have them come out the wrong size. I also recalled that I'd had an idea as to the cause of the problem, but hadn't been able to confirm it. But now, if I were to assume that the DRO was in fact correct, then I had to look elsewhere for the answer to the diameter problem, and might be able to prove or disprove the idea as to what had caused it in the past.

Now towards the end of the first article I wrote: "The capabilities and performance of these devices are such that you'll only get the full benefit if the machine is rigidly mounted, in good condition, and properly adjusted, set up and aligned. And properly used."

Yes, that nicely described my Myford. Very carefully set up, aligned and adjusted, and mounted on Myford's industrial stand which was firmly bolted to a concrete floor. Carefully used as well, each time I'd done a test the cross slide had been clamped, as was the top slide courtesy of GHT's clamping system. Since the DRO was reading cross slide movement and hadn't recorded any untoward creeping, the error didn't come from that quarter. The top slide was set with it's slides parallel to the work, so even if it had crept along slightly, that couldn't have caused the significant errors that were turning up. Only one suspect left, deflection within the top slide assembly. A few more tests, and Bingo, I'd got it!

Let's say we rough down with 0.020in. depth of cut from 0.875in. to 0.795in. diameter, measure the work and input the dimension to the DRO. Take another 0.020in. cut to 0.755in., followed by a finishing cut of 0.0025in. Normal practice, agreed? Well, that was the cause of the problem. When cutting at 0.020in. deep, the load applied at the tool causes slight deflection via the top slide, allowing the tool tip to move from the dialled position to some other point the amount of deflection will depend upon the depth of cut, the condition of the mating faces of toolpost and top slide, how well your top slide gib is adjusted, and the condition of the mating faces of top slide and saddle. So we input a diameter cut by a deflected tool, then finish with a light cut that doesn't deflect the tool. Hardly surprising that things go astray. The variation in error is then simply accounted for by the fact that I wasn't cutting consistently to the same depth of cut on either the measurement or finishing cuts, so I was getting variable results.

As soon as I started taking an intermediate finishing cut immediately before taking the initial diameter measurement, and always used that same depth of cut to get to finished diameter, instant disappointment was replaced by the instant happiness of perfect and repeatable results. As long as the depths of cut for the intermediate and final finishing cuts were kept sensibly alike. A bit inconvenient at times.

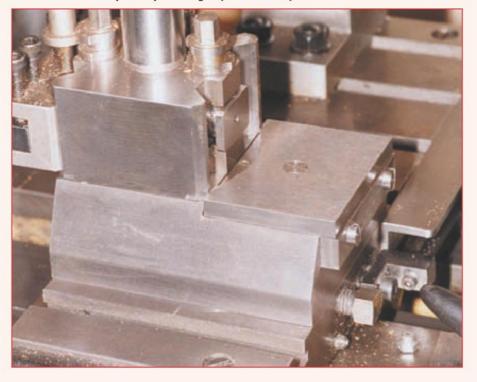
You might be tempted to think that the tool holding was at least partly to blame, but I can assure you that wasn't the case as I use a Myford-Dickson tool post and holders which are amongst the most rigid of the quick change varieties. And a few days later, I was able to show that wasn't the culprit.

Now why do we want a top slide? So that we can a) turn short tapers, and b)

advance the tool accurately towards the chuck when facing off. That's about it, I think. For me at least, a) is rare, and could be dispensed with for the vast majority of my lathe work. So far as b) is concerned, the machine's now got a DRO scale for movement to and from the chuck, so who needs a top slide for most work? Older readers may remember a tool post design by Tubal Cain that went straight onto the cross slide, no topslide in the way. He called it the 'Gibraltar' toolpost because it was as solid as a rock! So taking TC's toolpost as a hint, and my experiences as encouragement, I made a version to take the Myford-Dickson tool post. The finished item is shown in photo 2, and again taking the hint from TC, I call it the Bunker tool post - it'll take a bomb to shift it!

This has made an enormous difference to both the lathe's cutting capability (I'm not a paid up member of the Society for Prevention of Cruelty to Myfords, by the way!) as well as to it's accuracy and the repeatability of diameters cut against the DRO. It also indexes the M-D post, as well as my square 4-tool turret, so I can zero a tool in, twist it away to cut at an odd angle where clearance is needed, then index it back and still have the tool point as near as damnit to it's original, zeroed, position. I can't quote the accuracy of the tool positioning, but I can't detect any error on finished diameters after moving and re-setting the tool. Of course, since it still uses the same Myford-Dickson tool post and holders, it confirms that my top slide was indeed a source of slight deflection. This may have been inherent in the design, or more likely due to an element of wear, since on anything but a brand new machine, it can be tricky to ensure correct gib adjustment over total topslide travel. Additionally, it is not unknown for wear to occur on the swivel faces such that slightly convex surfaces lead to reduced rigidity.

### 2. The "Bunker" toolpost improves rigidity and accuracy.



### Other benefits

That tale has served to illustrate both how a lathe DRO is used for basic turning, and how it's performance can be negated by deficiencies in the machine and the operator. How else does it benefit one's working?

Well firstly a Myford is often used for drilling holes in a work piece mounted on the cross slide, so it's advantages for accurately positioning holes are the same as those described for the mill system, albeit with the obvious limitation that it can only work on a single axis. And you need to remember to switch it from diameter to radius mode!

Anything mounted on the cross slide can be moved towards and away from the headstock by precise distances, so facing castings and such to length becomes a simple matter. Yes you can use the leadscrew handwheel to do the same job, but the backlash can be significant on a worn machine, and tricky to compensate.

What about setting up to turn a taper? I haven't had occasion to try this as yet, but it should be very easy indeed. Any taper can be expressed as say 0.253" per foot, so with the cross slide connected to the taper turning attachment one would simply zero both axes, then move the saddle along the bed for a distance of 12", adjusting the taper turning slide until the said 12' lateral movement produces 0.253" of cross slide travel. No DTI needed, no master taper as reference. And if you want to set up for a metric taper, it's only necessary to switch to metric measurements on the read out, no conversion to be done.

That's another huge advantage, you can switch between imperial and metric at will, the DRO does the conversion for you. The lathe (or mill of course) becomes a dual-calibrated machine, equally at home and comfortable in both territories, and quite content to mix them on the same job. Can't think why anyone should want to do that, but if they do, the facility's there.

The next feature worthy of comment isn't available with all types of DRO, and in fact Newall offer a Microsyn/Topaz system without this feature, which reduces the cost significantly. Whether or not you decide to spend the extra will depend upon whether or not you put sufficient value on the facility. And that's the facility to zero-in nine different cutting tools.

Let's assume that you have a toolpost such as the Myford-Dickson, whereby you can interchange tools and each tool tip will re-locate at the same position as it was before it was removed. With a suitably featured DRO, each tool can be programmed into the DRO in the same way as I described above, each one's data (for both axes) stored against a tool number. So you set up each tool, giving it an identity number, and each time that tool is fitted you tell the DRO you're using say Tool 2, and its display changes to indicate either the distance of that tool point from lathe centre line (radius mode) or the diameter it will cut (diameter mode). This works for any

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tool, whether it's in the front or back toolpost, the only difference is that you need to remember to put the appropriate plus or minus sign before the measured diameter, according to whether the tool's at the front or the back. To date I've only used this capability for up to three tools, (roughing and finishing tools in the front tool post and a parting tool for grooving in the back one), but it's proved it's worth. In conjunction with the use of replaceable carbide tips which amongst their other advantages eliminate the need for tool re-setting (and therefore re-zeroing), the tool offset capability can bring real benefit when multiple components involving the use of a number of cutting tools have to be made. Not just several-off of one component, mind you, making different components also benefits from having the tools and the DRO effectively calibrated for each one. As long as you don't get a power cut that is, when you then have to go through re-calibrating the lot. Easy to cope with though - just spend even more money and buy an un-interruptable power supply to run the DRO!

Oh yes, I've used the offset facility for boring a large diameter blind hole where I had to open it out with a small tool initially, following up with a bigger, stiffer tool as the bore progressed. Each tool was programmed in for both diameter and distance from the face of the job. When I changed tools the DRO compensated for the different lengths of

the boring bars, so by watching the Z-axis read out I could get to the bottom of the bore without the 'orrible graunching noises that result when the tool hits the bottom. I could also accurately position the bottom of the bore, and skim either the bore or the bottom at any time through the progress of the work without fear of 'losing my place' and inadvertently running the tool into either one or t'other.

### Which way to look

Now that needed me to watch the display, not the work, and that's taken some getting used to. I was so accustomed, so conditioned, to watching the cut and keeping an eye on the dials, or vice versa, that to turn one's eyes completely away from the work and saddle was initially quite alien. As I said, it takes some getting used to, but eventually I did. Now I find it strange to do anything without the DRO, and look down at the work and saddle! No doubt I'll strike a balance eventually and become equally comfortable working either way.

After those initial problems were sorted, that's the only difficulty that I can think of, the only disadvantage. I'm still learning how to use some of the features nearly a year after I installed the kit, my excuse is that I'm not cutting metal eight hours a day, five days a week, and that naturally extends the learning curve in comparison to someone working in industry. And of

course I'm not using every feature every day, so there's still a need to resort to the instruction book every now and then. But those occasions are getting fewer each time I use the systems.

Each time I use them I marvel at their capabilities, and take pleasure from producing things that fit so nicely together, with such little effort on my part in terms of measurement, marking out, etc. I can assure you that not having to do all that, is not, for me, a down-grading of skill, it's a welcome relief from some of the tedium of peering through loupes and magnifying lenses in order to read scales on rules and vernier height gauges, then trying to locate a drill right atop an intersection of two fine lines. I never did enjoy marking out, and that lack of enjoyment has increased as my close vision has deteriorated. Nor did I enjoy making allowance for backlash when indexing on the mill, that drudgery has gone as well. They have saved me time, precious time, in many ways, time that can now be spent on other aspects of building a locomotive. Nearly a year down the line from that fateful trip to Donington in September 2001, I think I can answer the question 'Were they worth it?' For me the answer is 'Oh yes, they were. Most definitely.' And I'll kill anyone who tries to take them away from me!

In the next and final section of the article, I'll look in detail at the mounting brackets for the Myford.



# NEXT ISSUE

### Coming up in Issue No. 87 will be

### **Engraver Cutter Grinder**

Doug Ball looks at engraver cutter geometry, and presents a device for accurate grinding.



Adrian Kruger gets a quart into a pint pot with extra daylight.



### Issue on sale 13th December 2002

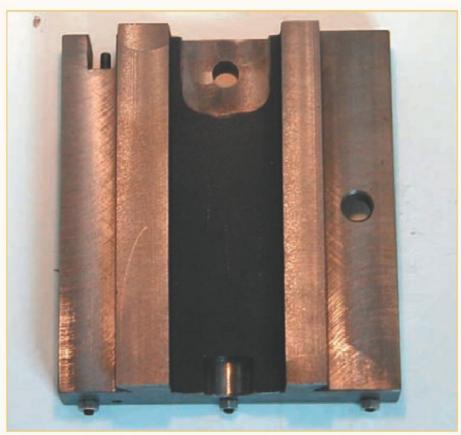
(Contents may be subject to change)

### **Gantry Crane**

For moving heavy models or workshop machinery, Philip Amos may have the answer.



## RETROFITING BALL SCREWS TO A WABECO MILL



1. Y-axis slide showing the two mounting holes for the X- and Y- axes nuts.

### Background

I purchased my CNC option Wabeco 1210 mill just over 2 years ago. The original reason for embarking on CNC was that my deteriorating eyesight was making fretting skeleton clock plates and crossing out wheels increasingly more difficult. Now two years on, I wonder how I managed before I had my CNC mill. Everything had been going smoothly and I was delighted with the accuracy obtainable with the machine. Recently however I began to notice that the parts I was making were no longer quite as accurate as they had been. I re-ran the backlash compensation routine that comes with the software only to find that the backlash, which initially had been uniform along the length of the X-axis screw, now varied quite considerably along the length of the screw. The same applied to the Y-axis screw. If I had only been using the mill as a hand operated machine this non-uniform wear would have been of no consequence. But as I use the mill very extensively in CNC mode (the machines in my workshop have to earn their keep!) the degree of non-uniform backlash meant that the screws were now worn to the point of justifying replacement. Either I replaced the old screws with new Acme screws and nuts with the prospect of replacing them again in a further couple of years or I replaced them with ball screws, which would last a lot longer. Before making a decision the cost implications of the two types of screws needed to be considered. Some years ago I looked into replacing the worn screws on a BCA Jigborer. Then the cost of a quality Acme screw and nut was in the region of £100. Not at all cheap! The replacement ball screws from Wabeco were about £200 each. The basic difference between the two types of screw is, the Acme screw involves sliding friction between the threads in the screw and the nut and the consequent wear. With ball screws the friction is rolling friction and the wear is significantly reduced as a consequence.

Dick Stephen describes a performance enhancing rework.

## The Alternatives and Options

Having reached the decision that replacement with ball screws was the only

realistic option, the next problem was how to actually carry out the fitting. There were two possible options. The first was to have Wabeco in Germany do the fitting for me. This would have involved my shipping the mill to Germany and being without it for about 8 weeks. The cost of fitting would be about £500. Together with shipping I was looking at a potential cost somewhere in the region of £1500 with VAT included. This was sufficiently large to prompt me to look for an alternative. After phoning around a bit I finally settled on the firm THK as the best possible source. The principal advantage of THK was they were able to supply 14 mm diameter, 4 mm pitch screws, the same pitch and diameter as the original Acme screws and a platform nut which potentially would make fitting a lot easier Incidentally THK are the

look for an alternative. After phoning around a bit I finally settled on the firm THK as the best possible source. The principal advantage of THK was they were able to supply 14 mm diameter, 4 mm pitch screws, the same pitch and diameter as the original Acme screws and a platform nut which potentially would make fitting a lot easier. Incidentally THK are the only manufacturer I have found that supplies a platform nut. The other nuts supplied by THK and all those from other manufacturers are cylindrical with mounting flanges on the end. These nuts are also significantly bigger than the THK platform ones and would be a lot more difficult to fit, at least to the Wabeco. The final decision could only be made once the mill had been dismantled and the possible methods of fitting the nuts considered. I had already seen the way Wabeco had fitted ball screws. This clearly involved significant modification to the castings. The screws from THK did have one disadvantage, namely only right hand screws were available. The X- and Z- axis Acme screws originally fitted were both right hand threads only the Y-axis had a left hand thread. THK said they could supply a left hand thread screw at a cost of several hundred pounds. I decided that the slight inconvenience of a right hand thread Y-axis, which would only be a "problem" for hand operation, was not worth

### **Nut Brackets**

spending a lot more money.

I set about stripping the mill down and only when I removed the nuts did I realise just how simple fitting the new nuts was

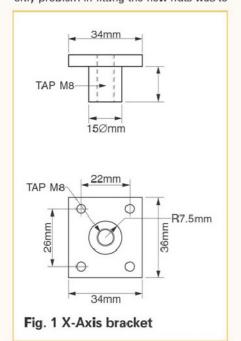
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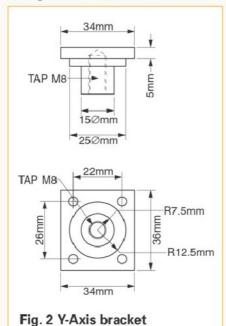
going to be. **Photo 1** shows the Y-axis slide to which are attached both the X- and Y-axes nuts. **Photo 2** shows the original Acme nuts. The 15 mm diameter cylindrical stub of the nut inserts into the 15 mm diameter hole in the casting The axis of the cylindrical section of the nut is lined up with the axis of the thread in the nut. The Z- axis nut is similarly fitted. The only problem in fitting the new nuts was to

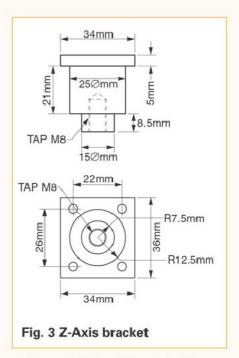
make an attachment bracket having similar features to the original nuts. The brackets I made for the new nuts are shown in **Photo 3**, and **Figs 1**, **2**, **and 3**. The only bracket that gave a slight problem was the X-axis one. In Fig 1 the thickness of the rectangular mounting for the X axis nut has not been given. The thickness will depend on precisely how much of the casting is milled off to accommodate the

new nut The height of the central axis of the original Acme screw above the machined surface of the casting is 10 mm. The distance of the ball nut to the mounting surface is 13 mm. To get the height of the nut correct and to give something to bolt the nut to required the depth of the recess originally machined in the casting to be increased by about 6 mm. This gave the thickness of the rectangular mounting plate after I had machined my casting as 3.24 mm. The only other machining that appeared to be required was to increase the width of the slots in both the Y- and Z- axes slots in which the nuts slide by 4 mm. The original width of these slots was just 34 mm, exactly the width of the ball nuts. I could probably have got away with using a file to increase the width, but preferred to do a neater job so I took the castings round to a friend who has a Theile Mill which made short work of the machining



3. Nut brackets and platform nut







4. The welded joint of the original Acme screw and extension shaft.





5. The machined ends of the screw shafts and the extension shafts.

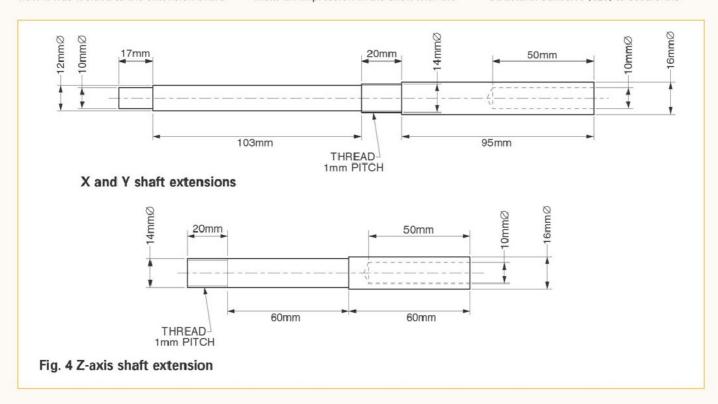
## Adapting the ball screws

The rolled ball screw shaft supplied by THK comes in either 1000 mm or 1500 mm lengths and is induction hardened. A single 1500 mm length of rod was adequate to make all the three screws for my mill. **Photo 4** shows a close up of one of the original Acme screws illustrating how it was welded to the extension shaft.



After some deliberation I decided that the best way of attaching the extension shaft was to grind down the ball screw shaft to 10 mm diameter and fit this into a reamed hole in the extension. The dimensions of the extension shafts required for the Wabeco 1210 CNC Mill are given in Fig 4. Before the ball screw shaft was delivered I turned up in the lathe the three extension shafts and reamed a 10 mm hole in the end to a depth of 50 mm. At this point I was faced with the problem of getting the ball screw shafts ground down to 10 mm diameter for a length of 50 mm. As soon as the ball shaft was delivered the first thing I tried was a file on one end of the shaft. Though clearly quite hard I was able make an impression in the shaft with the

file. This gave me hope that I would be able to turn the shaft down with a carbide tool in the lathe. My hopes were confirmed when I was able to cut off a length of shaft with a hacksaw. Clearly the surface of the screw was quite hard, however once through the skin, the steel cut quite easily. With the length of shaft held in a 14 mm collet taking light cuts the end was turned down to 10 mm diameter for a length of 50 mm. Initially I had a bit of difficulty until I arrived at the optimum depth of cut, feed rate and speed. Once I had these parameters worked out it was simply a matter of patience. The diameter of the ends were made approximately 0.02 mm under size as I planned to use Loctite Structural adhesive (320) to secure the





shafts in the shaft extensions. Photo 5 shows the screw shafts machined down to 10 mm and the three extension shafts. The Loctite will produce a perfectly adequate joint, as the axial forces on the screws under any normal operation are quite small.

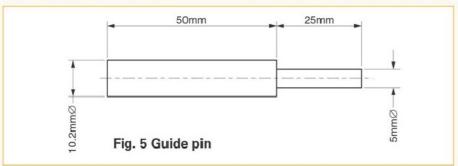
If you don't like the idea of using Loctite then a really snug fit and a pin to hold the shaft in place is an alternative method. Any form of join involving heat is not advisable as this may damage the ball shaft. The final job was to drill a 5 mm hole in the other end for a guide pin in each ball shaft (see below). The ends of the shafts and the holes in the extension shafts were carefully cleaned free of all oil and grease and thoroughly dried. The ball shaft was gripped in the collet, Loctite was smeared on the end and in the hole in the extension. Using a centre in the tailstock the extension was pushed in place, and left until the Loctite had set. The screw was removed from the collet and left overnight for the Loctite to fully cure.

The ball nuts are supplied on a short length of tube, which is used to retain the balls in place in the nut. If the tube is removed in the absence of the screw all the ball bearings in the nut will fall out which will give you two problems. The first is the balls will have all fallen onto the floor of the workshop. There they will either have got intimately combined with all the rubbish on the floor or if your floor is nice and clean rolled into some

inaccessible corner where you cannot find them! Having dropped out all the balls the next problem will be to get them back again. To overcome these problems I made the guide pin illustrated in Fig 5. One end of this guide pin inserts in the 5 mm holes drilled in the ends of the shafts and the other end into the ball retaining tube. Photo 6 shows the guide pin in place in the Z-axis nut. As the shaft is screwed into the nut the tube is forced out. Photo 7 shows the Z-axis shaft successfully fitted to the nut. The retaining tubes should be put carefully away as they will be needed if the shafts ever need to be removed from the nuts. I next fitted the Y and the X screws in place. The Y-axis was no problem however when I tried to slide the table over the X-axis nut I found that the top of the nut failed to clear the underside of the table by about 1 mm! The only remedy was to mill a slot in the underside of the table 3 mm deep and 25 mm wide to give plenty of clearance. Fortunately I had access to a mill with the capacity to cope with this simple job. Having machined the slot the fitting of the screws was completed.

## Alignment and backlash

The three screws appeared to work nice and smoothly. I finished reassembling the machine with the stepper motors in place.



The final job before I could test the system was to invert the direction of rotation of the Y-axis to take care of the change from left hand to right hand pitch. All that was required was to interchange the two wires from one of the windings of the motor. This done it was time to measure the magnitude of the backlash in the screws. The CNC software I use, PCLathe, has a very useful programme called SYNCUTIL for compensating for the backlash in the screws. On running this programme, the measured backlash in both the X and Y screws was a lot more than the figure of 0.05 mm given by THK. The Y-axis did feel a little "odd" when turned by hand so I began adjusting the alignment of the nut/shaft. This turned out to be the root cause of the problem. After a bit of tinkering and appropriately placed pieces of shim stock I was able to reduce the backlash on both the X and Y axes to almost the expected value. The ball nuts may appear initially to be tolerant of the alignment as I had thought. This is not the case alignment is absolutely critical if the screws are to work as designed.

### Conclusion

In spite of the alignment problems I encountered, I was surprised how easy and quick the job was to do. Having now worked out exactly how to do the fitting I reckon the whole job, once the required parts had been made, could be done just over a day. If you want to fit ball screws to any other mill, then using the platform nuts supplied by THK should make the job almost as easy as fitting new Acme nuts and screws.

Now that the mill is again in working order I have been able to appreciate just how superior the ball screws are. There is a small amount of backlash, which is very nearly constant along the length of the screws. The only way to avoid all backlash is to use preloaded precision nuts and ground screws. To go down this road you will need to have a very fat wallet.

If the screws on your mill are reaching the end of the road or have already got there I can recommend fitting ball screws. I have not found the change from left to right hand pitch in the Y-axis any problem at all for hand operation. If you do not wish to fit the ball screws yourself Maynard Ltd. are willing to undertake the work of retrofitting.

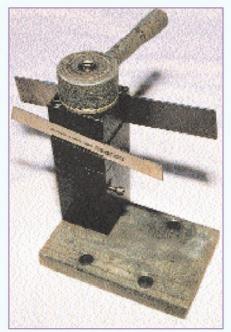
### **Suppliers**

For ballscrews contact: THK UK 25 Alston Drive, Bradwell Abbey, Milton Keynes, MK13 9HA Tel 01908 22 21 59

THK are an international Japanese company with branches throughout Europe and the US.

For retrofitting contact:-Mark Maynard, Maynard Ltd. 10 Merritts Mill Industrial Estate, Woolchester, Glos. GL5 5EX Tel: - 01453 833185

# PARTING OFF WITH THE QUORN



1. Initial attempt at Thomas design.

### **Background**

Parting Off! With the Quorn? Is the man mad? Well amongst other things this article is actually about the use of the Quorn to grind a parting off tool into the shape recommended by George Thomas in reference 1 and also about modifications to his style of rear tool post.

2. First turret detail.

Philip Amos reviews parting off techniques and describes a method for achieving accurate blade geometry.

ike just about every other home workshop lathe operator I have had my share of smashups when parting off - and very unnerving it is too. So when I read in reference 1 about the mechanics of the rear tool post, this made a lot of sense and I decided that I must have one. I followed the Thomas pattern tool post using "Eclipse" style blades, but still had a few smashups and I concluded that my emulation of the Thomas pattern was insufficiently rigid, and would not hold the blade accurately enough. My early attempts at shaping the blade to the Thomas "Ultimate" pattern were poor also. So since that time I have adopted the double side-by-side groove Thomas approach with marked success. Nevertheless it still seemed a worthwhile challenge to attempt to follow the Thomas rear tool post concept. Now read on.

### First Considerations

Thomas made a careful analysis of the factors likely to cause problems in parting off and set these out in a series of articles in ME entitled "Matters Arising" (later incorporated in his Model Engineers Workshop Manual). To recapitulate, these problems were:

- Lathe flimsy or in poor condition.
- Tools unsuitable or poorly set.
- Nature of workpiece material.
- 4. Type and quantity of lubricant.
- "Gun shy" operator using speeds too low.

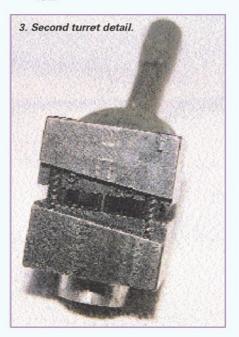


- (i) Minimum overhang of workpiece from front of chuck jaws.
- (ii) Less top rake than used for normal turning tool for same material.
- (iii) Tool set slightly below centre (front mounted tool)
- (iv) Tool narrower at back than front.
- (v) Tool exactly square to lathe axis.
- (vi) Saddle locked to bed.
- (vii) Speed about half that for turning same material.
- (viii) Feed in slowly by hand.

Thomas used these criteria in his development for a rear tool post for parting off, which latter has a geometric advantage against digging in. I first read all this information in 1994 and decided to make myself a Thomas rear tool post with such changes as required by my own lathe configuration. It is a Taiwanese model with 6 inch centre height; the Tee slots in the cross slide run from the back towards the front rather than the side-to-side arrangement for which the Thomas tool post was designed.

My original attempt followed the Thomas design quite closely see photos 1 and 2. However this did not work too well. It would seem that it is not possible to simultaneously clamp two parting off blades in the one turret unless all angles and dimensions are quite exact; mine probably were not.

Consideration of this problem led me to another try which had only one parting off blade with its own clamping piece





Model Engineers' Workshop



5. Kit at conclusion of original attempts.

separate from the turret proper - see photos 3 and 4.

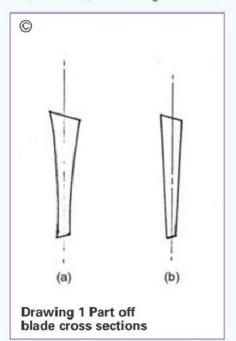
The opposite side of the turret was arranged to hold a chamfering tool secured in the conventional way by screws. This design did not perform much better and resulted also in a conventional smashup.

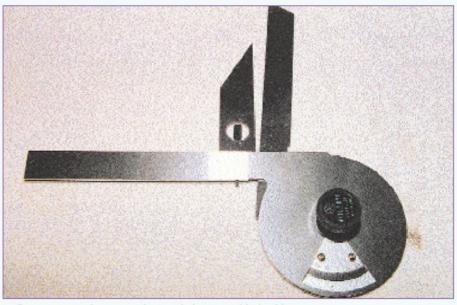
Photo 5 shows the whole kit at this stage. Turret 2 is in place on the post and turret 1 is on the bench. Two Tee bars for the cross slide slots allow the mounting base to be secured with three socket capscrews, each with a brass plug to keep out the swarf.

The whole project was then set aside for several years, and got under way again with a third try this year. Thinking about the Thomas advice, it seemed most important to be able to accurately shape the parting off blade by grinding, and to accurately position it and hold it securely in place.

### **Parting Off Tools**

Parting off blades are available in two types of cross section as depicted in **drawing 1** (as seen from the business end). Version (a) has hollow ground sides





Protractor set for measuring angle between blade sides.

whereas in version (b) the tapered cross section is straight sided. The top and bottom of the blade are chamfered at less than a right angle to the sides for gripping/location. Version (b) seems to be much more common these days. The angle between the long sides does not seem to have been standardised between manufacturers. The ones I possess lie between 3° and 5°.

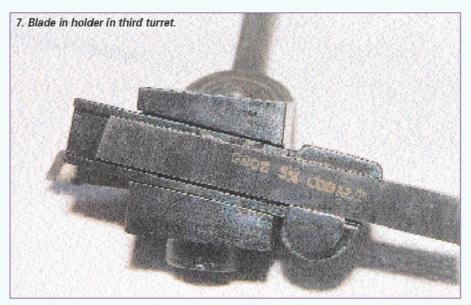
All lathe tools have clearances to allow them to cut. For a parting off tool, the front clearance can readily be ground; it is usually about 5°. Our very experienced toolroom foreman recommended a two stage front clearance - for about the first mm from the edge 2° to 3°, then 5° to 6°. I tried this but could detect no difference one way or the other.

As a parting off tool cuts into a slot it needs side clearance on both sides and this is manufactured into the blade by its cross sectional shape. The blade should be positioned vertically with equal clearances both sides.

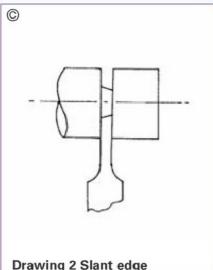
Many references suggest that in plan view the blade should taper in back from the edge on both sides at about 1deg. each side. While this may be appropriate for parting off tools of say 6 mm width and more, for those of 3 mm and less such practice severely weakens the already rather fragile tool. Considered as a cantilever beam in the horizontal plane the strength of the tool varies as the square of the thickness, and its stiffness varies as the cube of the thickness. If the tapering is to be of any use it must be continued back along the tool as far as the tool will penetrate into the workpiece. Thus it would not seem to be desirable to tamper with the plan configuration of thin parting off blades

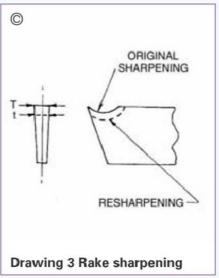
As pointed out by Thomas the often quoted suggestion in many references of slanting the cutting edge of the parting off tool slightly from parallel to the lathe axis, leads to sideways pressure on the tool and hence deflection which may cause jamming in the slot - see drawing 2, or an off square part off cut. Furthermore the chip width generated by the slant edged tool is wider than the slot so may not exit the slot as easily, and a higher tool loading is implied. The purpose (pipless component when cut off) is often not totally achieved and most workers are quite prepared to do a facing operation on the cut off part anyway.

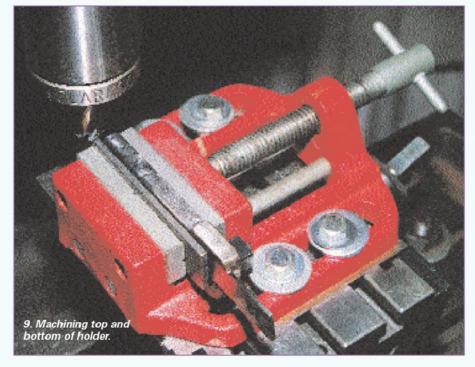
For most materials lathe tools are given











a top rake angle usually about 5° to 15°. A number of references suggest grinding the top of a parting off tool to achieve this as shown in **drawing 3**, but as Thomas points out, even if the initial sharpening leaves the cutting edge at the full height of the blade, re sharpening will reduce the height - but also the width of the cutting edge from "T" to "t" - hence the width of the groove cut, and the full width left at the top of the blade can jam in the cut. The Thomas design inclining the whole blade to achieve desired top rake angle avoids this problem. Smashups when parting off seem to stem mainly from:

- (a) the tool digging in, or
- (b) chips jamming beside the blade, and Thomas addresses these problems in the following manner:
- A rear mounted tool post is geometrically less likely to cause digging in if the tool is deflected by a chip not breaking from the workpiece - see drawing 4.
- II. If chips can be formed as ribbons rather than short pieces they are more likely to exit the groove in the workpiece. This is assisted by a flood of coolant in the case of a rear mounting tool post mounting.

### **Tool Positioning**

It is important to feed the parting off tool into the workpiece exactly at right angles to the lathe axis, as otherwise it will tend to at first bend, then jam and possibly break. It is fairly easy to precisely set the blade against a truly faced block held in the chuck or even against the chuck face or jaw face.

It is very much more difficult to precisely set the vertical centre line axis of the blade vertical so that equal side clearances are obtained on each side.

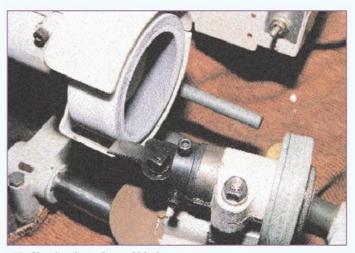
The exact cross sectional shape of the blade must be measured. The top and bottom chamfer angles can be measured with a vernler protractor, but it is not easy to measure the small angle between the vertical sides with this device as these sides do not come to a point. It is possible to fix the auxiliary arm to one main arm of the protractor so as to leave a small gap

### 10. Assembled third attempt.

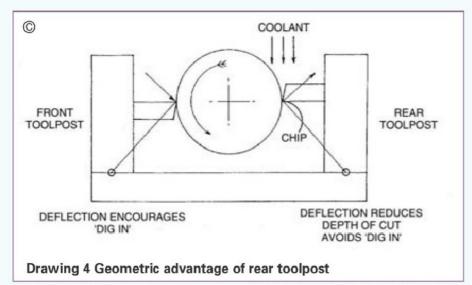








12. Shaping front face of blade



between it and the other main arm as shown in photo 6. In this way the sides of the blade can be made to contact both arms.

Although the vernier protractor itself can typically read to 5 minutes of arc, getting the two arms adjusted simultaneously is not easy; especially due to the arrangement for clamping the auxiliary arm in position, so that the final measurement can probably not be more precise than about a half degree.

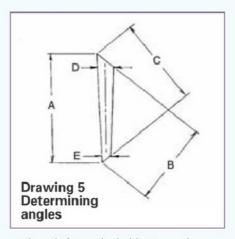
Another approach is to use a micrometer to measure the distances A,B,C,D, as shown in drawing 5, then plotting at 10 X scale and measure the angles resulting. This procedure is probably able to measure the angle between the blade sides to about one quarter degree accuracy.

Thomas uses small socket setscrews to bear against one side of the blade to cant it to get the axis vertical - seen in photo 2. It requires great patience and much trial and error (set screws, clamp blade, measure, remove blade, reset screws, etc,etc) and in my manifestation of his design, I felt that the blade was very insecurely held with this arrangement. There is anyway still the problem with the holding of the blade so as to be able to grind its top chamfered surface flat and at right angles to its vertical axis to produce its cutting edge.

From these considerations I elected to hold the blade in a traditional commercial holder, which has a tapered bolt forcing

the blade in against the back of the holder and its lower recessed edge - see drawing 6 and photo 7.

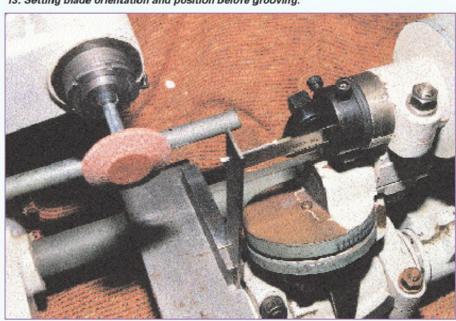
It would seem that the back of the holder slot is often machined perpendicular to the top and bottom of the holder and not so as to make the axis of the blade perpendicular to the top and bottom. By measuring the blade side



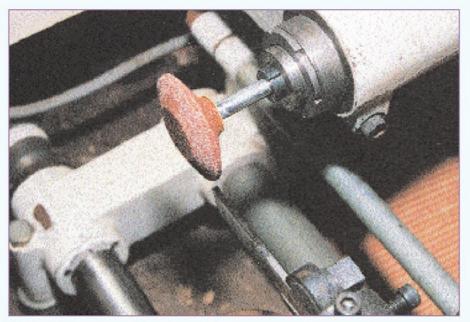
angles relative to the holder top and bottom it was determined that its axis was 2.25deg. out - see photo 8. So the top and bottom of the holder were then milled at a 2.25deg, angle to achieve the vertical blade axis. See photo 9 where a blade holder is clamped in a vice set on an angle table in turn mounted on the mill/drill table.

After machining the blade axis was again checked as in photo 8 and proved correct. The lathe centre height above the cross slide surface was measured with a vernier height gauge and determined to be

13. Setting blade orientation and position before grooving.



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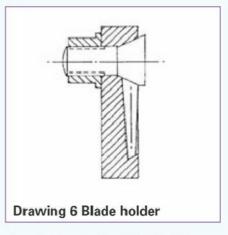
### 14. Completion of grooving.

87.70 mm. The arrangement was drawn out full scale with the parting off blade at 7deg. slope as recommended by Thomas and with the blade projecting 26 mm from its holder, with an aim of being able to part up to 2 inch diameter bar. Drawing 7 shows the general arrangement arrived at.

Because the blade slopes there exists a means of small height adjustment at its extremity by moving it in or out of its holder. The blade holder measures 18 mm high and 8 mm wide, and the slot to accommodate it was made 19 mm high

and 8 mm deep. It is secured in position with three M6 socket setscrews 6, 8 and 10 mm long. On the opposite side of the turret a slot 13 mm high and 10 mm deep is provided for the chamfering tool which has 10 x 10 mm cross section: the latter is secured with three M6 socket setscrews 20 mm long.

The third turret manifestation was then marked out prior to machining the slots in its sides. The slots were made with the turret clamped in the milling vice on the drill/mill: firstly a slot drill was run through

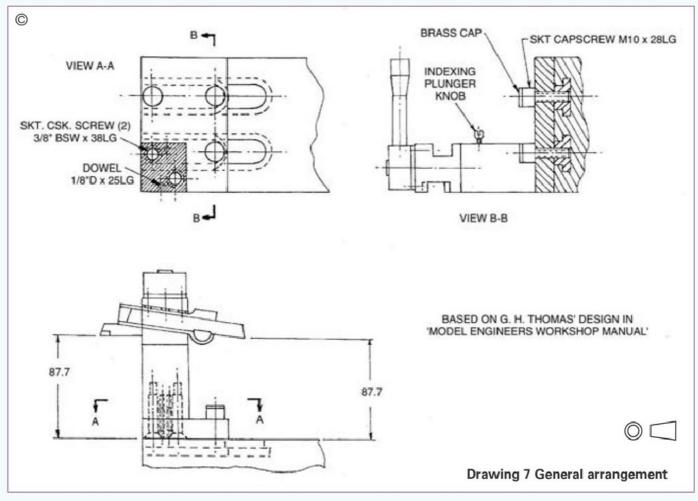


along the centre a line of the slot (0.5in inch diameter for the parting off tool slot and % inch diameter for the chamfering tool slot). In each case there were two passes at half slot depth. The slots were then brought to correct width with an end mill (%inch and % inch diameter respectively) against each slot side in turn.

The finished turret with the tools assembled in place is shown in **photo 10**.

### **Tool Shaping**

For the tool shape ("Ultimate") shown in reference 1- see drawing 8- having a Vee groove along its top surface, and a shallow ridge running down its front surface Thomas mandates the use of a Tool & Cutter Grinder. He used his "Union" machine but writes "it should be quite easy on a Quorn". Well maybe. However it would seem to require a methodical



approach and some care to effect this shaping with the Quorn. Below follows a step by-step procedure for achieving the required result.

When building my Quorn in addition to a toolholder with a square aperture for normal lathe tool shanks, I also made a similar one with a rectangular hole to accommodate parting off tool holders. For this current shaping exercise this arrangement proved most useful.

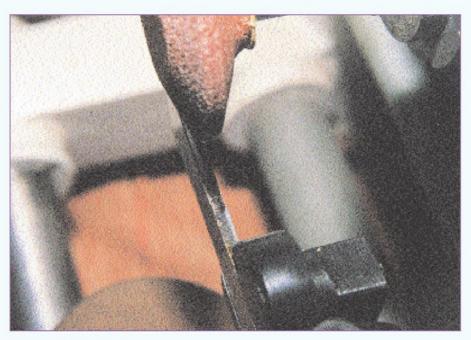
The shaping was effected in four stages as follows:

- To produce a flat surface on the top of the blade perpendicular to the vertical axis. The blade in its tool holder was clamped in the Quorn holder and assembled into the workhead, pointing at right angles to the main bars. Using a small square the side of the blade was set perpendicular to the rotating base upper surface, and then rotated by half the included angle between the blade faces (in my case half 4.5° i.e. 2.25°) using the scale on the division plate. The value was recorded for reference and then the blade rotated 90° so that its axis plane was now horizontal.
  - The workhead was moved to close proximity to the side of the grinding wheel, where the cut was put on with the front bar micrometer and taken by rotating the workhead around the front bar, see photo 11.
- To obtain a front face on the blade at 78° to the top flat (when the blade is raked at 7° this leaves a front clearance of 5°) the workhead rotating base was now turned through 102° anticlockwise in plan. The workhead was again moved close to the grinding wheel, the cut put on with the front bar micrometer and taken by rotating the workhead around the front bar - see photo 12.
- To develop the ridge along the front face of the blade having an 140° included angle, the same setup was used as in stage 2 above but with the workhead tilting bracket set at an angle of 20° up or down from the original zero setting. The end of the blade was blackened with a marking pen and a centre line marked along the blade vertical axis. Actually two lines because of the sloping blade sides and a mean was contrived from these to define the blade vertical axis plane. As before the cut was put on with the front bar micrometer and taken by

rotating the workhead around the front bar, until the marked axis line was reached - then repeated for the opposite side (after altering the tilting bracket setting).

The most exacting task is to cut the 140° included angle groove on the top surface of the blade. The largest available diameter grinding point of roughly disk shape had its edge formed with a diamond to yield a 140° included angle ridge around its periphery.

This point was mounted in a collet in the wheelhead spindle with its axis at right angles to the Quorn main bars, The parting blade had to be held in an extended position from its holder to allow the point to produce a groove back to

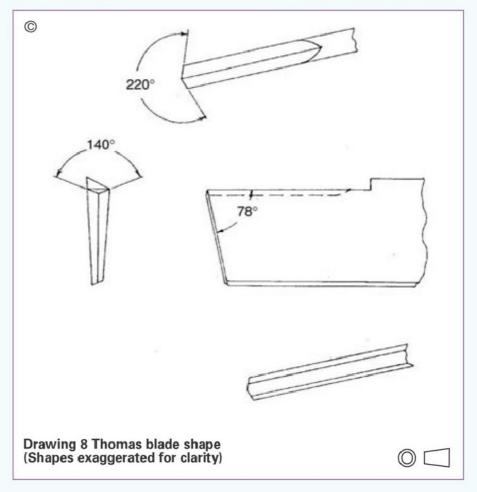


15. Close up of blade groove.

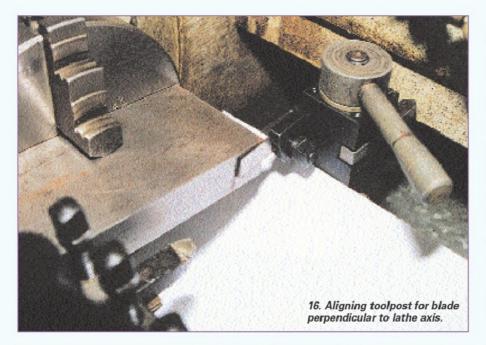
26 mm from the end of the blade.

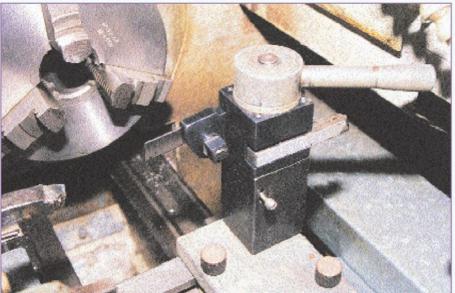
In order to get the blade in the same vertical plane and below the grinding point it is necessary to tilt the workhead backwards, and the toolholder assembly forward towards the operator. With some judicious juggling it was possible by eye to get the blade fairly well positioned, after which it was checked with a square placed on a parallel across the Quorn main bars. and then turned through the necessary 2.25° (as in stage 1) to get the blade axis vertical - see photo 13.

Using the rocking lever adjustment screw, the sideways positioning could be adjusted, but needed further checking of the verticality of the blade axis. The top surface was then blackened with a marking pen and a centre line marked on it with a jenny caliper. The machine was started and the point gradually lowered using the wheelhead adjusting screws until it just touched the blade. This was examined to confirm that the contact was on the marked line. The groove was then ground in a number of passes with the cut being



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17. Device with height set and ready for work.

set with the wheel head adjusting screws and taken by moving the workhead along the Quorn main bars.

It is of course quite vital that the blade is exactly parallel to the main bars both horizontally and vertically if a uniform

### 18. Trial result, showing improved surface finish.



groove is to be produced and centrally disposed on the blade: so an examination of the initial cut can show any slight deficiencies in these parallelisms, which can be corrected before proceeding. The production of the groove is thus quite a lengthy business, but can be achieved with care and patience - see photos 14 and 15.

### Tria

Having the parting off blade shaped it was then clamped securely in its holder with 26mm projecting, and the holder clamped in the rear tool post turret. It was again checked for verticality of the blade axis. The rear tool post was clamped in position on the cross slide with care to ensure that it was at right angles to the lathe axis, and at a position so that it would project forward of the lathe centreline when the cross slide was fully withdrawn - see photo 16. The height of the blade was checked and adjusted to be just slightly higher than the lathe axis - see photo 17.

A length of 1 inch diameter bright mild steel was chucked and skimmed with a right hand knife tool. Pieces of the bar were then parted off with the new device. These are shown in **photo 18**. As will be seen the surface finish is excellent, and can be compared with the rather indifferent surface finish of a conventional parting off operation shown for comparison.

Despite this good performance there was still a lot of chatter at some diameters and work overhangs, particularly at each starting point. Possibly this is due to forcing a narrow pointed tool into the workpiece, but see also the appendix discussing chatter. The chips produced were long and curly, consistent with the earlier observations by Thomas, although it is possible that the choice of workpiece material had a bearing on this.

### Conclusion

At the third attempt it would seem that a device has been produced which will improve the parting off process in my home workshop.

### **Appendix - Chattering**

Any mechanical system has a natural frequency of vibration, and if suitably excited by some disturbance will vibrate at that frequency. Common examples are organ pipes and violin strings.

In our case here the mechanical system comprises the workpiece, the chuck jaws, the chuck itself, the lathe spindle, its bearings, the lathe frame (that is headstock and bed), the cross slide, the tool post and the tool. Such a complicated system does not easily lend itself to analysis, but certain common principles apply:

- Heavy, solid, long objects tend to have low vibration frequencies, whereas light, thin, short objects have high vibration frequencies.
- II. Excitation can come from a single event - e.g. a hammer blow, the breaking off of a chip, etc or a series of repeated events. In the latter case the timing of these events must be such as to match the natural frequency of the system or its overtones (harmonics or subharmonics).

If a tool is deflected while cutting a chip and the chip breaks off, the tool can cease deflecting, and this process can repeat. If this deflection and recovery timing meets the criterion II above, then it is likely that chattering will occur. It may be stopped by increasing or decreasing the system frequency by changing the rotational seed, by changing the tool shape to yield continuous chips instead of small broken off pieces, by reducing the tool overhang or workpiece overhang from the chuck jaws or by adding mass to the tool itself.

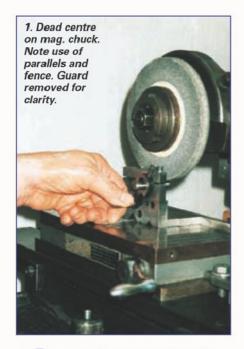
As a general rule minimum overhang in each case is recommended, and usually the slowest direct lathe speed achieves best results.

### References

- Model Engineers Workshop Manual - G.H.Thomas -1984.
- Quorn Universal Tool & Cutter Grinder - D.H.Chaddock -1984.

Model Engineers' Workshop

# ROTARY GRINDING



n the front cover of M.E.W for April 2002, I was interested to see a photo of an old friend, the Harig Grind-All. I first used this tool in the US of A in the early 70's and very useful it was too, working as I was, in the electronics industry on press tools, I made many punches using the Harig. A few years later, in England, I missed the old Harig and decided that I would build my own version. Now, the Harig is a fine tool, but it is a bit of a lump, and when you

Alan Booth describes a simple approach suitable for small punches or spindles.

have moved around from shop to shop and flown to and fro across the Atlantic as many times as I have, then portability is a consideration, so I made mine rather smaller and lighter, while retaining the capacity of the Harig. I will get around to my version of the Harig, in a later article, but for now I would like to discuss some simpler means of rotary grinding.

#### The dead centre

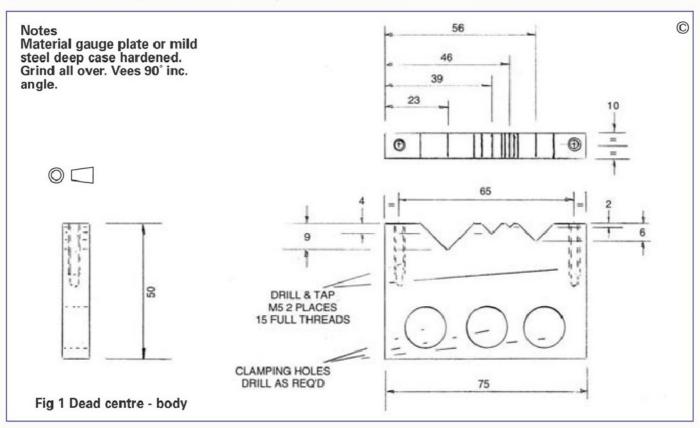
Again, I first came across this method in the United States in the early 70's, and the piece of equipment we are going to talk about I have heard referred to variously as a -"Whirlygig - Whirlyjig or -Dead Centre". Let's call it by the latter name, Dead Centre, from now on, (See figs. 1 & 2). Being by background, a toolmaker, I have liberally specified "Hardened and ground", on the drawings. For amateur purposes, unhardened components would probably give a reasonable service life, but it should be noted that in order to grind a parallel diameter, the Vees must be formed to accurately support the workpiece, with the axis horizontal. Another piece of equipment which will be needed to complement the Dead Centre is a means of gripping the workpiece for rotation. Let's call it the 'V' centre handle. (See fig. 3), V handle for short.

#### Method of operation

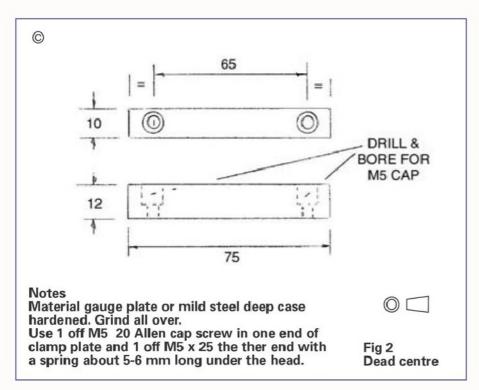
If you have access to a surface grinder then the Dead centre is placed on the mag. chuck against the fence or rail, with sufficient parallels in between to ensure working room. ( See Photos 1 & 2) Safety conscious readers will be reassured to know that all the photos were posed with the machine stationary. The wheelguard was removed to improve visibility of the workpiece, and it was unnecessary to don the safety glasses. For actual operation, these safety measures are, of course, mandatory.

If you are working with a tool and cutter grinder, then the means of setup will depend on the machine design. (I am assuming some basic knowledge at this time. For this method to give accurate results the material that you intend to grind will ideally have a hardened and ground outer diameter, as the accuracy of the ground section is dependant on that of the location section. Broken cutters, centre drills, etc. are ideal for making up little punches, cutters etc. - you can, of course, buy punch blanks in a variety of sizes. Whatever the source of material the precision ground diameter of the blank forms its own bearing.

The punch blank, is gripped with the 'V' handle and placed in the most suitable vee of the Dead Centre to give a small gap between the dead centre body and the



November 2002

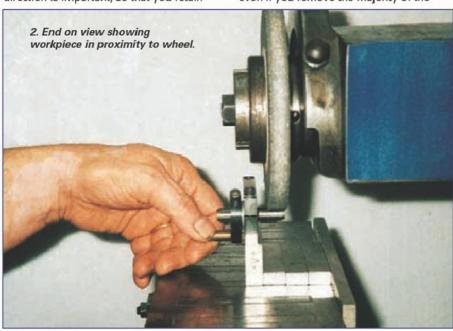


clamp plate, with the portion that you intend to grind protruding. You will need to place a suitable spacer, (a washer would be fine), on the punch blank, between the 'V' holder and the Dead Centre, so that the handle doesn't rub. The clamp plate is then adjusted so that it is level, and the spring adjusting screw tightened correctly, enough to ensure that the work doesn't tip in the vee but is still able to rotate freely. Now, the wheel having been dressed, the punch blank is positioned under the wheel at the lowest point of the wheel and the wheel moved to within about 0.050" -0.060" of the dead centre. Commence rotating the 'V' handle with your left hand, you need to develop the facility to maintain a constant rotation speed of somewhere about 70 or 80 rpm. The knack also needs to be acquired of rotating the workpiece in the vee without tipping it.

Now, you have your left hand merrily spinning away, clockwise of course, the direction is important, so that you retain control of feeding the workpiece against the rotating wheel. Your right hand will be used to operate the wheelhead, (see **photo** 3) and the cross slide. Bring the wheel down to touch on and note the dial reading. Now, there are two ways of removing material;

 a. Plunge grinding – in which the wheel head is fed slowly down, whilst continuing rotation all the time with your left hand, take it steady, this method generates a lot of heat.

b. Traverse grinding. Having touched on, wind the workpiece clear sideways, and bring the wheel head down by about 0.001" – 0.0015". Now, this is where the clever bit comes in, it is a bit like the old trick of rubbing your tummy while patting your head! Left hand rotating the work, feed the cross slide slowly into the wheel to your finish position, 0.050in.-0.060in. from the dead centre and feed slowly out again, this will give the best finish and, even if you remove the majority of the



stock by plunge grinding, it would be adviseable to finish off with a little traversing cut.

#### Vibration

When grinding diameters below 5 or 6mm, (you will notice that I switch between metric and imperial measurements with cheerful abandon) then vibration can become a problem. You will feel this vibration through the 'V' centre handle and the grinding finish will deteriorate dramatically. This, unfortunately, tends to damage the wheel surface and you will need to re-dress the wheel.

This vibration can be overcome by introducing a damping mass, in contact with the underside of the rotating workpiece. This damping mass takes the form of a half-inch cube of metal mounted on a spring finger and a swivel mount as shown in fig. 4. feel free to scale the drawing! - this should damp out the vibration successfully.

#### Lubrication

If you intend to remove more than a few thou then it is helpful to introduce a little lubrication as follows: -

Take a piece of masking tape, sufficient to cover the gap between the top plate and Dead Centre body and to wrap around the ends plus a couple of inches; place on a block of wood, sticky side up, and punch a hole with the punch that you have quickly knocked up, I use my shim die for this kind of thing.

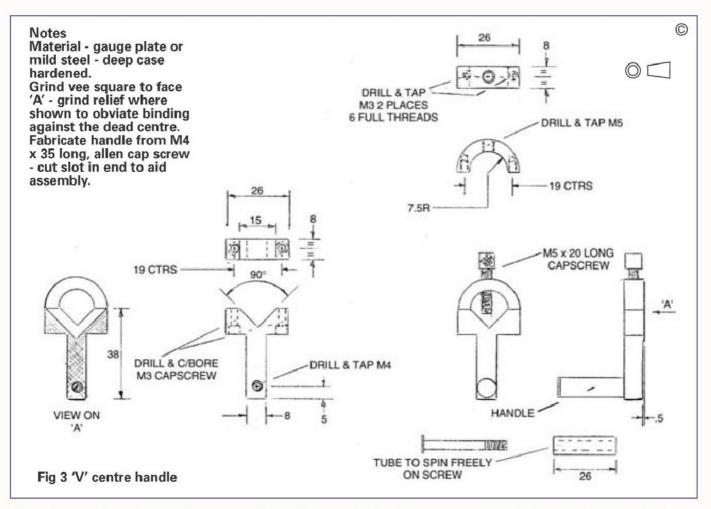
Place the punch blank in the dead centre and **lightly** tighten the spring tension screw. Slip the tape over the punch blank and stick it to the Dead Centre, covering the gap at the front and sides of the dead centre, tear off the excess at the ends. Remove the punch blank, smear a finger end of grease into the 'V', replace the punch blank, tension the spring screw and, hey presto, you have a grease lubricated sealed bearing, works a treat!

#### **End Plunge Grinding**

Some years ago, whilst working in a sub-contract toolroom I had a job making what were known as *pinsert punches*, which had to be reduced from, I think, 0.250in. down to 0.060in. for a length of about half an inch and of course it had to be done very quickly, as well as accurately. The method I used, after some head scratching, was to 'end plunge grind' - details as follows: -

The punch blank is placed in the 'V' centre holder protruding about \_ of an inch, rotated and blued with a marker pen. The wheel is then positioned about 0.050in. away from the dead centre, the working position, and touched on the rotating workpiece. The workpiece is then retracted into the deadcentre, and the wheel head brought down by 0.094in. This is arrived at by subtracting the finish punch diameter of 0.060" from the blank diameter of 0.250in. giving 0.190in. Divide this by 2, giving 0.095in. Prudently we need to bring the wheel head down by, 0.001in. less than this, hence 0.094in.

Now, you are going to need a good supply of coolant for this operation, directed full on the punch, otherwise the workpiece will glow dull red in no time!



(the coolant will act as a lubricant also). Start the coolant, a face mask is advisable, feed the cross slide in to the working position, and, rotating the workpiece, feed in and grind the blank sufficiently to give enough length of diameter to measure.

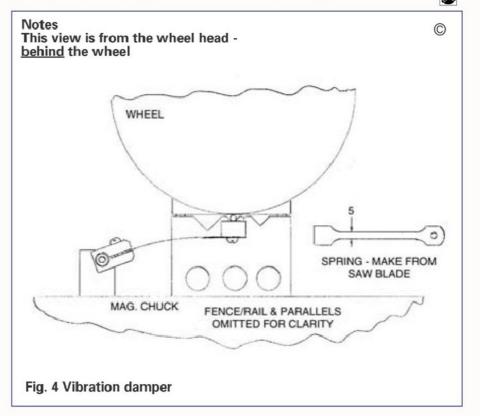
Withdraw the cross slide, measure,

adjust for the final cut and continue grinding by rotating and feeding the punch blank through the dead centre and into the wheel, not as easy as it sounds! This technique works well because the wheel is cutting across it's whole face, I used to grind upwards of a dozen punches without

redressing the wheel by this method.

The particular punch I used to grind by this method specified a concave blend radius between the body and the finished diameter and ideally this should be dressed on the wheel, but that is a subject for another day.





# TAILSTOCK FLOAT



ow many of us has at some time needed to cut a really small diameter thread which needs to be square, and free from the curse of drunken thread syndrome? The problem with using a tailstock die holder is, that should there be a slight misalignment of the tailstock for whatever reason, then the thread carries a risk of being stripped. The die holder to be described does not suffer from this fault. It is intended to faithfully follow the blank being threaded, keeping itself concentric with the centreline of the blank. In use, the floating head is moved manually so that the die runs onto the blank, and is prevented from turning by holding with the fingers. The degree of side float in any direction is a maximum of 0.02in. which I reckon should be more than sufficient to cater for most contingencies. In use the die is centred manually against the end of the

part to be threaded. The lathe can be run at a slow speed and the die will feed itself onto the part. To stop threading, simply release the hand grip. Note that the spring compression forces may need to be adjusted. The pressure is about right when the die head can be easily moved off centre, but still strong enough to prevent loss of parallelism. The die holder recess is bored to suit the die O/D's available to the individual. My small dies measured 0.8125in. dia. I did consider making the bore larger, and making adaptor sleeves to suit the smaller dies, but the main reason for making this tool was to enable the reliable cutting of small threads, and anything larger can be left to the conventional tailstock die holder as most of us will have one already. Construction of the tool is quite straightforward, the thread probably being the most difficult to machine. One other point comes to mind.



#### Dyson Watkins offers a method for cutting more accurate small threads on well worn lathes

It is as well to mention the apparently excessive length of the head end of the section, which fits into the tailstock. By all means make this shorter if you wish. My reason for making it this length was that I want to run off lengths of studding up to 4in. long. If you don't need this facility, then reduce the length of the overhang, but take care not to allow the reamed hole to break through the side of the Morse taper! So, let's get started and make it!

#### Die Holder

#### (Fig 1)

Set up a length of 1.375in. dia. Bar in the three jaw chuck. Square up the end face, and clean up the O/D. Centre drill the end.. Drill and ream to finish at %in. This diameter is not fussy, but it gives a clean and concentric datum from which to clock up when reversing to machine the other end. Bore it out lightly if you wish. Turn the diameter to be screw cut back to just short of the shoulder. When the diameter is down to size, finish to length with a squared off parting tool, and turn the undercut at the same time. Next set up the screw cutting tool and set the machine to cut 26 t.p.i. The tool needs an included angle of 55 degrees being Whit form. Do use a screw cutting gauge to set up the tool. It is imperative that the flanks of the thread should end up at the correct angles. Photo 2. If you don't happen to have a gauge handy, then make one from a Whitworth form bolt (e.g. \_ B. S. F. ) with the same t.p.i. turn down the head, and remove half the thickness as shown in the diagram. Hold the "gauge" in the tailstock chuck and offer up the tool to check alignment. Now machine the thread and chamfer the first thread back to clean off the burr. Reverse in the four jaw chuck and clock true. Face the end to a length to suit your particular die thickness. Bore out the recess and apply a small lead-in chamfer to the bore. Remember that if in your case, the die thickness happens to be greater than the recess depth given in the drawing, then increase the overall length of the die holder by the difference, otherwise the depth of the spring plunger holes will have to be reduced, which will affect the spring loading, and possibly the brass plunger lengths.

Mark out, centre punch, drill and tap the grub screw holes, which are M4. I used a home made dividing head to mark out, but because it was too big to set up on the drilling machine table I used a Vee block to support the die holder, the actual set up as in **Photo 3**. I was obliged to hold the part on the Vee block by hand, as I did not possess a suitable clamp.

# ING DIE HOLDER

Whichever method you use, just make sure that the holes are true along the radius of the part. Three M4 grub screws will be needed, and the ends should be dressed to suitable points.

Next mark out the three 7mm dia. holes for the brass spring plungers. Drill to depth, (I used a small piece of %in. flat strip as a depth setting gauge for the drilling machine) and chamfer all edges lightly.

#### **Retaining Cap**

#### (Fig 2)

Set up the bar in the three jaw chuck Face and turn the O/D to size. Centre and drill the through hole, and bore in preparation for screw cutting. Back face the end of the bore and turn the undercut. The back face needs to be finished smooth and square with the axis. Proceed with screw cutting the internal thread, (Photo 4) setting up the screw cutting tool accurately as with the male thread. I favour wrapping a piece of plastic insulation tape around the tool shank, and without switching on the machine, advancing the tool into the bore up to the point where it has to be disengaged. I then mark a line on the tape in line with the mouth of the bore. This gives me an indication as to the point where I have to disengage. Carry out trial fitting as the final cuts are approached until a satisfactory fit is achieved. When assembled the two parts should fit with their shoulders butting together. Check the inside gap dimension where the flange of the sliding tube is accommodated. This must be a clearance fit, with not more than 0.005in. of clearance.

### **Morse Taper Shank**

### (Fig 3)

Face and centre, leaving enough overhang to machine the Morse taper. My part was made to fit a Myford, so should you have a lathe furnished with a smaller size, then don't forget the danger of the bore breaking through the wall of the shank. You might have to make some modifications if this is the case.

Take a light skim off the outside diameter with the overhanging end supported on the tailstock. Check that the machined surface is parallel over the full length. Adjust the tailstock if required and re-skim until parallel. Set over the top slide to half the required M.T. included angle. In the tables, No 2 M.T has an included taper of 0.5994in. / foot.

Half the included taper will be = 0.5994/24 = 0.02497in. per inch.

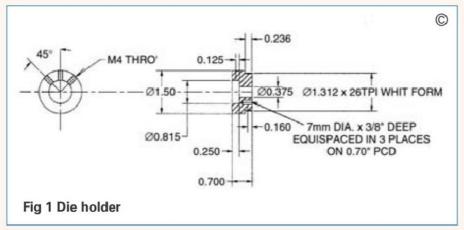
Set up a dial indicator in the tool post and adjust the dial reading to zero when the top slide has been wound back to a convenient starting position, where the tool tip just touches the work Now advance the top slide forward, a distance of one inch, when the dial indicator should

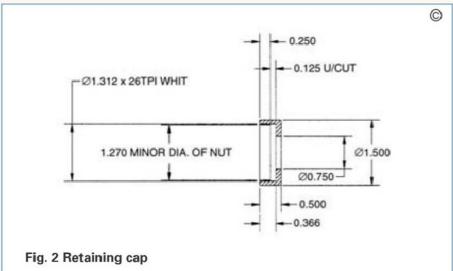


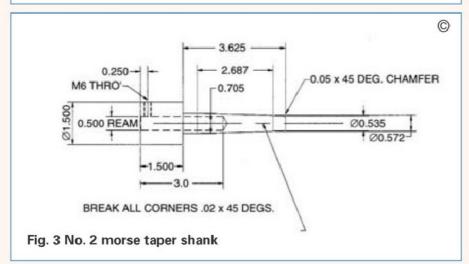


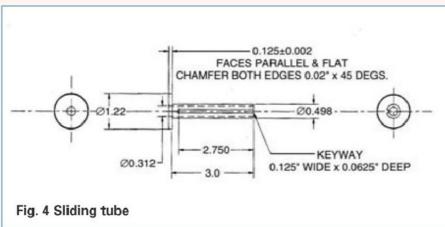


5. Turning the No.2 Morse taper. Note for finishing cuts, the tailstock support was not found necessary.









move a distance of 0.025in. If not then adjust until correct. Strictly speaking, for dti movement of exactly 0.025in. the topslide movement should be slightly greater than one inch i.e. 1.0012in.

Check the fit as the turning progresses, by sliding the tailstock into engagement after applying a little high-spot blue to the taper. The quality of the fit will become evident well before the final diameter is reached. Make slight adjustments as required should they be necessary, and when satisfied with the result, turn to the final size (see **Photo 5**). I decided against machining a tang onto the end of the shank as it was superfluous in my case, but it may be added, should it ever be required.

Remove the part from the chuck, and after removing the chuck from the machine, clean out the spindle nose taper thoroughly and mount the component directly in the spindle taper. Finish turn the end. Centre drill, drill and ream the hole to depth, and lightly chamfer the mouth of the hole. Drill and tap the M6 hole for the key, which is simply an M6 brass screw, with its end modified as shown.

#### **Sliding Tube**

#### (Fig 4)

Grip the bar at one end in the three iaw chuck. Face and centre. Drill %in. dia. through (Photo 6). Check that the centre drilling has not been totally removed, and if this is the case, then re-cut so that the tailstock can be used for support. With the end so supported, take a light skim and check for parallelism over the length. Turn down to the finished diameter aiming for a good finish. Check for a good sliding fit with the support. Machine the inner face of the end flange. Reverse in the chuck (or use the 4 jaw chuck if it does not run true). and face the end to leave a flange of 0.125" +/- .002" (Photo 7). Turn the flange O/D to size and add the chamfers. Remove from the lathe and check the assembly for the correct clearance. If too much play is evident, then this may be adjusted by carefully removing the desired amount from the mouth face of the screw cup, making certain that the cup is running true in the lathe.

Next machine the keyway, using whichever method is available to you. I used a vertical slide lash-up made up of an angle plate to which a spare ML8 cross slide was bolted. (Photo No. 8).

#### Key

#### (Fig 5)

This item is made of brass. Either make it from an M6 brass bolt, or make it from scratch. File, or machine the inner end to produce a sliding fit in the keyway. Outline details only are given for making this part.

#### **Spring Plungers**

#### (Fig 6)

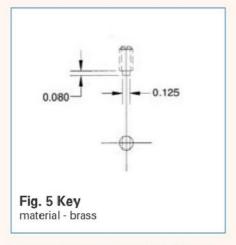
These are turned from Phosphor Bronze, although brass will suffice. I approached the problem from the situation of first finding suitable springs, and then making plungers to suit the springs (**Photo 9**).



6. Drilling through the sliding tube.



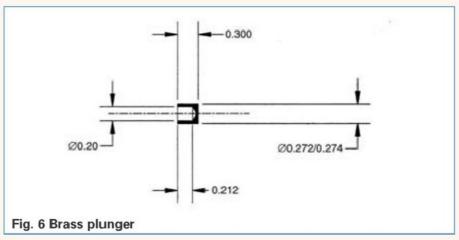
7. Facing the flange on the sliding tube.



Three are required. Again, these need to be a nice sliding fit in their housings.

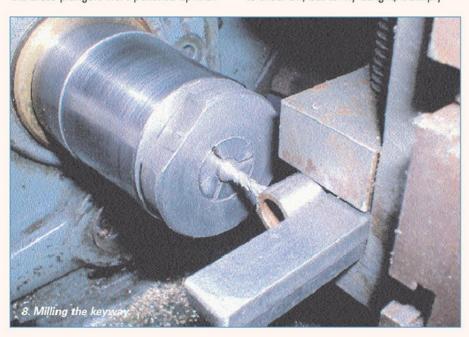
### **Assembly and Use**

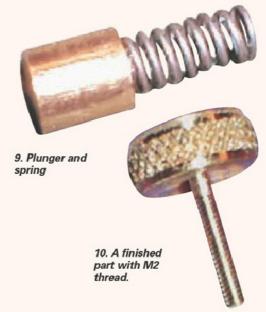
Ideally the faces of the sliding tube should be case hardened and ground, but being without the facility for carrying out these operations, I lapped the end face on a piece of cast iron, with some fine carborundum lapping paste. The ends of the brass plungers were polished up with



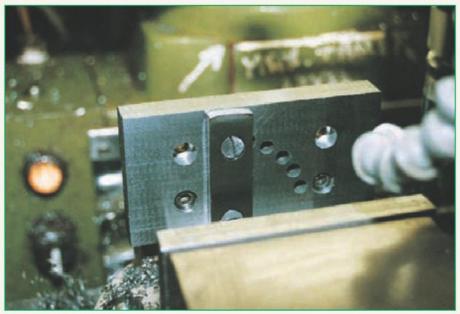
some 600 wet or dry paper. All parts were thoroughly cleaned, oiled and assembled. I initially tried the tool without assembling the key, and found no problems without it. I assembled the key and, satisfied with the ease of sliding the tube into and out of the M.T. holder, I cut another thread. This time I released the die holder once the die had engaged, and allowed it to feed on its own up to, and against the end face. I half expected the M2 screw that I was cutting to shear off, but to my delight, it simply

stopped cutting and rotated smoothly. I simply reversed the lathe rotation, and the die head screwed itself off, leaving a nicely cut thread. The finished part can be seen in **Photo 10**. The operation was repeated, with the tailstock deliberately moved off centre by about 0.015in. and another perfect thread was the result. I felt that the project was very worthwhile, and another useful tool joined my collection in the cupboard.





# AN ANGLE MILLING FIXTURE



1. Fixture fitted to vice.

#### The human limitation

This accessory was first dreamed up some years ago as a means of avoiding the frustration of not having three hands. I had for many years, as I believe most Engineers do, machined the ends of bars etc at an angle by holding them in a vice and using either a square or protractor to set the angle.

This method requires:

- A. One hand to hold the workpiece,
- B. A second to hold the square, and
- C. A third hand to tighten the vice.

### The two handed solution

To overcome this problem a simple jig was built see **Photo 1** and **Fig 1** which was adjustable from 15 deg. to 90 deg. in 15 deg. Increments. It can be built either as a free standing unit or can be bolted in as a substitute rear jaw of a standard milling vice.

The photographs and drawing relate to a unit made to suit my own vice which is an "ABWOOD". However the dimensions can be simply modified to suit any size or shape of vice which has removable jaws, which I would think is 99.9%. Generally vices are supplied with hardened and ground jaws held in place with two cap head or countersunk screws. However, as soft jaws are used extensively in industry we should not be unduly worried if we don't go the whole hog with hardened and ground finish.

### **Backplate**

My "ABWOOD" vice is a 4in. (102mm),

and has a jaw size of 102mm x 38mm x 12mm as standard, but I decided to use taller jaws to ease the holding of larger pieces. I therefore made my backplate 115mm long x 60mm high x 16mm thick, and made a matching front jaw.

The back plate is drilled clearance size and counterbored to suit the size and spacing of the attachment bolts in the vice, however by drilling the plate such that it may be used either up its correct way or upside down it becomes considerably more versatile (see Photo 2). (Use your hardened jaw as a drill jig to drill these holes). Also at this stage drill, ream, and tap the lower pivot hole. I am a great believer in using whatever suitable tools

Peter Rawlinson describes a device to speed angled setups for milling.

are available, and therefore I have used a mixture of metric and imperial as available. The reader may choose to use what he has and modify the drawings accordingly.

#### Arm

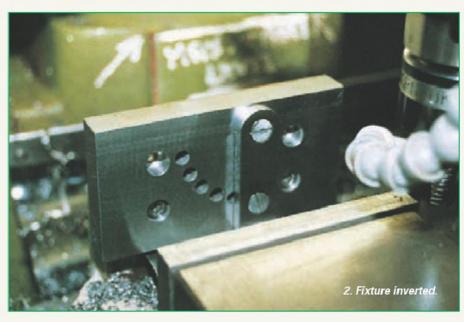
The arm should be made from 20mm x 6mm x 60mm long B.M.S. The holes are marked out, drilled, reamed, and counterbored. To this end I used a 6mm counterbore, pilot drilling the arm 6mm, then counterboring, and finally reaming the holes ¼in. dia.

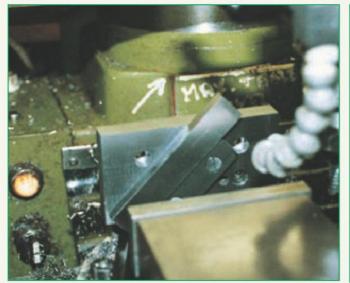
The ends of the arm should be rounded as shown by which ever method suits your equipment. Note that for accuracy in use, it is IMPERATIVE that the hole positions be accurately aligned with the edge of the arm.

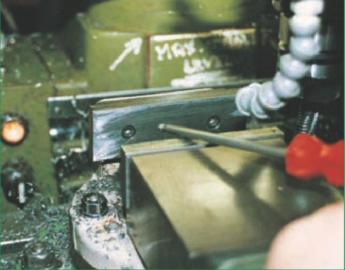
#### **Bolts**

Special bolts are required these being cheese headed shouldered bolts. I chose M5 for the thread, but 2BA would be just as suitable. The shank was turned to ¼in. to match the reamed holes mentioned earlier. My 6mm counterbore leaves a hole of 11.33mm dia. so I used 12mm B.M.S. bar turned down to suit. The remainder of the work on the bolts is a straight forward turning job, but the thread must be concentric with the shank.

Ideally the arm and the bolts should now be hardened, especially the arm as it will be used as a reaming jig in the last operation.







4. A ball ended Allen key screwdriver eases jaw swapping.

3. Workpiece in place, to be clamped.

Also two small drill bushes will be required. These can be B.M.S. and casehardened, or Silver steel and hardened. Each is turned as a tightish fit in the counterbored hole "B" in the arm, and is drilled ,and bored if necessary to guide the tapping drill 4.2mm(M5)or 4mm(2BA). The second is drilled or bored to suit the undersized hole for the Reamer.

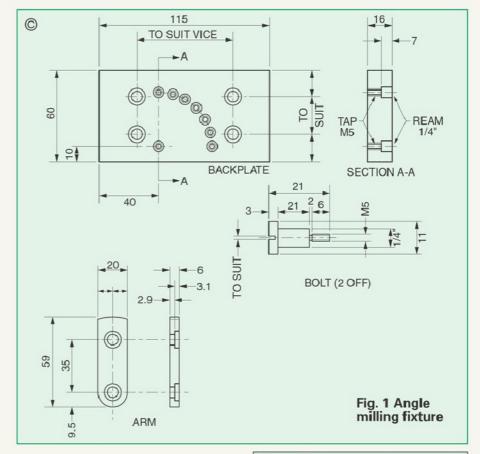
Fit the arm to the back plate such that when the pivot bolt is fully tightened there is no slop but the arm moves smoothly.

### Machining the angle holes

The holes which set the angles can be tackled in several ways, less precise or more precise depending on the degree of accuracy intended, and the equipment available.

- 1. Using a universal bevel protractor, set at 15 deg. offer up, clamp arm, fit drill bush, drill tapping size, fit second drill bush, drill undersize for reaming, remove drill bush and ream using arm. Repeat at 30, 45, 60, 75, and 90 degrees.
- 2. Using a Rotary Table.
  - A. Clamp to mill table.
  - B. Centre under mill spindle using "D.T.I."
  - C. Clamp back plate to rotary table with pivot hole aligned with spindle by use of "D.T.I." on mill table and indicating on a short stub of silver steel in the pivot hole while rotating the table.
  - D. Line up Base of Back Plate with table axis again using "D.T.I." and zero rotary table.
  - E. Offset pivot hole by 35mm, or what ever radius has been chosen. This must be accurate.
  - F. Fit arm. Line up. Fit tapping bush, clamp arm, drill. Change bush, drill, remove bush, ream.
  - G. Repeat for all angles adjusting rotary table accordingly.
- 3. Using direct indexing.

If you have a DRO on your mill, then this becomes a doddle. If you don't, all is



not lost, but you do have to keep track of the dials, and work one way to take up backlash.

For the 35mm radius suggested, the X-Y coordinates for the various positions can be calculated from basic trigonometry (X= 35 cosA, Y=35 sinA), and the figures are in Table 1.

The machining process is then very much as described earlier.

#### **Operation**

The method of use is, (Photo 3) I believe, self explanatory. It saves a lot of frustration and is quick and simple to use, making life just a little easier for us mere two handed mortals. I would, however

| TABLE 1       |             |                   |
|---------------|-------------|-------------------|
| Angle (A deg) | X(mm)<br>35 | <b>Y(mm)</b><br>0 |
| 15            | 33.807      | 9.059             |
| 30            | 30.311      | 17.500            |
| 45            | 24.749      | 24.749            |
| 60            | 17.500      | 30.311            |
| 75            | 9.059       | 33.807            |
| 90            | 0           | 35                |

recommend the purchase and use of a ball ended Alan key Screwdriver (Photo 4), which makes swapping jaws a good deal easier in confined spaces. As always, I am happy to help where I can, but phone only please. Peter Rawlinson, Charing, Kent, 01233 712 158.

# CHUCKS -HOW MANY?



1. The larger commercial chucks and one self built collet chuck.

2. The smaller chucks with heavy drilling fitment to rear, and sensitive drilling attachment in foreground.

do not class myself as a model engineer but someone who enjoys machining for interest. I make small pieces of equipment for myself and produce or repair things for other people. It keeps the mind active and the fingers supple. Before proceeding, I should note my thanks to Mr. G. Willis for providing the photographs.

The early years of my working career were spent in a workshop where the only lathe chucks were 4 jaw and somewhat larger than we are accustomed to in the amateur context. The smallest was about 12 inches in diameter and the largest several feet bigger. It was rumoured that 3 jaw chucks were only for amateurs!

In my home workshop, I now own a Harrison L5 lathe with the standard

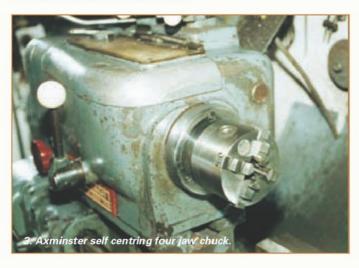
equipment of one 8 inch four jaw and one 6 inch three jaw chuck. Over the years, I have added to these, so that the collection now totals some sixteen chucks as shown in **Photo nos. 1 and 2**.

#### The collection

The first photograph shows the Pratt 8 inch and Bison 6 inch, Burnerd 5 inch four jaw, Axminster 4 inch four jaw self centring, Burnerd 3 inch three jaw and a 5 inch magnetic chuck fitted with a backplate for mounting on the boring table; also a small collet chuck I made for use in the lathe spindle Morse taper.

And in the second can be seen, identified by their numbers:

- A heavy drilling fitment in 4 M. T which after removal of the top slide is fitted to the cross slide.
- Jacobs Super chuck ¾ inch- 1 inch capacity.
- Westcott 0- % inch capacity sliding jaw chuck.
- Westcott 0- ½ inch sliding jaw chuck with large Slocombe centre drill permanently fitted
- 5. Keyless 0 ½ inch tailstock chuck.
- Cardinal 0 ½ inch secondary tailstock chuck.
- Alfred Herbert Quick chuck with collets.
- Sensitive drilling attachment for tail stock
- No 3 M.T. arbor fitted with No 3 centre drill.





Model Engineers' Workshop

#### **Applications**

The Axminster four jaw S.C. chuck is particularly useful for machining square stock. It can be seen in **Photo 3**. It also has another backplate to suit my wood turning lathe and a set of Axminster bolt-on jaws.

Having a lathe of fair capacity, it becomes possible to grip a smaller chuck in a larger. In this way, you can get down to smaller diameters as in **photo 4** where the Burnerd 3inch three jaw (which can also be fitted to my wood turning lathe) is mounted in the main three jaw, and also make a quick change to the Bison four jaw independent. As a "Pop in" this saves time on small odd shaped items to be turned (photo 5).

Having the facility to mount a four jaw chuck on the toolpost opens up various possibilities for drilling and milling operations on the lathe. The Burnerd 5inch four jaw can be seen set up in this way in **photo 6**.

The Herbert Quick chuck is a super piece of equipment. It has two parts; the main body with M. T shank and a sliding sleeve. A drill is fitted to the parallel collet and entered in the body. The sleeve is then slid forward which locks the collet in the drive position. As soon as a turning force is exerted on the drill the whole chuck locks solid and exceedingly true; the moving and locking parts are all ball bearings working on a cam action. After use slide the sleeve back, remove drill and collet . With several collets fitted with increasing sizes of drill a very rapid work rate is possible.

The Westcott sliding jaw chuck has a grip like a bulldog. This is achieved by using a screw with left and right hand threads operated by a square key, which moves the jaws. I find that keeping a centre drill on its own arbor saves a lot of time and fiddling - likewise the large Slocombe fitted to the small Westcott used for putting a radius in the end of work.

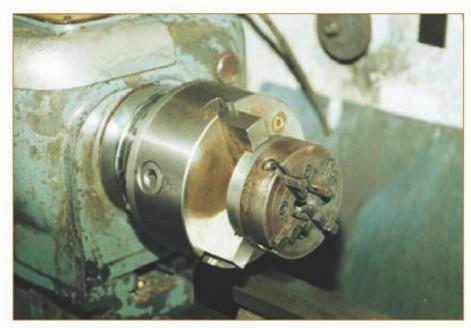
The Jacobs Super Chuck is a massive drill chuck being % inch - 1 inch capacity. It is inscribed with the dates:- September 16th 1902, January 26th 1909, June 5th 1915.

Perhaps it is nearly a hundred years old. It certainly does not look it and is in very good condition. I use it in either end of the lathe for holding milling cutters. It may not be best recommended practice, but I find it ideal for bottoming out blind holes etc.

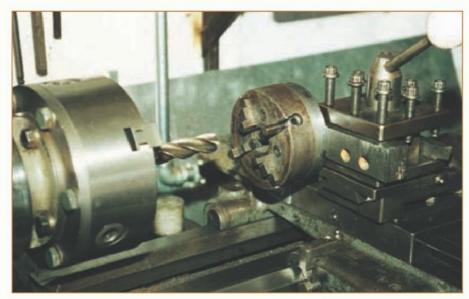
Of all these chucks I bought only the Bison and the Axminster new. All the others have been bought for as little as five, to as much as twenty pounds. Perhaps my collection is a bit O.T.T., but I find when machining repetitive work, it pays to have a row of chucks fitted with a selection of drills or cutters ready for instant use and saves much time.

### Not a chuck but still very useful

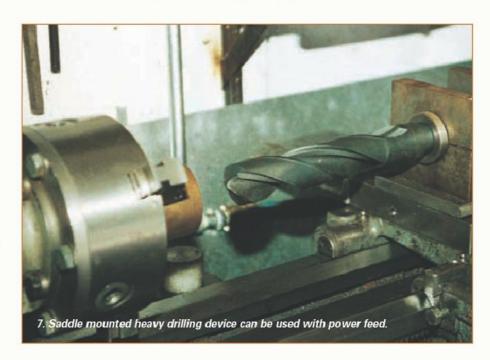
One piece of somewhat non standard kit is the heavy drilling fitment, shown in **photo 7**, being used with 32 mm drill. I use this when opening the end of a work piece, and employ the power feed to the saddle it saves much time and effort - Note the hexagon screw fitted in the end (photo 2) to eject the drill.



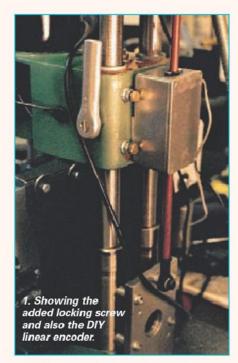
5. A four jaw piggy back gives a quick change for odd shapes.



6. Toolpost mounted four jaw allows milling/drilling operations.



# ENHANCEMENTS TO



fter building a rigid machine frame, and having worked on the cutter head to give a stiff spindle with minimal end-float, the final step towards accurate sizing of the work requires the user to make precise moves in the Z-axis. In my terminology moving the cutter vertically towards the work is a positive move. This means that a Z+ move on a knee mill is a vertically upward move of the knee, whereas on a mill-drill or sliding head machine such as Compumill a Z+ move entails moving the cutter vertically downwards.

The knee mill configuration works well in keeping the nut consistently located against the working flank of the Z-leadscrew. In contrast to this the sliding cutter head configuration has considerable mass causing the cutter head to fall away

Having covered the basic machine construction, and spindle speed variation, Richard Bartlett turns his attention first to improving Z axis accuracy, and then to ultra low budget DIY DRO's.

from the working flank of the Z-screw. This characteristic has to be known and understood before accurate sizing cuts in the Z-axis are possible. In order of simplicity some of the options for achieving this are:

### Use of the vertical adjuster

The vertical slide adjustment is by four M8 screws on the phos.bronze bushes of the twin columns. Adjusting these to increase the friction on the columns to a point where the cutter head will not slide down under its own weight will work for small cutters and/or light cuts. The interrupted cutting loads which are natural to milling can cause this light frictional locking to be overcome allowing the cutter to descend by the full amount of the backlash in the Z-leadscrew. Since careful adjustment of these screws is necessary for a 'good feel' to the slide when wound by hand, it is not practicable to adjust them after each cut.

This 'good feel' factor is a direct result of a small stick-slip characteristic. All machine slides respond to small discrete inputs in this stick-slip way, the first 1/10,000inch will NEVER produce movement of a dovetailed slide controlled by a previously unloaded acme thread. As further small inputs are made the energy is stored in the elasticity of the mechanism, at some point this 'spring energy' will overcome the static friction and the slide will move by an amount approaching the sum of the small inputs.

A high level of friction does reduce any tendency for the head to drop under cutting, but increases the stick-slip value to a level which eliminates any chance of moving in 0.0005inch increments using the index ring. Conversely, too light a setting of gib or bush adjusters will result in a minimum stick-slip characteristic but inadequate lateral location of the slide.

Adding a separate 'locking' screw to the slide allows the adjustment to be set and maintained with the additional locking force added prior to cutting (see photo 1).

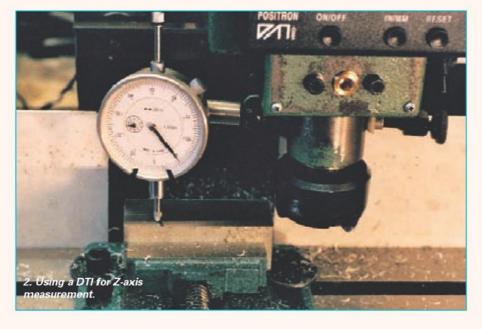
### Eliminate Backlash and Endfloat in the Z-axis

This is the first component of the ideal option, construction details were covered in previous articles and although the points were mentioned as mods to do when "CNCing your mill", the above might encourage the builder of a manual machine to incorporate them on the Z-axis at least. Eliminating backlash/end float and counter balancing the cutter head requires some extra work but is well worth the effort and together they provide the ideal solution for the Compumill configuration.

### Use of a counterbalance for the vertical head

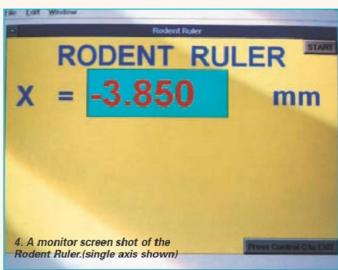
This has the advantage of reacting the vertical load of the cutter head through a point much nearer the centre of gravity of the head, as well as maintaining reliable contact between the nut and the working flank of the screw. Certainly the simplest way to achieve this counterbalance is to tap the top surface of the head casting M8 to give an attachment for a Bowden (bicycle brake) cable. Run this up to a cable 'splitter' attached to the front of the column top plate and run the outer cable over the machine well clear of the vertical feed handle to a second 'splitter' mounted on the rear of the column top plate. The wire then passes through the base and is fixed into an M8 tapping in 15Kgs of 3inch dia. steel bar or whatever sash/clock weights etc. you have to hand. Set the cable length to allow the counter balance weight to sit on a 1cm thick piece of scrap chipboard when the cutter head is at its highest. This allows easy fixing/adjusting of the weight.

The prospect of drilling another hole through my 50mm pressed granite slab base for the above 'dangler' option did not appeal, so a pneumatic cylinder is used as a constant rate spring in a similar way to the gas struts used on the rear hatch of an estate car. Note, if the pneumatic cylinder is not backed up by a relatively large



# COMPUMILL - Part 3





volume pressure tank then the counterbalance effort will not be consistent throughout the vertical travel of the head. The reservoir will need to be at least twenty times the volume of the air cylinder. The spare wheel for our camping trailer provides this, otherwise the small receiver from a commercial vehicle airbrake system is available at low cost from a breakers, a CO2 'pub-gas' cylinder would also do the job. The attachment of the wire on the vertical head is similar to the 'dangler' option with the added design luxury of being able to run the cable in any direction to the conveniently mounted cylinder. My cylinder runs down parallel to the backstay and shares the stay's mounting in the base.

The vertical head weighs approximately 12Kgs which suggested a counter weight of approx 15 Kgs, this balancing force is easily adjustable using a footpump. A relatively inexpensive range of air cylinders from RS are double acting with 25mm diameter pistons and have a range of accessories to allow the fixing of either end to any anchorage. They are available in a range of lengths, mine is 250mm max stroke from which I require 220mm actual movement. Pressures are still pounds per square inch for me so for an effective piston area of 1 x Pi/4 sq.ins to exert an effort of approx 33lbs. in 'push' mode needs (33/0.785) or 42lbs/sq.inch. From a safety point of view this is well within the capacity of standard airline fittings. Do remember that if you choose to apply the cylinder in "pull" mode the piston area has to be reduced by the piston rod area to give the effective area. This will need a slightly higher air pressure to give the same effort, but the pressures will still be fairly modest.

The valve core is removed from the spare wheel and a connection made at the valve by either tapping a brass tube fitting or using a spare "push&lock" fitting bought as a spare for a footpump. A 3-way fitting is used at the cylinder to give connection to the reservoir and an inflation point which can be a Schrader valve to

allow pressurising using a footpump. The air line between reservoir and cylinder can be any length to allow neat storage of the spare wheel. Rubber solution provides a long term seal if using a "push&lock" type of quick connector.

### Fit a linear positional indicator to the Z-axis.

This is very much the "soft option" as the machine can be used straight from the box and the sizing cuts put on while viewing the actual vertical movements, including any biasing needed to allow for the vertical component of the locking force.

#### a. Using a D.T.I.

The indicator can be as simple as a Dial Test Indicator (see Photo 2) firmly clamped to the cutter head casting and referenced to the table, fixture or work. It is used in incremental mode, which means the datum is re-established for each cut, the dti being removed whilst cutting. Since sizing cuts are likely to be less than 1mm the accuracy of a "straight spindle" clock will suffice. A "lever" type dti can be used with feeler gauges built up and checked by micrometer or vernier to equal the cut required. This is fundamentally accurate as the dti only has to repeat at its zero reading. As a dial test indicator is so useful for setting fixtures or setting the work true to the machine slides that it is almost essential equipment for milling, so this method of positional indication can almost be regarded as a zero cost option.

#### b) Linear Scales

As with most items produced in volume for world markets the cost of Inductive or Capacitive based linear scales with digital LCD readout has fallen to a level which makes them attractive for amateur use Indeed, the latest crop of Chinese capacitive scales are aimed at this market. The scales are accurate and have a typical

resolution of 0.01mm (0.0005inch). (See Photo 3) At a cost of approximately 50 pounds per 12inch axis they are very good value. Siting them on the machine needs some planning, as the display is an integral part of the measuring head. To keep them swarf free and still readable can involve quite a lot of work/imagination. Suppliers of these scales also offer remote display units with larger digits which help solve the mounting/viewing problem, this sets the cost at approx. 100 pounds per axis. In my experience the remote display is very susceptible to interference generated by switching the main spindle motor ON/OFF or driving the dc feed motors when powered from the mains adaptor, this is much better when powered from the internal 3.6v battery. All motors should be suppressed for use with these remote displays.

### c) DIY linear or angular position indicator

Being a DIY modification of something



intended for another function puts this indicator very much in tune with the rest of the Compumill project. The 'borrowed' part of this unit is the complete circuit of a serial mouse used as a pointing device with a PC computer. These are currently being offered brand new by Farnell (No. 889-1968) and CPC (No. SB0186304) for NINETY NINE pence each. The supplied lead plugs straight into the 9-pin serial COM port of a PC.

Running the 'Rodent Rules' program on any PC allows up to three position measuring devices to display linear or angular positions in LARGE clear format on the screen. This program has been written by Allan Good, a Compucutter who uses CNC woodworking machines at hobby level, and is available as a free download in 3axis form from the Compucut Users Forum. The simplest way to access the forum is to log on to the Compucut Website at

www.compucutters.com and then click the link at top left called Compucutters users forum. The program is in the Software section under "Rodent" and includes a DOS mouse driver. Anyone wishing to play with the 'Rodent Rules' but having no internet access for the download can send five pounds to COMPUCUT for the Rodent programs on CD. The address is elsewhere in this magazine. Further information will be given on the use of the software and hardware requirements in the follow up article.

**Photo 4** shows the display which allows the screen to be mounted well away from the suds/swarf environment of the machine.

Photo 1 also shows a linear encoder with a simple frictional linear to angular translator which uses a Tufnol rod and silver steel axle attached to the Z-axis of Compumill. This device has a resolution of 0.001inch and in incremental mode has an accuracy of +- 0.001inch in the range needed for this Z-axis application.

Adding a push button to the lid of the die-cast housing to actuate the right hand mouse switch on the PCB allows the display to be zeroed prior to putting on the

cut when running the Rodent Rules program. This stops any errors accumulating.

That's it, using your selection from the methods suggested above will allow accurate work to be produced on your Compumill.

The rest of this article and one which will follow in a future issue are devoted to building and testing different forms of DIY digital readouts using the serial mouse PCB. These are cheap enough to allow their dedicated use on any linear or rotary machine slides including digitising heads for the logging of CNC machining data.

#### **Suppliers**

HPC Gears 01246268080 for gears, racks and pinions.
RS Components http://rswww.com for bushes, bearings, die cast boxes

bushes, bearings, die cast boxes Farnell Electronics 08701 22 77 22 for A4Tech Serial Mice

CPC Electronics 08701 20 25 30 for A4Tech Serial Mice

### **Rodent rules**

t is most important to look at the construction of a PC mouse pointer if you have not already succumbed to curiosity and done so. Remove the mouse ball as though for cleaning and it will be seen that when the mouse is moved the silicon rubber covered ball rolls along the mouse mat surface with little or no slip. The ball is spring loaded against two axles which are set at 90 degrees to each other. This sprung loaded ball mechanism translates the linear movements in X and Y into proportional rotation of the two axles.

Removing the screw which holds the two mouldings of the outer shell together and carefully separating reveals that each axle carries a radially slotted disk. The slots are arranged to pass between an optical source (LED) and a pair of detectors (Photo transistors).

The mice from the suppliers mentioned are badged A4TECH 'fast mouse' and have a relatively high resolution at 520 lines per inch. They have 45 slots in the periphery of each encoding wheel. Other resolutions can be used by scaling the following examples to suit your serial mouse.

Before removing the plugged lead from the mouse PCB, note which way round it is connected. The four way connector is not keyed. On mine the green wire is adjacent to the opto switches.

#### The mouse PCB

The good news is that there are NO electrical modifications required to this circuitry, we use it straight out of the box! Looking at the components either side the slotted wheel, on one side a Light Emitting Diode emits a beam which is collimated by a tiny lens moulded in the end of the led, this beam will, if not cut off by one of the teeth of the slotted disk, fall upon the face of the detector which has dual sensors (A & B) that are spaced within the moulding by one quarter of the circular pitch of the slotted wheel. This spacing gives a

sequence of logic signals at A and B that are called quadrature outputs.

### The optical switches

If we assume a tooth on the slotted wheel is cutting off the beam from the detectors resulting in both outputs A and B being OFF, then by turning the slotted wheel first clockwise by TWO slots then anti-clockwise by two slots the following pattern would be detected by the electronic counting circuit. (Take 0 for OFF and 1 for ON)

START clockwise anticlockwise A 0 11001100 01100110 B 0 01100110 11001100

From the position where one tooth is completely blocking the beam, shown by A=0 B=0 to the position where the next tooth completely blocks the beam there are FOUR unique equally spaced outputs 00, 01, 11, 10, and the sequence will depend on the direction of movement of the slotted wheel. The mouse circuitry counts each change of state in A and B.

This sets the ANGULAR resolution of the mouse as:

1 COUNT = No. SLOTS in wheel \* 4

and the LINEAR resolution as:

1 COUNT = 

Effective circumference of measuring axle

No. SLOTS in wheel \* 4

Note, the above is independent of diameter of the ball. The ball simply translated linear movement into movement around the circumference of the measuring

1) The basic components of: PC plus Program plus Mouse PCB plus Slotted

axle. From this it follows that:

wheel make up an ANGULAR measuring device, and

2) By adding a linear to angular translator the system can be used for LINEAR measurement. The translator divides the CIRCUMFERENCE of the measuring axle into: (Number of slots \* 4) counts.

### Example as an angular encoder

The mouse axle/slotted wheel is set in the end of the worm of a dividing head which is fitted with a 90T wheel.

Using the 'as bought' slotted disk (45 slots) the resolution will be:

1/(45 \* 4 \* 90) of a turn of the work spindle = 1/45 degree or 1.333' minutes or 1/16200th of a work spindle turn.

This is accurate but not wildly convenient. If we used a dividing wheel of 40 teeth we would get: 1/(45 \* 4 \* 40) =1/7200 or 0.05 degrees of work rotation.

With a 90T dividing wheel, let's aim for a resolution of 1 minute of arc. This equates to 90/(360\*60) of a spindle turn. So, 90 \* ( SLOTS \* 4) = 360 \* 60

SLOTS needed = 60

I prefer to work in decimal fractions of a degree, so for a resolution of 0.01 degrees and 90T the slots required are:

(360 \* 100) / (90 \* 4) slots needed = 100

It would require a very good mechanism to support such high resolution and a more practical choice would be 0.02 degrees resolution provided by 50 slots.

#### Making slotted disks

Checking the recommended mice will show that their standard slotted disk has a circular pitch closely equivalent to a 0.4MOD gear. This circular pitch must be maintained to preserve the quadrature relationship of the outputs. Buying a standard gear with teeth equal to the number of slots required is a good start towards making an encoder if

one has no dividing equipment. Due to the difficulty in placing the PCD of a standard gear exactly on the invisible beam of the optical path to preserve the quadrature relationship, the tooth space should be deepened with a radial slot of width nominally equal to the circular pitch/2 to give a total depth of 1.5 times the original depth (1.5mm or 0.06inch).

Making the new slotted encoder disk could be as simple as sawing down the tooth space of a 0.4Module gear with a piercing saw of CP/2 blade width. A junior hacksaw blade can be stoned down to width which will remove the secondary (wavey edge) clearance to give a fine finish. Remember to fit the blade to cut on the downward 'pull' stroke. Half the circular pitch of 0.4 module is 0.63mm however the actual slot width of the standard wheels is 0.5mm (20thou) which I assume is cut to obtain quadrature phase outputs allowing for hysterisis in the opto switches, so use a saw blade of 0.5mm width unless you intend to check the phase outputs against known rotation of your specific circuit.

Producing a 90 slot encoder by hand sawing needs good light, a depth stop and some patience. The depth stop is easily made by tapping a piece of 1/2inch steel plate M5 (the bore of my gear was 5mm) at a distance from the edge to allow the saw to touch the edge of the thick plate at full depth.

Example for 90 slots: The gear has an OD of 36.8mm giving a radius 18.4, the tapping is centred 18.4 - 1.5 = 16.9mm from the edge.

### Using a mechanical

#### Sav

See photo 5 I found this method of producing slotted encoder wheels to be fairly bearable. The Taig top slide is spotted on to the table of the scroll saw with a blob of Super glue with the pivot point for the gear in line with the blade when viewed down the slide, and the angular alignment of each tooth space was done by eye with a little help from a fairly strong glass. A similar setup could be done quickly using a slitting saw in the lathe with the gear pivot mounted in the toolpost and the work fed in on the cross slide.

Obviously the accuracy of this hand slotting process will depend on the care taken, but remember that: ONE COUNT is generated by a rotation equivalent to a quarter of a circular pitch of the encoder (0.31mm) so a rotation through ONE complete tooth space is equivalent to TWO COUNTS. Any error in sawing down the centre of the tooth space is unlikely to exceed 10% of the space when bearing in mind that the gear locates the saw precisely at the start of each cut. 10% off centre would give rise to a cyclic error of (2 RESOLUTION/0.1) With a resolution of 0.001inch this equates to 0.0002inch, which should provide some encouragement for this quick and easy approach.

Once the slots are formed the disk will need to be thinned to 0.04inch. If using Polyacetyl for the disk it is important to cut

this width using a sharp HSS tool with plenty of top rake. This avoids making burrs which take forever to remove.

A light spray with matt black paint and the slotted disk is complete.

If the gears are being made from scratch then black Delrin is a good choice.

The opto assembly of slotted wheel and PCB is mounted to the machine and needs to be covered to stop extraneous light from fooling the detectors. Small diecast boxes make good housings and as the photo 1, shows, are easy to mount.

A prime application for a 'Rodent Rule' is to fix a slotted wheel into the end of the shaft carrying a worm which meshes in the Bull wheel of the lathe. This allows a very accurate and cheap method of dividing around work held 'as true as it was turned' when making gears, cams or dividing plates etc. Using the Myford bull wheel of 60T as an example and aiming for a resolution of 0.02 degrees of the lathe spindle, the slots required in the encoder would be:

(slots \* 4) = (360 / 0.02) / (60)slots = 75

Returning to the application in hand, which is to display the sizing cut on the Z-axis of Compumill. This is a linear application and will require some form of 'LINEAR TO ANGULAR TRANSLATION' as performed by the ball in the original mouse pointer.

In the next article we will address various solutions to this "Translation" question, and the use of Rodent Rules.

### A brief note on steel specifications

or readers involved professionally in engineering, the following notes may be "Old Hat", however from the telephone queries received to the editorial office, it seems that an outline explanation may be in order. Back in the 1950's, The British Standards Institution published B.S.970: 1955 which presented a standardised range of steels – the En series. This was then rewritten in 1983 as the British six character system which in theory has already been replaced, although just about everyone in the UK still uses one or other of the B.S.970 systems.

### The 1983 System

This system uses six characters, grouped as three numbers, one letter, and two numbers.

The first three numbers denote the general type of steel:

000 – 199 Carbon and Carbon Manganese steels where the figures indicate the manganese content.

200 - 400 Free cutting steels where the second and third figures indicate sulphur content.
 250 Silicon - manganese spring steels.

300 – 499 Stainless and heat resisting steels

500 - 999 Alloy steels

The fourth character is a letter which for stainless steels will be "S", and for others

will be either "M, A, or H". For non stainless steels this relates to the condition of supply.

M indicates specified mechanical properties, e.g. tensile strength, yield strength, % elongation, etc.

A that the metal has been supplied to a closely controlled chemical composition.

H that the steel conforms to hardenability requirements.

The fifth and sixth characters are numbers and for non stainless steels, show the mean carbon content.

Thus as an example, 070M20 is a non alloy steel having a manganese content around 0.7%, a carbon content around 0.2%, and having specific mechanical properties rather than chemical composition.

Suffix letters may be added in certain cases either to indicate chemical additions (e.g. lead Pb) or that the material has been heat treated to a particular condition (typically T)

## Steels for the Amateur Workshop

While there is a great multiplicity of steel specifications, a relatively small number will satisfy the majority of needs. For machining work, the following are readily available in bright bar form, some also in hex, square, and flat.

For low stressed parts it is sensible to

make the machining process as easy as possible and use a free machining steel. One very popular and readily commercially available is EN 1A or 230M07 also available with a slight addition of lead or lead and tellurium in which case the suffix Pb or PbTe is added to the specification. The freecutting steels are not generally recommended for welding.

Moving up the strength range a little, En 8 (080M40) or its free machining variant En 8 DM (212A42) have a higher strength than En 1A, and may be further heat treated.

For even higher stressed components, En 19 (708M40) is a chrome-moly steel, and En 24 (817M40) is a nickel-chromemoly steel. Both of these are available hardened and tempered to the "T" condition, having a tensile strength of 55-65 tons/sq.in. eg En 24T (817M40T) For those wishing to delve further into the many varieties of steels, Macreadys, (phone 01788542 191) are one of the largest UK steel stockholders/distributors, and publish the "Orange Book" price £15-00 which has gained a reputation as a steel users bible, extending to over three hundred pages, covering carbon, alloy, stainless, tool, silver and spring steels as well as bronze bars and cast iron. In addition, their wall charts, produced in conjunction with Castrol and Kennametal Hertel give excellent summary information on properties, machinability, and choice of tooltips and coolants.

November 2002

# SCRIBE A LINE

#### **Hardness Tester**

#### Mr W. T. Glenn from Dundee writes:

The "novel hardness tester" mentioned in the *Scribe a Line* section in MEW issue No 84 by Prof. R. F. Cane, had me make a bee line to the box my seventy-six year old mind told me I should find it. My tester, like his, has a range of Rockwell "C" scale 46 – 62 in 2 unit intervals. I write this letter for a number of reasons. First to mention that moulded into the gauge housing on the same side as the scale numbers is "Pats. Pending Prov. No 26443". Such information may help one of our current small firms looking for a new product. The accompanying **photo 1** shows the "spoked device" and the two parts of the Bakelite case.

Second, to thank Philip Amos and his like for helping to give us a wonderful magazine.

Finally, other readers may be interested in a small modification to my Myford 7. As a firm believer in regular oiling, I found that surplus oil found its way from the rear headstock bearing on to the pulley and thence to the belt, eventually causing degradation and slip. A new belt was fitted, and a "flinger ring" made in two halves and attached to the pulley. **Photo 2** shows the general arrangement. Now, even if I get a little over enthusiastic with the oil gun, the belt drive stays dry.





### What was it? – The Answers

### Mr A. Rowland from Formby writes:

Under *Scribe a Line (issue 84)* Mr K. P. Kleiser is puzzled as to the purpose of the small gauge illustrated.

The instrument is similar to devices used in military target rifle shooting some years ago. These were used to adjust the simple military rifle sights in steps of one minute of angle, so giving the rise or fall of the bullet on the target as one inch per 100 yards of range. Several designs were used, but typically the instrument was hooked under the sliding part of the sight and moved up or down with the adjusting screw. The presence of the vernier

graduations would give an accurate reading irrespective of screw backlash.

Various models by manufacturers such as O'Hare, and Lyman Gun Sight Corp. are illustrated and described in the book "Military and Sporting Rifle Shooting" by Edward Crossman, and published in the U.S.A. in 1932.

Modern rifle sights have the micrometer principle built into the sight, with clicks indicating elevation changes of one quarter minute of arc.

### Mr C. A. Currie from Bath writes:

The item in SAL iss 84 is nothing to do with clock and watchmaking. It is in fact a vernier adjustment for ladder type rear sights on rifles used for target shooting. This type of rear sight was universal on most military and many civilian rifles both before and after 1900.

The rifle sight was coarsely graduated in steps of 50yds from 50 to 1000, and the vernier gauge was used to fine tune the sight to a particular rifles characteristics. By recording the vernier readings for actual ranges, the sights could be adjusted and repeated for any setting.

In use the screw controlled the elevation, and the slotted link controlled windage. These adjustors were made with slight variations by most of the large gunmakers.

I hope Mr Kleiser looks after his adjustor as it is a nice reminder of a golden age before the sport became the victim of philosophically bankrupt politically correct politicians.

Mr Arthur Chankin of Hartsdale, N.Y. wrote with details of a similar tool made by O'Hare, and asking "What is it". The above would seem to provide the answer. Mr Peter Jackson of Knaresborough also wrote offering the "rifle sight vernier" identification.

#### **Milling Advice**

#### Mr. M. A. Delaney from Oakville, Ontario, writes:

Having had similar experiences to those of Mr. Hall "Milling machine projects for beginners (1)", Model Engineers Workshop No.84. August September 2002. I find myself not so much at odds with the author as wishing to amplify some of his information. Much of this additional material is based on bitter experience, some of it costly, but fortunately not irreparable.

First; one must never try to mill using a drill chuck no matter how much it is tightened The reason is not only will the mill be pulled out of the chuck, but the chuck will come loose from the mandrel. The "Jacobs" series tapers used for drill chucks are short and relatively steep. The rotating vibratory load applied by a milling cutter will soon work it loose.

Second: All milling cutter holders, set screw, collet or "Clarkson", that are attached to the spindle with "Morse" tapers, must be retained by suitable draw bars. Even these slow tapers will work free

over time. Murphy says they will hang on until during the last finishing cut.

Third: Never climb mill! Mr. Hall explains the reason; it is backlash. You can adjust as much as you like. but with a worn lead screw, you will still not be able to avoid a crash when hand feeding. My technique to get the improved finish that the production people get on their C.N.C. machines is to wind the work back slowly with the cutter running but no change in the cutter position. On my small home machines there is always just that tiny bit of spring that takes the lightest possible amount off on the way back.

Fourth: Have the quill and the non feeding slide locked during every cut. Vibration will move any unlocked feature at some time. Ball handles are seldom truly balanced.

Regarding cutters and holders, I accept that I can only speak for my part of North America, but I have measured the %in. shanks of all my cutters; some 20 plus, that come from all parts of the world, and carry cutting diameters from 1/2 in. to 1/2 in. in two and four flute types. The beautifully ground shanks are all the same size as near as I can tell with my tenths micrometer. Also, how much run out is acceptable? All it does is make a very small difference to the feed rate from tooth to tooth. I mostly use set screw type plain holders, being careful to engage the set screw in the flat on the shank and checking it after the first cut. My %in. holder was purchased finished for very little money( the equivalent of about £5-00) courtesy of the fine factories in India. The 1/2 in. dia. I made from a Morse taper blank with a one inch dia. by one inch long end, by mounting it in the lathe spindle and drilling and reaming the hole. Both have the small end of the taper tapped %in. U.N.C. for the draw bar. For the smaller shanks on the mills below 1/sin. dia, I have made a series of bushes all %in.O.D. and reamed inside ¼in. ¾in. ¼in. and ‰in. Each is fitted with a set screw. I also have a series of collets, bought when on sale, sized from 1/8 in. to 1/8 in. by 1/8 in. steps, that fit into a No. 3 Morse taper. They are operated by a draw bar and are fine for milling cutters and drills.

I hope Mr. Hall will mention coolant/lubricant in a future article. I have particular problems in this field, as my workspace is indoors, so that smell and smoke is not acceptable.

### And continuing on coolant

#### Dyson Watkins from Swansea writes:

Mr. Sylvester mentioned in M.E.W. issue 81a blue cutting coolant. It could possibly be a type that I used about eight years ago in trials that I conducted in continuous production of gearbox parts. The coolant was greatly superior to the common sulphurised water soluble coolant we called "suds". Sulphurised cutting oil has an unpleasant smell, and over a period of time attacks components such as rubber seals, and paint used on many machine tools except stoved finishes. The blue cutting coolant called "Metosol 506" had a pleasant smell, gave an increased tool

life and therefore an improved productivity. The downside was a higher initial cost. It was diluted with water to a strength of approximately 5%, always adding Metosol to water - Never water to Metosol, otherwise an emulsion would not form. More details can be found on the internet by looking up the name "Metosol" or www.petrokimiagresig.com or Metolube. It does not attack machine paints to the same degree as "suds". Like suds however it will break down if lubricating oil is allowed to leak into it. This forms an air seal over the emulsion, and bacterial breakdown will occur due to the anaerobic conditions which are then formed. Other than that it is good stuff. Hope this info will be of help.

## Retirement complexes and workshops

# Mr. W.A. Brading, of Auckland, New Zealand, writes:

I read with interest your editorial comment on the demand for workshop facilities within retirement complexes and offer my experiences on retiring to such a location in New Zealand.

I am a retired professional electrical engineer and have enjoyed model engineering, in particular 5-inch gauge steam locomotive and rolling stock construction for very many years even before retirement. When the time eventually, and long put off, came to retire, my wife and I were faced with the dilemma that you describe in your editorial column of August 2002. I certainly did not want to give up my main hobby nor dispose of the tools acquired over half a lifetime.

Happily, in New Zealand, the demand for the pursuance of hobbies of all types is very strong among potential retirees and the need has been met over the last decade in many retirement complexes by generous provision of working space among the central facilities of such schemes. Here I must add that I prefer the word "complex" to "home" in such context. A brief description of the facilities offered in our "village" is offered below and this is by no means unusual in this country.

Our village comprises 100 houses of I, 2, or 3 bedrooms, many with single or double garages and a separate central block with administrative office with lounges and restaurant. We have a library, gymnasium and heated indoor swimming pool with snooker and games rooms. But, best of all, there are three "craft rooms", each of about 150 square metres in extent. One is for art (there is a non-resident teacher), another is for pottery, weaving and the like, and the third is for wood and metal work. In there we have two enthusiasts, namely myself and another equally keen with his woodworking lathe and tools. I have my Myford Super Seven and other machines installed with perfect confidence that that they are for my exclusive use and the room is secured after hours by the Management. I shall shortly be augmenting this with a Myford VMB milling machine. Since moving into this superb environment five years ago my hobby activity has blossomed. In there I have completed the

John Wilding % second clock and several other smaller projects in metal and wood including a case for the clock, which has now been running for over two years. Interest in the "goings-on" in this hive of activity is such that among both the other residents and the Management the enterprise is known as the "Engineering Department" so that we do receive requests for the odd repair job. We let it be known that miracles can take a bit longer.

I should add that all this may sound expensive but having just returned from a visit to the UK where we were both born I can assure you that this sort of thing is available for just about the UK average house price. Our monthly levy, which includes local rates and taxes and water as well as lawn maintenance and use of all the central facilities amounts to about £100 per month.

Incidentally I am aged 81.

#### Mr. L.I. Varty of Pickering, North Yorkshire writes:

I was surprised to read your item on Retirements Homes and Workshops in the Editorial of the August/September edition, as my own thoughts have mirrored yours for the last 18 months. My own mental ramblings have possibly gone a little further.

My own ideas envisage a large residence with a reasonable amount of mature land, preferably rural, but near to a larger conurbation. Such a home would need to be managed by one of the recognised care organisations, but it would be the additional facilities of workshops that would be of interest to the craftsman. I say craftsman, for it may be reasonable to included wood workers in the scheme of things! Also should there be craft rooms for any resident wives? No doubt a large house of the right character would have stables blocks or similar suitable for conversion. The possibility of small bungalows in the grounds for married couples would be attractive.

Machinery is unlikely to be a problem as prospective residents would no doubt donate their own equipment. So too with models, but this implies somewhere to operate them. Should there be a dual 7½/5inch track? Would one cater for smaller gauges? Would there be a model railway room? Out in the grounds there may need to be some form of road system for model steam road vehicles and possibly a model boat pond!

The question of funding of this side of the accommodation would need attention as it would be unfair to place all of the cost on the operation of the Home itself, but with suitable attention to layout of the grounds, public access may be viable for (say) Sunday public running. If the facilities could be made available to a local club, this would provide a core of younger people to assist in this way. They may even appreciate the experience of some of the older residents! Additional support funding may be possible through raffles at the major exhibitions.

Finally, where do we place this Home? May I suggest that the aim would be ultimately to have possibly five regional Homes to give reasonable accessibility to people and their relatives.

I am sure that other people will have different thoughts, but don't hang about - time is ticking by!

# TO HELP YOU GET THE BEST FROM THE MODEL ENGINEER EXHIBITION

These notes are written purely for guidance. Full information is contained in the Competitors' Information booklet which is sent to every entrant as part of the information package. If you have an item and are unsure as to the Class into which it should be entered, leave that section blank and we will take care of it. The Judges have the right to move any competition exhibit into another dass if they feel that by doing so its chances of gaining higher marks or a more appropriate award are improved.

If the item is offered as a Loan exhibit please indicate this by writing Loan on the form in the box identifying the Class. Loan models are not judged but carry all other privileges associated with competition entries.

Part built models are particularly welcome in the Loan Section; visitors like to see work in progress, and entry does not preclude the item being entered in competition when completed.

The classes listed below are those associated with mainstream model engineering.

#### Club exhibits

Where a club is exhibiting, each model should be entered on a separate entry form and clearly identified as a club exhibit by entering Loan/Club in the class section box. This ensures that we have a full record of all models on display during the show and facilitates matters of administration and insurance.

#### **Additional forms**

If you do not wish to deface your copy of the magazine we are happy to receive photocopies of the entry form, one for each model. We will be pleased to send out extra forms if required, so if you know of a modeller who is not a reader of one of our magazines but who you think may wish to participate, please advise them to contact our Exhibitions Office (01322-660070), or simply photocopy the entry form for them.

The success of the show depends largely on the number of models on display. Your work could well be the stimulus which inspires someone else to start in the hobby. There can be no doubt that this event is our showcase on the world of modelling in all its aspects. Every modelling discipline needs more and more participants, and it is by displaying not only the crème-de-la-crème, but also examples of work of a more achievable standard, that people are encouraged to join into the wonderful world of modelling, in whatever aspect.

We look forward to seeing a sample of your work at the show!

#### **COMPETITION CLASSES**

#### **Engineering Section**

- A1 Hot air engines.
- A2 General engineering models (including stationary and marine engines).
- A3 Internal combustion engines.
- A4 Mechanical propelled road vehicles (including tractors).
- A5 Tools and workshop appliances.
- A6 Horological, scientific and optical apparatus.
- A7 General engineering exhibits not covered by the above

#### **Railway Section**

- BI Working steam locomotives 1in scale and over.
- B2 Working steam locomotives under 1in scale.
- B3 Locomotives of any scale, experimental, freelance or based on any published design and not necessarily replicas of full size

- prototypes, intended for track duties.

  B4 Scratchbuilt model locomotives of any scale, not covered by classes Bl, B2, B3, including working models of non-steam.
- including working models of non-steam, electrically or clockwork powered steam prototypes. B5 Scratchbuilt model locomotives gauge 1
- (10mm scale) and under.
- B6 Kitbuilt model locomotives gauge 1 (10mm scale) and under.
- B7 Scratchbuilt rolling stock, gauge 1 (10mm scale) and under.
- B8 Kitbuilt rolling stock, gauge 1 (10mm scale) and under.
- B9 Passenger or goods rolling stock, above 1in scale.
- B10 Passenger or goods rolling stock, under 1in scale.
- B11 Railway buildings and lineside accessories to any recognised model railway scale.
- B12 Tramway vehicles.

#### **Marine Models**

- C1 Working scale models of powered vessels (from any period). Scale 1:1 to 1:48
- C2 Working scale models of powered vessels (from any period). Scale 1:49 to 1:384
- C3 Non-working scale models (from any period). Scale 1:1 to 1:48
- C4 Non-working scale models (from any period). Scale 1:49 to 1:384
- C5 Sailing ships and oared vessels of any period working.
   C6 Sailing ships and oared vessels of any
- period non-working.
  C7 Non-scale powered functional models
- C7 Non-scale powered functional models including hydroplanes.
- C8 Miniatures. Length of hull not to exceed 15in for 1:32 scale; 12in for 1:25 scale; 10in for 1:16 scale; 9in for 1:8 scale. No limit for smaller scales.
- C9 For any model boat built from a commercial kit. Before acceptance in this class the kit must have been readily available for at least 3 months prior to the opening date of the exhibition and at least 20 kits must have been sold either by mail order or through the retail trade.

#### Model Horse Drawn Vehicle Section

G1 Carriages & other sprung vehicles.
(Omnibuses, trade vans etc.) Wagons,
carts and farm implements. Caravans.

#### Junior Section

- J1 For any type of model, mechanical or engineering work, by an under 14 year old.
- J2 For any type of model, mechanical or engineering work, by an under 16 year old.
- J3 For any type of model, mechanical or engineering work, by an under 18 year old.

All entries will be judged for standard of craftsmanship, regardless of the modelling discipline, i.e. a boat will not be competing against a military figure. Providing a model attains sufficient marks it will be awarded a

gold, silver or bronze medals

#### Model Vehicle Section

- K1 Non-working cars, including small commercial vehicles (e.g. Ford Transit) all scales down to 1/42.
- K2 Non-working trucks, articulated tractor and trailer units, plus other large commercial vehicles based on truck-type chassis, all scales down to 1/42.
- K3 Non-working motor bikes, including push bikes, all scales down to 1/42.
- K4 Non-working emergency vehicles, fire, police and ambulance, all scales down to 1/42.
- K5 Non-working vehicles including small commercial vehicles (e.g. Ford Transit). Scale from 1/43 or smaller.
- K6 Any available body shells including Concours, in any scale or material, to be judged on appearance only.
- K7 Functional model cars/vehicles which must be able to move under its own power of any type. Can be either freerunning, tethered radio controlled or slot car, but must represent a reasonable full size replica

#### DUKE OF EDINBURGH CHALLENGE TROPHY

Rules and Particulars

- The Duke of Edinburgh Challenge Trophy is awarded to the winner of the Championship Award at the Model Engineer Exhibition.
- The trophy remains at all times the property of Nexus Special Interests.
- 3. The name of the winner and the date of the year in which the award is made will be engraved on the trophy, which may remain, at the discretion of Nexus Special Interests Ltd, in his/her possession until required for renovation and display at the following Model Engineer Exhibition.
- Any piece of model engineering work will be eligible for this Championship Award after it has been awarded, at The Model Engineer Exhibition, a Gold or Silver medal by Nexus Special Interests Ltd.
- No model may be entered more than once.
- Entry shall be free. Competitors must state on the entry form:
   (a) That exhibits are their own bona-fide
  - (a) That exhibits are their own bona-fid work.
  - (b) Any parts or kits that were purchased or were not the outcome of their own
  - (c) That the model has not been structurally altered since winning the qualifying award.
- Nexus Special Interests Ltd. may at their sole discretion vary the conditions of entry without notice.

#### **COMPETITION RULES**

- Each entry shall be made separately on the official form and every question must be answered.
- Competition Application Forms must be received by the stated closing date.

LATE ENTRIES WILL ONLY BE ACCEPTED AT

#### THE DISCRETION OF THE ORGANISERS.

- Competitors must state on their form the following:
  - (a) Insured value of their model.
  - (b) The exhibit is their own work and property.
  - (c) Parts or kits purchased.
  - (d) Parts not the outcome of their own
  - (e) The origin of the design, in the case of a model that has been made by more than one person.

NOTE: Entry in the competition can only be made by one of the parties and only their work will be eligible for judging.

- Models will be insured for the period during which they are in the custody of Nexus Special Interests Ltd.
- A junior shall mean a person under 18 years of age on December 31<sup>st</sup> in the year of entry,
- Past Gold and Silver medal award winners at any of the exhibitions promoted by Nexus Special Interests Ltd. are eligible to re-enter their model for the 'Duke of Edinburgh Challenge Trophy.'

Past winners at any of the exhibitions promoted by Nexus Special Interests Ltd. will not be eligible for re-entry into the competition unless it has been substantially altered in any way.

- Nexus Special Interests Ltd. reserve the right to:
  - (a) Transfer an entry to a more appropriate class.
  - (b) Describe and photograph any models entered for competition or display and to make use of any such photographs or descriptions in any way they may think fit.
  - (c) Refuse any entry or model on arrival at the exhibition and shall not be required to furnish a reason for doing
- 8. Entry into the competition sections is not permitted by:
  - (a) Professional model makers
  - (b) Anyone who has a financial interest in the direct supply of materials and designs to the public.

NOTE: If unsure, please contact the Competition organisers, prior to the show.

- The judges' decision is final. All awards are at the discretion of the judges and no correspondence regarding the awards will be entered into.
- Exhibitors must present their model receipt for all models collected at the end of the exhibition and sign as retrieved.
- The signed release for each model must be presented to security staff when leaving the exhibition complex with display model(s) after the close of the exhibition

IMPORTANT NOTE PLEASE MAKE COPIES, INCLUDING PHOTOGRAPHS, OF ALL INFORMATION RELATING TO YOUR MODEL, AS NEXUS WILL NOT ACCEPT LIABILITY FOR ANY LOSS

**CLOSING DATE 16TH DECEMBER 2002** 



# THE MODEL ENGINEER

ENTRY NO.

**EXHIBITION** 

Please return completed form to: Model Engineer Competition, The Leys, Church St., Twyford, Bucks. MK18 4EU

# CLASS ENTRY NO.

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# ENTRY FORM - COMPETITION & LOAN MODELS

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|   |  |
| Post Code Daytime Tel:  |  |
| Model Club or Association   |  |
| Have you entered before? (Y/N) Do you purchase or subscribe to a Nexus magazine? (Y/N)  |  |
| How many years have you been a modeller?  |  |
| Mail Order Protection - please tick this box if you would prefer not to receive mail from other companies which may be of interest to you |  |
| MODEL DETAILS - PLEASE TICK BOX IF MODEL IS FOR LOAN  |  |
| Entry Class (competition entries only)  |  |
| Model Title (to be used for catalogue and display card)   |  |
|   |  |
| Model Description   |  |
|   |  |
|   |  |
| Model Scale Length Width Height Weight  |  |
| Type of construction  |  |
|   |  |
|   |  |
| Parts not made by you and commercial items  |  |
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Mr A.D. Jones, Drummond Round Bed la the.

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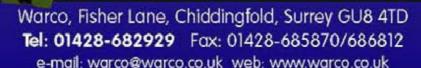
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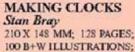
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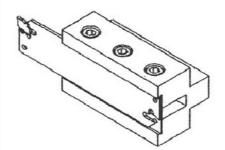
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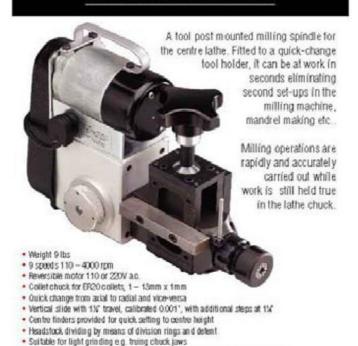
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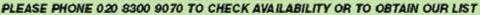
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| ADDOOK AND SHIFLET BIS Horizonative risal Head, 30" x 8" governed table and feed gears, oce<br>BOXFORD VMSD variable speed (30 Bit head, but be 21"x' x 8" a shawcod vice and collect chock.<br>BR DGEP OR T Servise 1 - 2 HP Visrible speed R8 head, powered (grast bot) table, 45" x 9".<br>BR DGEP OR T Set head 2 speed (above motor) head, R8 powered (grast bot) table, 42" x 9" to<br>Very CENTEC 28 Horizonati, 1" arbor, table powered, 3 ph motor single phase main motor.<br>CENTEC 28 Verdoutherborrad, quif feed 28"T head, 26" x 8" table, pediestal model:<br>ELLIDT DGWNHAM minis boret, very late machine complete with collects and dhistic feed with feed 28" x 9" table.   | £1,950<br>£2,250<br>able<br>rice £2,250<br>£1,400<br>ad) £2,250<br>at in £1,850   |
| ADDOOK AND SHIFLET IIIS Horizonative/roal Head, 30" x 8" powered table and feed pears, oce<br>BOXFORD VMID variable speed / 30 MT head, table 21"\"\" x 6" + alwood vice and collect chock.<br>BRIDGEP ORT Series 1 - 2 HP Variable speed RS head, powered (gearbox) table, 42" x 9" -<br>SRIDGEP ORT Set Head 2 speed (after motion) tead, R8 powered head, variable speed 42" x 9" s<br>Very CENTEC 28 Horizonati, 1" artice, table powered, 3 ph motion skiple phase main motion.<br>CENTEC 28 Vertica/Horizonati, quill feed 29"NOT head, 26" x 5" table, pedestal model:<br>ELLIOT SOW OWNHAM mis boret, very later machine complete with collect and child (sower down fee<br>ELLIOT SOY OWNIMILL 3 Motion taper qu'il universal head, 26" x 5" x 7"\"\"\"\"\"\"\"\"\"\"\"\"\"\"\"\"\"\"\  | £1,950<br>£2,250<br>able<br>rice £2,250<br>£1,400<br>ed) £2,250<br>et in £1,850<br>£1,500   |
| ADDOOK AND SHIFLET IIIS Horizonative roal Head, 30" x 8" governed table and feed gears, cool BOXFORD VMID variable speed (30 NT head, table 21" x 8" + altwood vice and collect check. BICOGEP OR 1 Series 1 - 2 MP Variable speed (80 head, powered (gearbox) table, 42" x 9" to BICOGEP OR 1 Set head 2 speed (after motion) head, RR governed head, variable speed 42" x 9" to Very CENTEC 28 Heritonial, 1" artor, table powered, 3 ph motic single phase main motion. Very CENTEC 28 Vericas/Horizonial, quil feed 281T head, 26" x 6" table, pediestal model ELLIOT DOWNHAM mine bornt, very late machine complete with collect and thick (sower down fee ELLIOT DOWNHAM mine bornt, very late machine complete with collect and thick (sower down fee ELLIOT TOP 00" OMNIMILL 3 Morret taper quill universal head, 26" x 7" y" powered table. Just ELLIOT TURINET M.L. NR- 30 speed 70-3000 pm, table 45" x 90" (governed table and | £1,950<br>£2,250<br>able<br>rice £2,250<br>£1,400<br>ad) £2,250<br>it in £1,850<br>£1,500<br>best mand<br>flow £1950  |
| ADDOOK AND SHIFLET IIIS Horizontative/roal Head, 30" x 8" powered table and feed pleans, oce BOXFORD VMID variable speed /30 lift head, table 21%" x 6" + alwood vice and collect chock. BRIDGE ORT Series 1 - 2 HP Variable speed RS head, powered (gearbox) table, 42" x 9" - 8RIDGE ORT Series 1 - 2 HP Variable speed 42" x 9" in RIDGE ORT Series head 2 speed (after motion) tead, R8 powered head, variable speed 42" x 9" in Very CENTEC 28 Horizontal, 1" artice, table powered, 3 ph motion skiple phase main motion. CENTEC 28 Vertical/Horizontal, quili feed 29/17 head, 26" x 6" x 6" table, pedestal model ELLIOT DOWNHAM mis boret, very later machine complete with collect and child (sower down fee ELLIOT 90" CMINIMILL 3 flores taper qu'il unamental head, 26" x 7" y" powered table Jul ELLIOT TIMBELT ML, I NR-10 speed 70-3000 (mm, table 45" x 7" y" powered table Jul ELLIOT TIMBELT ML, I NR-10 speed 70-3000 (mm, table 45" x 7" y" powered table Jul ELLIOT TIMBELT ML, I NR-10 speed 70-3000 (mm, table 45" x 0" table, full coolant tray and cable All fills on horizontal, 31" x 6" powered table Jul All fills on horizontal, 31" x 6" powered table Jul All fills on horizontal, 31" x 6" powered table   | £1,950<br>£2,250<br>able<br>rice £2,250<br>£1,400<br>ed) £2,250<br>ft in £1,890<br>£1,500<br>dow £1540<br>6585  |
| ADDIOCK AND SHIFLET IIIS Horizonative roal Head, 30" x 8" governed table and feed gears, cool BOXFGRO VMID variable speed (30 NT head, table 211½" x 8" abwood vice and collect chack. BRIDGEP OR T Series 1 - 2: HP Variable speed RS head, powered (gearbox) table, 42" x 9" to RRIDGEP OR T Series 1 - 2: HP Variable speed RS head, powered (gearbox) table, 42" x 9" to Very CENTEC 28 Heritonial, 1" artor, table powered, 3 ph motor single phase main motor. CENTEC 28 Vericas/Horizonial, quil feed 291 T head, 25" x 5" table, pediestal model ELLIDT DOWNHAM minis boret, very late machine complete with collects and shruk (power-down fee ELLIDT DOWNHAM minis boret, very late machine complete with collects and shruk (power-down fee ELLIDT TO-OWNHAM. 2 Micros taped 70-0000 mm, table 45" x 10" (powered table. ELLIDT TRUBET MILL RS-10 speed 70-0000 mm, table 45" x 10" (powered).  EMCO FB2 Verical 6 speed quil bed head; 26" x 10" (powered).  J phase and does not like a committee to only.  NARRISON horizontal, 3" x 6" powered table.  | £1,950<br>£2,250<br>£1,400<br>£1,400<br>£1,500<br>£1,500<br>£1,500<br>chet stand<br>60w £1,500<br>£1,500  |
| ADDOOK AND SHIFLET IIIS Horizontative roal Head, 30" x 8" powered table and feed pears, oce BOXFORD VMID variable speed / 30 lift head, table 21%" x 6" v altwood vice and collect chock. BIX DGS PORT Series 1 - 2 MP Variable speed file head, powered (gearbox) table, 42" x 9" x 8R DGS PORT Series 1 - 2 MP Variable speed file head, powered (gearbox) table, 42" x 9" x Very CENTEC 28 Horizontal, 1" after, table powered, 3 ph motor single phase main motor. Very CENTEC 28 Verticative roal, quilifierd 290 T head, 26" x 5" table, pediestal model ELLIGIT DGWNHAM mis borst very late machine complete with collects and of unk (governdown fer ELLIGIT DGWNHAM mis borst very late machine complete with collects and of unk (governdown fer ELLIGIT THREET MLL, 18% to speed 70-3000 pm, stable 45" x 7" y powered table unk (ELLIGIT DGWNHAM mis borst per quil the unknematined, 26" x 7" y powered table unknematined of preed quilt liked head? MT, powered 24" x 6" table, full coolant tray and cet a phase and does not tile a commenter to colly.  HARRISON NOTRORAL 31" x 6" gowered table  HARRISON NOTRORAL 30 INT which head 6 clubs, 30" x 6" table/powered.   | £1,950<br>£2,250<br>able<br>rice £2,250<br>£1,400<br>ed) £2,250<br>it in £1,850<br>£1,550<br>chet stand<br>fow £1540<br>655<br>£1550<br>£1550   |
| ADDIOCK AND SHIFLET IIIS Horizonative roal Head, 30" x 8" governed table and feed gears, cool BOXFGRO VMID variable speed (30 NT head, table 211½" x 8" abwood vice and collect chack. BRIDGEP OR T Series 1 - 2: HP Variable speed RS head, powered (gearbox) table, 42" x 9" to RRIDGEP OR T Series 1 - 2: HP Variable speed RS head, powered (gearbox) table, 42" x 9" to Very CENTEC 28 Heritonial, 1" artor, table powered, 3 ph motor single phase main motor. CENTEC 28 Vericas/Horizonial, quil feed 291 T head, 25" x 5" table, pediestal model ELLIDT DOWNHAM minis boret, very late machine complete with collects and shruk (power-down fee ELLIDT DOWNHAM minis boret, very late machine complete with collects and shruk (power-down fee ELLIDT TO-OWNHAM. 2 Micros taped 70-0000 mm, table 45" x 10" (powered table. ELLIDT TRUBET MILL RS-10 speed 70-0000 mm, table 45" x 10" (powered).  EMCO FB2 Verical 6 speed quil bed head; 26" x 10" (powered).  J phase and does not like a committee to only.  NARRISON horizontal, 3" x 6" powered table.  | \$1,950<br>\$2250<br>\$16e<br>\$12,250<br>\$1,400<br>\$1,2250<br>\$1,100<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1, |
| ADDOOK AND SHIFLET BIS Horizonative roal Head, 30" x 8" governed table and feed gears, oce SOXFORD VMSD variable speed (30 fit head, table 21" x 8" a shwood vice and collect chock. BR DOEP OR 1 Seriest 1 - 2 HP Variable speed RS head, powered (grantox) table, 42" x 9". BR DOEP OR 1 Seriest 1 - 2 HP Variable speed RS head, powered (grantox) table, 42" x 9". CENTEC 28 Horizonat, 1" artor, table powered, 3 ph moral single place main moral. CENTEC 28 Vertical Properties, quill feed 28" t 1" and 28" x 9" also, pedestal model. ELLIDT DOWNHAM ministore, very late machine complete with collect and chick (power-down fee ELLIDT 9" OWNHILL 3 Moral speed quill seed head 2" x 9" x 7", powered also be ELLIDT TUTION THE MILL RS-10 speed 70-3000 pm, table 45" x 9" (powered). BY ELLIDT TUTION THE MILL RS-10 speed 70-3000 pm, table 45" x 9" (powered). BY HEAD STAND AND AND AND AND AND AND AND AND AND  | \$1,950<br>\$2,250<br>\$16e<br>rice \$2,250<br>\$728<br>\$1,1400<br>ed) \$2,250<br>\$1 in \$1,800<br>\$1,500<br>\$6e \$1,800<br>\$1,500<br>\$6e \$1,800<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,          |
| ADDOOK AND SHIFLET IIIS Horizontative roal Head, 30" x 8" governed table and feed gears, cool BOXFORD VMIO variable speed (30 NT head, table 21%" x 6" + altwood vice and collect chack. BILDGE ORT Series 1 - 2 MP Variable speed (8) head, powered (gearbod) table, 42" x 9" to BILDGE ORT Series 1 - 2 MP Variable speed (8) head, powered (gearbod) table, 42" x 9" to Very CENTEC 28 Heritontal, 1" artor, table powered, 3 ph motor single phase main motor.  CENTEC 28 Verical/Horizontal, quit less 25MT head, 26" x 9" to Very CENTEC 28 Verical/Horizontal, quit less 25MT head, 26" x 7" y, lege pedietal model ELLIDT DOWNHAM mine bornt, very late machine complete with collect and shruk (power down fee ELLIDT DOWNHAM mine bornt, very late machine complete with collect and shruk (power down fee ELLIDT TOWNHAM mine bornt, very late machine somplete with collect and shruk (power down fee ELLIDT DOWNHAM mine bornt, very late machine somplete with collect and shruk (power down fee ELLIDT TOWNHAM mine bornt capet 70-3000 pm, table 45" x 9" (powered table and shruk 10 mine table and collect and capet 10 mine to very late 10 mine town feet 10 mine table 10 powered 24" x 6" table powered 10 mine table 10 mine table 25" x 9" table powered 10 mine table 10 mine table 25" x 9" table powered 10 mine table 25" x 9" table 10 mine table 10 mine table 25" x 9" table 10 mine table 10 m | \$1,950<br>\$2,250<br>\$2,250<br>\$2,250<br>\$1,400<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500  |
| ADDOOK AND SHIFLET IIIS Horizonative roal Head, 30" x 8" governed table and feed gears, code SOXFORD VMSD variable speed 50 Bit Tead, table 21" x 5" a shwood vice and collect chock. BR DOEP OR 1 Series 1 - 2 HP Visribble speed 88 head, powered (gearbox) table, 42" x 9".  BR DOEP OR 1 Set head 2 speed (after motion) lead, R8 powered (gearbox) table, 42" x 9".  CENTEC 28 Horizonal, 1" artor, table powered, 3 ph motion single phase main motion. CENTEC 28 Verical Horizonal, quil feed 28" t 1 head, 25" x 5" table, pediestal model: ELLIDT DOWNHAM minis borer, very late machine complete with collect and shuck (power-down fee ELLIDT OF OWNHAM. 2 Motion and shuck and 2 MT head, 25" x 5" table powered by ELLIDT TURNET M.L. 19-30 speed 70-3000 rpm, table 45" x 3" (powered by ELLIDT TURNET M.L. 19-30 speed 70-3000 rpm, table 45" x 3" (powered by HEALIDT TURNET M.L. 19-30 speed 70-3000 rpm, table 45" x 3" (powered by HARIBISON N.M 30 INT swhell head 6. chrb., 30" x 6" table/powered hARIBISON VERTICAL 30 INT swhell head 6. chrb., 30" x 6" table/powered hARIBISON VERTICAL 30 INT swhell head 6. chrb., 30" x 6" table/powered hARIBISON VERTICAL 101L 2 More tape 2 speed motor, variable selector 775 0000 rpm, cabinet 519 RR30, millingdiffiling machine complete with accessories.  TOM SENIOR M1 horizontal, 25" x 6" powered table, 1" after 100 MT SENIOR M1 horizontal, 25" x 6" powered table, 1" after 100 MT SENIOR M1 horizontal, 25" x 6" powered table, 1" after 100 MT SENIOR M1 horizontal, 25" x 6" powered table, 1" after 100 MT SENIOR M1 horizontal, 25" x 6" powered table, 1" after 100 MT SENIOR M1 horizontal, 25" x 6" powered table, 1" after 100 MT SENIOR M1 horizontal, 25" x 6" powered table, 1" after 100 MT SENIOR M1 horizontal, 25" x 6" powered table, 1" after 100 MT SENIOR M1 horizontal, 25" x 6" powered table, 1" after 100 MT SENIOR M1 horizontal, 25" x 6" powered table, 1" after 100 MT SENIOR M1 horizontal, 25" x 6" powered table, 1" after 100 MT SENIOR M1 horizontal, 25" x 6" powered table, 1" after 100 MT SENIOR M1 horizont | \$1,950<br>\$2,250<br>\$2,250<br>\$1,400<br>\$0,725<br>\$1,400<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500  |
| ADDIOCK AND SHIFLET IIIS Horizontative roal Head, 30" x 8" governed table and feed gears, oce BOXFGRO VMID variable speed (30 NT head, table 211½ x 8" + alwood vice and collect chack. BRIDGEP OR T Series 1 - 2 HP Variable speed RS head, powered (grantox) table, 42" x 9" to RRIDGEP OR T Series 1 - 2 HP Variable speed RS head, powered (grantox) table, 42" x 9" to CENTEC 28 Heritontal, 1" artor, table powered, 3 ph motor single phase main motor. CENTEC 28 Vericaphorousal, quil feed 291 head, 69" x 9" table, pediestal model ELLIOT DOWNHAM minis borer, very late machine complete with collects and shoulk (power-down fee ELLIOT 90" QMNIMILA. 2 Morrer speed quil universal head, 26" x 7" y powered table. ELLIOT 3 LIBRET M.L. RS-10 speed 70-0000 pm, table 45" x 10" (powered).  EMOO FEE Vericaphorous Green quil bed head 2 MT, powered 34" x 9" stoke, full coolant tray and cell 3 phase and does not like a comenter to colly. NA RIBISON NA 10" (NIT anvival head & cutch, 30" x 9" table/powered.  ARRIESON NETTICAL 20 INT switch head & cutch, 30" x 9" table/powered.  RACILAR VERTICAL 20 INT switch head & cutch, 30" x 9" table/powered.  RACILAR VERTICAL 20 INT switch head & cutch, 30" x 9" table/powered.  RACILAR VERTICAL 20 INT switch head & cutch, 30" x 9" table/powered.  RACILAR VERTICAL 20 INT switch head & cutch, 30" x 9" table/powered.  RACILAR VERTICAL 20 INT switch head & cutch, 30" x 9" table/powered.  RACILAR VERTICAL 30" X 9" x 9" x 9" x 9" table/powered.  RACILAR VERTICAL 30" X 9" x 9" x 9" x 9" x 9" table/powered.  TOM SENIOR M1 VM 29" x 9", 2 more taper, 1" after.  TOM SENIOR M1 VM 29" x 9"   | \$1,950<br>\$2,250<br>\$2,250<br>\$1,400<br>\$0,725<br>\$1,400<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500<br>\$1,500  |
| ADDOOK AND SHIFLET RISH concombinative had, 30" x 8" governed table and feed gears, occ  BOXFORD VMSD variable speed (30 Bit had, bub 21" x 8" a shwood vice and collet chock.  BR DOSEP DRIT Series 1.2 HP Visribble speed R8 head, governed (gearbor) table, 45" x 9".  BR DOSEP DRIT Set head 2 speed (after motor) head, R8 powered (gearbor) table, 45" x 9".  Very CENTEC 28 Nontromal, 1" arbor, table powered, 3 ph motors single phase main motor.  CENTEC 28 Verifications, 1" arbor, table powered, 3 ph motors single phase main motor.  CENTEC 28 Verifications, 1" arbor, table powered, 3 ph motors single phase main motor.  CENTEC 28 Verifications, 1" arbor, table 28" t 7" and 25" x 5" table, pedicatal model:  ELLIDIT DOWNHAM mine boret, very lase machine complete with collects and thrust (power-down fee  ELLIDIT DOWNHAM mine boret, very lase machine complete with collects and thrust (power-down fee  ELLIDIT DOWNHAM mine boret, very lase machine domplete with collects and thrust (power-down fee  ELLIDIT TOWNHAM (1" No. 10" 50 power 10" 10" 10" 10" 10" 10" 10" 10" 10" 10"   | £1,950 at le constitution de la   |
| ADDOOK AND SHIFLET RIS Horizontative roal Head, 30" x 8" governed table and feed gears, code SOXFORD VMSD variable speed (30 Bit hand, build a "11" x 8" alwood vice and collect chock. BR DOGEP OR T Seriest 1 - 2 HP Visribble speed RR head, governed (gearboy) table, 42" x 9".  BR DOGEP OR T Set head 2 speed (after motted) head, RR governed head, variable speed 42" x 9" to Very CENTEC 28 Nortcomat, 1" arbor, table powered, 3 ph mottes single phase main motor.  CENTEC 28 Verificat Plantage and the 2 Bit 1" say, 5" x 5" table, gederati motor.  CENTEC 28 Verificat Plantage and the complete with collects and thrust (governdown for ELLIDT DOWNHAM mine borst, very late machine complete with collects and thrust (governdown for ELLIDT TO "OWNHAM. Bit 3 Bitters tapped quill week head 1" ket 2" x 9" (governdown falle ELLIDT TO "Verificat 6" gene quill level head 5" x 10" (governdown falle).  EMOC RIS 2 Verificat 6 gened quill level head 5" x 10" (governdown falle).  HARRISON NAV 20 INT switch head 6" cityth, 20" x 6" table/bowered.  HARRISON NAV 20 INT switch head 6" cityth, 20" x 6" table/bowered.  HARRISON NAV 20 INT switch head 6" cityth, 20" x 6" table/bowered.  HARRISON NETITICAL SUD INT switch head 6" cityth, 20" x 6" table/bowered.  SENIOR RIS VERTICAL SULL 2 Mores tappe; 2" speed motor; variable selector 175 52200 spm, cabinet SENIOR RIS NOW 1" X 1" x 6" powered table. 1" abor.  TOM SENIOR STYPE 2 mode taper quill feed motorisod head, 20" x 0", table in external was according.  TOM SENIOR STYPE 2 mode taper quill feed motorisod head, 20" x 0", table in external was according.  Please rings to  | £1,950<br>£2,250<br>mice £2,250<br>£1,1400<br>£1,2250<br>£1,1400<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1   |
| ADDIOCK AND SHIFLET IIIS Horizonative roal Head, 30" x 8" governed table and feed gears, oce BOXFGRD VMID variable speed (30 ft head, bell 211½" x 8" abwood vice and collect chack. BRIDGEP OR T Series 1 - 2 HP Variable speed RS head, powered (gearbox) table, 42" x 9" to RRIDGEP OR T Series 1 - 2 HP Variable speed RS head, powered (gearbox) table, 42" x 9" to Very CENTEC 28 Heritontal, 1" artor, table powered, 3 ph motor single phase main motor. CENTEC 28 VerticalPortantal, quil feed 281 head, 25" x 5" table, pedestal model ELLIST TOOWNHAM ministore, very late machine complete with collect and druck (governdown fee ELLIST TOO CONNINELL 3 Motors taped 70-3000 mpt, table, 45" x 7", powered table. ELLIST TOO CONNINELL 3 Motors taped 70-3000 mpt, table, 45" x 70" (governdo). EMCO FB2 Vertical 6 speed quill feed head 2 MT, powered 24" x 6" table, full coolant tray and cell 3 phase and does not like a comenter so only. NA RIBISON NA TOO INT anwest head 5 clutch, 30" x 6" table/powered. ARRISSON NETTICAL 30 INT anwest head 5 clutch, 30" x 6" table/powered. MRRISSON NETTICAL 30 INT anwest head 5 clutch, 30" x 6" table/powered. MRRISSON NETTICAL 30 INT anwest head 5 clutch, 30" x 6" table/powered. MRRISSON NETTICAL 30 INT anwest head 5 clutch, 30" x 6" table/powered. MRRISSON NETTICAL 30 INT anwest head 5 clutch, 30" x 6" table/powered. MRRISSON NETTICAL 30 INT anwest head 5 clutch, 30" x 6" table/powered. MRRISSON NETTICAL 30 INT anwest head 5 clutch, 30" x 6" table/powered. MRRISSON NETTICAL 30 INT anwest head 5 clutch, 30" x 6" table/powered. MRRISSON NETTICAL 30 INT anwest head 5 clutch, 30" x 6" table/powered. MRRISSON NETICAL 30 INT anwest page quil feed motor variable selector 175 c2000 cpm, cabinet 51 PRESS, milegal feed machine complete with accessories. TOM SENIOR ST TYPE 2 more taper (util feed motorsocker selector 175 c200 cpm, cabinet 51 PRESS, machine complete with accessories.   | £1,950<br>£2,250<br>mice £2,250<br>£1,1400<br>£1,2250<br>£1,1400<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1   |
| ADDOOK AND SHIFLET RISH concombinative had, 30" x 8" governed table and feed gears, occ  BOXFORD VMSD variable speed (30 Bit had, but be 21% x 8" alwood vice and collect chock.  BR DOSEP DR T Series 1 - 2 HP Visrible speed R8 head, governed (gearbor) table, 42" x 9".  BR DOSEP DR T Set head 2 speed (after motor) head, R8 powered (gearbor) table, 42" x 9".  Very CENTEC 28 Nontromal, 1" arbor, table powered, 3 ph motors single phase main motor.  CENTEC 28 Verifications, 1" arbor, table powered, 3 ph motors single phase main motor.  CENTEC 28 Verifications, 1" arbor, table 28" t 7" and 25" x 5" table, gedestal motors.  LELIDIT DOWNHAM mine boret, very late machine complete with collects and thrusk (governdown for  ELLIDIT DOWNHAM mine boret, very late machine complete with collects and thrusk (governdown for  ELLIDIT DOWNHAM mine boret, very late machine complete with collects and thrusk (governdown for  ELLIDIT DOWNHAM mine boret, very late machine domplete with collects and thrusk (governdown for  ELLIDIT THIRET M.L. 18-10 speed 70-3000 pm, table 45" x 9" (governd bits.  JA Planted Own M.L. 18-10 speed quill level head 3", 2" table (which per  ARRIGINO N hortcoreal, 2" x 9" powered table.  MARRISON N N/V 00 INT awkel head 6. chtch, 20" x 9" table/bovernd.  MODE WAS HEAD CHILLY for a Hotobyroat table with metric graduitions.  MACLARY VERTICAL BILL 2 Mone taper 2 speed motor, variable as actor 175 52200 cm, cabinet  SENIOR ST VERTICAL BILL 2 Mone taper 2 speed motor, variable as actor 175 52200 cm, cabinet  SENIOR ST VERTICAL BILL 2 Mone taper 2 speed motor variable as actor 175 52200 cm, cabinet  SENIOR ST VERTICAL BILL 2 Mone taper 2 speed motor variable as actor 175 52200 cm, cabinet  SENIOR ST VERTICAL BILL 2 Mone taper 2 speed motor variable as actor 175 42200 cm, cabinet  SENIOR ST VERTICAL BILL 2 Mone taper 2 speed motor variable as actor 175 42200 cm, cabinet  SENIOR ST VERTICAL BILL 2 Mone taper 2 speed motor variable as actor 175 42200 cm, cabinet  SENIOR ST VERTICAL BILL 2 Mone taper 2 speed motor varia | £1,950<br>£2,250<br>mice £2,250<br>£1,1400<br>£1,2250<br>£1,1400<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1500<br>£1,1   |
| ADDIOX AND SHIFLET IIIS Horizonative roal Head, 30" x 8" governed table and feed gears, cool BOXFORD VMID variable speed (30 ft head, but 21% x 8" altwood vice and collect chack. BRIOGEP OR T Series 1 - 2 HP Variable speed RS head, powered (gearbox) table, 42" x 9".  REDGEP OR T Series 1 - 2 HP Variable speed RS head, powered (gearbox) table, 42" x 9".  REDGEP OR T Series 1 - 2 HP Variable speed RS head, powered (gearbox) table, 42" x 9".  REDGEP OR T Series 1 - 2 HP Variable speed RS head, powered head, variable speed 42" x 9".  Very CENTEC 28 Heritonial, 1" artor, table powered, 3 ph motor single phase main motor.  CENTEC 28 Vertical Horizonial, quil feed 28T head, 25" x 5" table, pedestal motorial ELLIDIT DOWNHAM mine bornt, very late machine complete with collect and chruik (power-down fee ELLIDIT DOWNHAM mine bornt, very late machine complete with collect and chruik (power-down fee ELLIDIT DOWNHAM mine bornt, very late machine complete with collect AV 7", powered table and ELLIDIT TURNET M 1, 18" to speed 70-3000 mpt, table 45" x 9" (powered).  EMOD FB2 Vertical Signed quill lead head 2 MT, powered 24" x 6" table, full coolant tray and cell 3 phase and does not like a come rate so celly.  NARRISON N NY 30 INT anweal head 5, clutch, 30" x 6" table/powered.  NARRISON N W 10 INT anweal head 5, clutch, 30" x 6" table/powered.  HOUR WAY HEAD CHLU 5" has highly head 6, clutch, 30" x 6" table/powered.  HOUR WAY HEAD CHLU 5" has a highly had table with metro gradulents.  TOM SENIOR M1 VIPL 20" x 6" x 6" powered table, 1" arbor.  TOM SENIOR M1 VIPL 20" x 6" x 6" powered table, 1" arbor.  TOM SENIOR M1 VIPL 20" x 6" x 6" powered table, 1" arbor.  TOM SENIOR M1 VIPL 20" x 6" x 6" powered table, 1" arbor.  TOM SENIOR M1 VIPL 20" x 6" x 6" powered table, 1" arbor.  TOM SENIOR M1 VIPL 20" x 6" x 6" powered table, 1" arbor.  TOM SENIOR M1 VIPL 20" x 6" x 6" powered table, 1" arbor.  TOM SENIOR M2" x 6" x  | 11,950 12,250 12,250 12,250 12,250 12,250 11,1400 12,250 11,15,80 17,50 11,15,80 17,50 11,15,80 17,50 11,15,80 17,50 11,15,80 17,150 11,15,80 17,150 11,15,80 17,150 11,15,80 17,150 11,15,80 17,150 11,15,80 17,150 11,15,80 17,150 11,15,80 17,150 11,15,80 17,150 11,15,80 17,150 11,15,80 17,150 11,15,80 17,150 11,15,80 17,150 11,15,80 17,150 11,15,80 17,150 11,15,80 17,150 11,15,80 17,150 11,15  |
| ADDOOK AND SHIFLET BE increasal/verteal Head, 30" x 8" governed table and feed gears, code SOXFORD VMSD variable speed (30 fit head, table 21% x 8" alwood vice and collect chock. BR DOGEP OR 1 Seriest 1 - 2 HP Vicrible speed RS head, powered (grant-box) table, 42" x 9".  BR DOGEP OR 1 Seriest 1 - 2 HP Vicrible speed RS head, powered (grant-box) table, 42" x 9".  BR DOGEP OR 1 Seriest 1 - 2 HP Vicrible speed RS head, powered (grant-box) table, 42" x 9".  CENTEC 28 Horizontal, 1" artor, table powered, 3 ph more single phase main more.  CENTEC 28 Vertical Report of the seriest of table speed AR 1  | £1,950<br>£2,250<br>side<br>£2,250<br>£1,400<br>£0, £2,250<br>£1,400<br>£1,500<br>£1,500<br>£1,500<br>£1,500<br>£1,500<br>£1,500<br>£1,500<br>£1,500<br>£1,500<br>£1,500<br>£1,500<br>£1,500<br>£1,500<br>£1,500<br>£1,500<br>£1,500<br>£1,500<br>£1,500<br>£1,500<br>£1,500<br>£1,500<br>£1,500<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,600<br>£1,6  |
| ADDIOCK AND SHIFLET IIIS Horizontative roal Head, 30" x 8" governor table and feed gream, oce BOXFORD VMID variable speed (30 NT head, table 21% x 8" + alwood vice and collect chack. BRIDGEP OR T Series 1 - 2 HP Variable speed RS head, powered (great-bot) table, 42" x 9" to RRIDGEP OR T Series 1 - 2 HP Variable speed RS head, powered (great-bot) table, 42" x 9" to CENTEC 28 Herizontal, 1" artor, table powered, 3 ph motor, single phase main motor. CENTEC 28 Vericas/Horizontal, quil feed 2917 head, 69" x 9" table, pediestal model.  ELLIDT DOWNHAM minis boret, very late machine complete with collects and shruk (power-down fee ELLIDT DOWNHAM minis boret, very late machine complete with collects and shruk (power-down fee ELLIDT DOWNHAM minis boret, very late machine complete with collects and shruk (power-down fee ELLIDT DOWNHAM minis boret, very late machine complete with collects and shruk (power-down fee ELLIDT DOWNHAM minis boret, very late machine complete with collects and shruk (power-down fee ELLIDT DOWNHAM minis boret, very late machine complete with collects of "7", power-down fee ELLIDT DOWNHAM minis boret is consequent table.  ELLIDT DIRRET M.L. RS-10 speed 70-0000 pm, table 45" x 10" (power-down fee) had ministed and collected feed of the power-down feed of t | 11,950 12,250 able 12,250 able 17,255 able 17,255 able 17,255 able 17,550 able  |
| ADDOOK AND SHIFLET BIS increasative real Head, 30" x 8" governed table and feed gears, oce SOXFORD VMSD variable speed 50 Bit Thesis, table 21% x 6" alwood vice and collect chock. BR DOGEP OR 1 Series 1 - 2 HP Visrible speed 88 head, powered (gearbox) table, 42" x 9".  BR DOGEP OR 1 Series 1 - 2 HP Visrible speed 88 head, powered (gearbox) table, 42" x 9".  BR DOGEP OR 1 Series 1 - 2 HP Visrible speed 88 head, powered (gearbox) table, 42" x 9".  CENTEC 28 Horizonas, 1" arbor, table powered, 3 ph motor single phase main motor.  CENTEC 28 Verical Series and 1" arbor, table powered and 1" and  | 11,950 12,250 able 10,2250 17,400 able 17,252 11,4100 able 17,550 able 17,500 able 17,405 able 17,505 able 17,405   |
| ADDIOX AND SHIFLET IIIS Horizonative roal Head, 30" x 8" governed table and feed gears, oce BOXFORD VMID variable speed (30 ft head, belt 211% x 8" abwood vice and collect chack. BRIDGEP OR T Series 1 - 2 HP Variable speed RS head, powered (gearbox) table, 42" x 9" to RRIDGEP OR T Series 1 - 2 HP Variable speed RS head, powered (gearbox) table, 42" x 9" to CENTEC 28 Heritontal, 1" artor, table powered, 3 ph motor single phase main motor. CENTEC 28 Verical/Horizontal, quil feed 281 ft head, 69 x 9" table, pedestal model   ELLIDT DOWNHAM ministroet, very late machine complete with college and shall know for ELLIDT DOWNHAM ministroet, very late machine complete with college and shall know for CENTEC 28 Verical Series and shall be shal | 11,950 12,250 able 12,250 able 12,250 able 17,255 able 17,255 able 12,250 able 17,500 able 12,250 able 17,500 able  |
| ADDOOK AND SHIFLET IIIS increasativement Head, 30" x 8" governed table and feed gears, cos  EXCEPTION VMSD variable speed (30 MT head, table 21% x 8" alwood vice and collect chock.  BR DOGEP OR T Seriest 1 - 2 HP Visrible speed 88 head, powered (gearbox) table, 42" x 9".  BR DOGEP OR T Seriest 1 - 2 HP Visrible speed 88 head, powered (gearbox) table, 42" x 9".  BR DOGEP OR T Set head 2 speed (after motion) head, 89 powered head, variable speed 42" x 9".  Very CENTEC 28 Horizontal, 1" arbor, table powered, 3 ph motion single phase main motion.  CENTEC 28 Verifications, 1" arbor, table powered, 3 ph motion single phase main motion.  CENTEC 28 Verifications, 1" arbor, table powered with collect and shoulk (power-down fee ELLIDIT DOWNHAM minis boret, very late machine complete with collect and shoulk (power-down fee ELLIDIT TO CONNINILL 3 Motion speed 70-3000 prin, table 45" x 9" (powered bit 1 ELLIDIT TURNET M.L. 19-30 speed 70-3000 prin, table 45" x 9" (powered bit 1 ELLIDIT TURNET M.L. 19-30 speed 70-3000 prin, table 45" x 9" (powered bit 3 phase and down not like a consenter to colly MR powered 44" x 6" table, full coolant tray and coll 3 phase and down not like a consenter to colly MR powered 44" x 6" table/powered MR prints on VERTICAL 30 INT switch head 6, civith, 30" x 6" table/powered MR prints on VERTICAL 30 INT switch head 6, civith, 30" x 6" table/powered MR prints on VERTICAL 1811. 2 More tape 2 speed motor, wantate selector 775 0000 pm, cabinet 519 RR 93, millingdiffiling machine complete with accessories 10 MR SENIOR 3" TO TIME 2 motion taper 1" arbor 10 MR SENIOR 3" TYPE 2 motion taper 1" arbor 10 MR SENIOR 5" TYPE 2 motion taper quil field motorised head, 20" x 9", table / me ard fail, cool 10 MR SENIOR 5" TYPE 2 motion taper quil field motorised head, 20" x 9", table / me ard fail, cool 10 MR SENIOR 5" TYPE 2 motion taper quil field motorised head, 20" x 9", table / me ard fail, cool 10 MR SENIOR 5" Type 2 motion taper quil field motorised head, 20" x 9", table / me ard fail, cool 10 MR SENIOR 5"  | 11,950 12,250 14/40 16,122,250 17,400 16,122,250 17,400 16,122,250 17,500 18,11,950 17,500 18,11,950 17,500 18,11,950 17,500 18,11,950 17,500   |
| ADDOOK AND SHIFLET BIS horizontative/real Head, 30" x 8" governed table and feed gears, code SEX.FORD VMSD variable speed 50 Bit 1 had, table 21% x 5" alwood vice and collect chock. BR DGEP OR T Seriest 1 - 2 HP Variable speed 88 head, powered (gearbox) table, 42" x 5".  BR DGEP OR T Set head 2 speed (after motor) head, 88 powered (gearbox) table, 42" x 5".  BR DGEP OR T Set head 2 speed (after motor) head, 88 powered head, variable speed 42" x 5" to Very CENTEC 28 Norteonal, 1" arbor, table powered, 3 ph motor single phase main motor.  CENTEC 28 Verifications, 1" arbor, table powered, 3 ph motor single phase main motor.  CENTEC 28 Verifications, 1" arbor, table powered with collect and drively (governdown fee ELLIDT DOWNHLAM minis boret, very late machine complete with collect and drively (governdown fee ELLIDT OF Verification of 18 Mpter taper quill unamental head, 28" x 7", powered table  ELLIDT TURRET M.L. 18-10 speed 70-3000 pm, table 45" x 9" (governdo).  EMOC F62 Verification on titles a consenter to colly  ARRIGHSON NAY 20 INT swhell head & chitch, 20" x 6" table/covered.  HARRIGHSON NAY 20 INT swhell head & chitch, 20" x 6" table/covered.  HARRIGHSON VERTICAL 20 INT swhell head & chitch, 20" x 6" table/covered.  HARRIGHSON VERTICAL SILL 2 thorse taper (2 speed motor, warrable selector 775 5200 pm, cabinet 15P RF30, millingdiffiling machine complete with accessories.  TOM SENIOR M1 horizontal, 25" x 6" powered table, 1" after.  TOM SENIOR M2 The Tomoto taper quill feed motorised head, 28" x 6", table in external notes yeared on the condition.  TOS F62 AV vertical mill, 20 INT, 54" x 10" table, power alloway.  Please ring to VICER CY AEW vertical time mill, 60 INT, 54" x 10" table, power alloway.  Please ring to VICER CY AEW vertical mill, 20 INT, 54" x 10" table, power alloway.  Please ring to VICER CY AEW vertical time table with motorised head, 28" x 6", table in external notes on the COURCY by Decoh, time table gas decomplication of the McDoNoto St 70 and table gas decomplication of the McDoNoto St 7 | 11,950 12,250 14/40 16,12,250 11,400 16,12,250 11,400 16,12,250 11,500 17,500 16,12,500 16,12,500 16,12,500 16,12,500 17,  |
| ADDOOR AND SHIPLET BIS Increamative real Head, 30" x 8" governed table and feed gears, oce SOXFORD VMSD variable speed (30 Bit hand, table 21% x 8" alwood vice and collect chock. BR DOGEP OR 1 Seriest 1 - 2 HP Visriable speed 88 head, powered (gearbox) table, 42" x 9".  BR DOGEP OR 1 Seriest 1 - 2 HP Visriable speed 88 head, powered (gearbox) table, 42" x 9".  BR DOGEP OR 1 Set head 2 speed (after motor) head, 88 powered head, variable speed 42" x 9".  Very CENTEC 28 Horizontal, 1" arbor, table powered, 3 ph motor single phase main motor.  CENTEC 28 Verifications, 1" arbor, table powered, 3 ph motor single phase main motor.  CENTEC 28 Verifications, 1" arbor, table powered x 9" x 9" x 9" and dhis knowledge 1" better table 1" | 11,950 12,250 14/40 16,12,250 11,400 16,12,250 11,400 16,12,250 11,500 17,500 16,12,500 16,12,500 16,12,500 16,12,500 17,  |
| ADDOOK AND SHIFLET RISH tonton brivers at Head, 30" x 8" governed table and feed gears, one BOXFORD VMBO variable speed 50 Bit Tead, table 21" x 5" alwood vice and collect chock. BR DOGEP OR 1 Series 1 - 2 HP Visrible speed 88 head, governed (gearbor) table, 45" x 9".  BR DOGEP OR 1 Series 1 - 2 HP Visrible speed 88 head, governed (gearbor) table, 45" x 9".  BR DOGEP OR 1 Set head 2 speed (after motor) head, 89 governed head, variable speed 42" x 9".  Very CENTEC 28 Ventouthersons, quit feed 28" the ad, 25" x 5" table, gedestal motor.  CENTEC 28 Ventouthersons, quit feed 28" the ad, 25" x 5" table, gedestal motor.  CENTEC 28 Ventouthersons, quit feed 28" the ad, 25" x 5" table, gedestal motor.  ELLIDOT DOWNHAM mine boret, very late machine complete with collect and druk (governdown fee ELLIDOT OF OWNHALL 3 British speed 70-3000 rpm, table 45" x 9" (governdown fee ELLIDOT TO Ventoutherson table 1 head 25" x 7" (governed 24" x 6" table, fell coolant tray and ost) 3 phase and does not like a consenter to only.  ARRIGISON NAV 20 INT awked head 5. CNUE, 30" x 6" table/sovered.  MARRISON NAV PERTICAL 20 INT awked head 5. CNUE, 30" x 6" table/sovered.  MARRISON NAV PERTICAL 20 INT awked head 5. CNUE, 30" x 6" table/sovered.  MARRISON NAV PERTICAL 20 INT awked head 5. CNUE, 30" x 6" table/sovered.  MARRISON NAV PERTICAL 20 INT awked head 5. CNUE, 30" x 6" table/sovered.  MODE WAS HIGH 5" X 1" X 6" your complete with accessoring.  TOM SENIOR 5" TYPE 2 mode taper quill feed motorisod head, 32" x 6", table 7 me and fad, cool TOM SENIOR 5" X 6" x 5" x 6" your taper 1" after 1 and 7" x 10" table, power all ways.  Please fing to 10 Speed 2MT pecked bell mad, powered table 34" x 8" Vary of DR 1 No. 10 Table 1 table 1 table 1 motorisod head, 30" x 6", table 7 me and 1 a     | 11,950 12,250 162,250 162,250 172,51 173,00 181,12,250 173,00 181,13,950 173,00 182,250 173,00 183,13,950 173,00 1  |
| ADDOORS AND SHIFLET BIS Horizonative roal Head, 30" x 8" governed table and feed gears, code SOXFORD VMSD variable speed (30 ft head, bath 21" x 8" alwood vice and collect chock. BR DOGEP OR 1 Seriest 1 - 2 HP Variable speed RS head, powered (gearbox) table, 42" x 9".  BR DOGEP OR 1 Seriest 1 - 2 HP Variable speed RS head, powered (gearbox) table, 42" x 9".  BR DOGEP OR 1 Set head 2 speed (gloon motice) tead, RB powered, wariable speed 42" x 9".  CENTEC 28 Horizonas, 1" arbor, table powered, 3 ph motic single phase main motion. CENTEC 28 Verical Representative and feed 21" x 9".  Very CENTEC 28 Verical Seriest 1 always table machine complete with collect and chick (power-down fee ELLIDT DOWNHAM mine bornt, very late machine complete with collect and chick (power-down fee ELLIDT TO CONNHILL 3 Motion speed 70-3000 mm, table 45" x 9" (powered bit 1 mines) and collect and chick (power-down fee ELLIDT TO Verical Series and chick power-down fee ELLIDT TO Verical Series and chick head 2 MT, powered 24" x 6" table, full coolant tray and coll 3 phase and down not like a consenter to only.  HARRISON N NOT 00 INT aware head 3, circh, 30" x 9" table/powered.  HARRISON VERTICAL 30 INT aware head 3, circh, 30" x 9" table/powered.  HARRISON VERTICAL 30 INT aware head 5, circh, 30" x 9" table/powered.  HARRISON VERTICAL 10 INL 2 More taper (2 speed motion, wantable selector 175-2200 cpm, cabinet 51 PRF30, millingdiffiling machine complete with accessories.  TOM SENIOR M1 horizontal, 25" x 6" powered table, 1" abor.  TOM SENIOR M2 TYPE 2 motion taper quil feed motorisod head, 25" x 9", table / men and fail, cool TOM SENIOR M2 TYPE 2 motion taper quil feed motorisod head, 25" x 9", table / men and fail, cool TOM SENIOR M2 TYPE 2 motion taper quil feed motorisod head, 25" x 9", table / men and fail, cool TOM SENIOR M3 Type 2 M 2 M 2 M 2 M 2 M 2 M 2 M 2 M 2 M 2  | \$1,950 to 2,250 to 2,250 to 2,250 to 2,250 to 2,250 to 2,250 to 1,140 to 1,250 to 1,150 to 1,   |
| ADDOOK AND SHIFLET BIS Horizontative roal Head, 30" x 8" governed table and feed gears, code SOXFORD VMSD variable speed 50 Bit 1 had, table 211's x 8" alwood vice and collect chock. BR DOGEP OR 1 Series 1 - 2 HP Variable speed 88 head, powered (parabot) table, 42" x 9".  BR DOGEP OR 1 Series 1 - 2 HP Variable speed 88 head, powered (parabot) table, 42" x 9".  BR DOGEP OR 1 Set head 2 speed (after motor) head, 88 powered head, variable speed 42" x 9".  Very CENTEC 28 Nortcomal, 1" arbor, table powered, 3 ph motor single phase main motor.  CENTEC 28 Verifications, 1" arbor, table powered, 3 ph motor single phase main motor.  CENTEC 28 Verifications, 1" arbor, table 2811 head, 25" x 5" table, pedestal motor.  ELLID TOWN HEAM mine bornt, very late machine complete with collects and thrust (power down for ELLID TOWN HEAM. 18% to speed 70-3000 mm, table 45" x 30" (powered).  ELLID T WEITHET MILL 18% to speed 70-3000 mm, table 45" x 30" (powered).  ARRIFLED X Verification group quality table head 30" table, 30" x 5" table, 5"  | 11,950 12,250 alve 12,250 alve 12,250 alve 12,250 alve 12,250 at 1  |
| ADDIOCK AND SHIFLET BIS Horizontative roal Head, 30" x 8" powered table and feed gears, code SOXFGRO VMSD variable speed 50 MT head, table 21% x 6" alwood vice and collect chack. BR DGEP DR 1 Series 1 - 2 HP Variable speed 88 head, powered (gearbox) table, 42" x 9".  BR DGEP DR 1 Series 1 - 2 HP Variable speed 88 head, powered (gearbox) table, 42" x 9".  CENTEC 28 Heritonial, 1" artor, table powered, 3 ph moting single phase main motion. CENTEC 28 VertoalPhorizonial, quil field 281 head, 25" x 5" table, pediettal model ELLIDT DOWNHAM mini-bornt, very late machine complete with college and druck (gower-down fee ELLIDT DOWNHAM mini-bornt, very late machine complete with college and druck (gower-down fee ELLIDT DOWNHAM mini-bornt, very late machine complete with college and druck (gower-down fee ELLIDT TOWNHAM mini-bornt, very late machine complete with college and druck (gower-down fee ELLIDT TOWNHAM mini-bornt, very late machine complete with college and druck (gower-down fee ELLIDT TOWNHAM mini-bornt, very late machine complete with college and down notifies a commenter go celly.  EMGO FB2 Vertical 6 speed quill feed head 2 MT, powered 34" x 6" table, full coolant tray and cell 3 phase and down notifies a commenter go celly.  ARRIESON NET DOWN 10 DIST alwest table with mini-bornt (governed).  HARRIESON NET DOWN 10 DIST alwest thead 6 chich, 30" x 6" table/powered.  HARRIESON NET TOKAL SILL 2 Morre tape (2 speed motics variable selector 175 52200 spm, cabinet 5P RR30, millingdiffiling machine complete with accessories.  TOM SENIOR MT Noticetal, 25" x 6" gowered table, 1" arbor.  TOM SENIOR MT Noticetal, 25" x 0", 2 more taper, 1" advor.  TOM SENIOR MT Noticetal, 25" x 0", 2 more taper, 2" speed motics variable selector 175 52200 spm, cabinet 5P RR30, millingdiffiling machine complete with accessories.  TOM SENIOR MT Noticetal, 40 MT, 50 MT, 50" x 10" table, power alloway.  Please rings to your process of the power alloway.  Please rings to your process of the power alloway.  Please rings to your process of the p | 11,950 12,250 alve 12,250 alve 12,250 alve 12,250 alve 12,250 at 1  |
| ADDOORS AND SHIFLET BIS Increamative real Head, 30" x 8" governed table and feed gears, oce BOXFORD VMSD variable speed (30 Bit hand, but 211% x 8" alwood vice and collect chock. BR DOGEP OR 1 Series 1 - 2 HP Visrible speed 88 head, powered (parabot) table, 42" x 9".  BR DOGEP OR 1 Set head 2 speed (after motor) head, 88 powered (parabot) table, 42" x 9".  CENTEC 28 Horizontal, 1" arbor, table powered, 3 ph motor single phase main motor.  CENTEC 28 Verical Plant and table table 1 head, 25" x 5" table, pedicatal motor.  CENTEC 28 Verical Series 1 - 2 MP table 1 head, 25" x 5" table, pedicatal motor.  CENTEC 28 Verical Series 1 - 3 More taper quil survense with collect and shoulk (power down fee ELLIDT TO COMMILLA). 3 More taper quil survense head, 26" x 7", powered table.  ELLID T TURRET M.L. 18-10 speed 70-3000 rpm, table 45" x 9" (powered).  EMOC 672 Verical 6 speed quill seed head 2 MT, powered 34" x 6" table, full coolant tray and cell 3 phase and down not like a consenter to celly.  HARRISON N.M. 20 INT swhell head 6. chtch, 30" x 6" table/powered.  HARRISON N.M. 20 INT swhell head 6. chtch, 30" x 6" table/powered.  HARRISON N.M. 20 INT swhell head 6. chtch, 30" x 6" table/powered.  HARRISON N.M. 20 INT swhell head 6. chtch, 30" x 6" table/powered.  HARRISON N.M. 20 INT swhell head 6. chtch, 30" x 6" table/powered.  HARRISON N.M. 20 INT swhell head 6. chtch, 30" x 6" table/powered.  HARRISON N.M. 20 INT swhell head 6. chtch, 30" x 6" table/powered.  HARRISON N.M. 20 INT swhell head 6. chtch, 30" x 6" table/powered.  HARRISON N.M. 20 INT swhell head 6. chtch, 30" x 6" table/powered.  HARRISON N.M. 20 INT swhell head 6. chtch, 10" x 6" table/powered.  HARRISON N.M. 20 INT swhell head 6. chtch, 10" x 6" table/powered.  HARRISON N.M. 20 INT swhell head 6. chtch, 10" x 6" table/powered.  HARRISON N.M. 20 INT swhell head 6. chtch, 10" x 6" table/powered.  HARRISON N.M. 20 INT swhell head 6. chtch, 10" x 6" table/powered.  HARRISON N.M. 20 INT swhell head 6. chtch, 10" x 6" table/powered.  HARRISON N.M. 20 INT swh | 11,950 12,250 162,250 1728 17400 181,12250 181,1390 17500 181,1390 17500 181,1390 17500 181,1390 17500 182,250 182,250 182,250 182,250 183,250  |
| ADDOOK AND SHIFLET BIS Incorporative real Head, 30" x 8" powered table and feed gears, ope SOXFORD VMSD variable speed 50 Bit Tead, table 211's x 8" alwood vice and collect chock. BR DOGEP OR T Series 1 - 2 HP Variable speed 88 head, powered (parabot) table, 48" x 8".  BR DOGEP OR T Set head 2 speed (after motor) head, 88 powered (parabot) table, 48" x 8".  BR DOGEP OR T Set head 2 speed (after motor) head, 88 powered head, variable speed 42" x 9" to Very CENTEC 28 Monteonal, 1" arbor, table powered, 3 ph motor single phase main motor.  CENTEC 28 Verification and table table. 28" x 9" to Very Set ELLIDT DOWNHAM mine boret, very late machine complete with collect and dhisk (power down fee ELLIDT TO COMNHALL 3 Britest taper quill serve main head, 28" x 7", powered table.  ELLIDT TURRET M.L. R9-10 speed 70-3000 pm, table 45" x 9" (powered).  ELLIDT TURRET M.L. R9-10 speed quill beet head 2 MT, powered 34" x 6" table, following table. 44" x 6" table, following table in extraordinal table. 44" x 6" table, following table in extraordinal table. 44" x 6" table, following table in extraordinal t | 11,950 12,250 162,250 1728 17400 181,12250 181,1390 17500 181,1390 17500 181,1390 17500 181,1390 17500 182,250 182,250 182,250 182,250 183,250  |
| ADDOORS AND SHIFLET BE increase and each cold of xif y and yourse and colors chook.  BERDGEP OR T Series 1 - 2 HP Visible speed 68 head, powered (pastbot) table, 45" to".  BR DGEP OR T Series 1 - 2 HP Visible speed 68 head, powered (pastbot) table, 45" to".  BR DGEP OR T Series 1 - 2 HP Visible speed 68 head, powered (pastbot) table, 45" to".  BR DGEP OR T Set head 2 speed (after motor) head, 86 powered head, variable speed 42" x 9" to CENTEC 28 Heritagnas, quil feed 281 head, 25" x 5" table, pediestal motor.  CENTEC 28 Verical Series and table powered, 3 ph motor single phase main motor.  CENTEC 28 Verical Series and table powered with collect and drively (power down fee ELLIDT OF COMMILLA). British speed 70-3000 rpm, table 45" x 9" (powered table below 51 km collect and drively (power down fee ELLIDT THE ML, 18-10 speed 70-3000 rpm, table 45" x 9" (powered).  BROOR 57 Verical Series and collect and of table powered with collect and drively power down fee ELLIDT THE ML, 18-10 speed 70-3000 rpm, table 45" x 9" (powered).  BROOR 57 Verical Series and collect and collect and drively powered with past and down not like a consenter to only MARINISON NAV 90 INT swhell head & chitch, 30" x 9" table/powered.  BROOR 50 X VERTICAL 30 INT swhell head & chitch, 30" x 9" table/powered.  BROOR 50 X VERTICAL 30 INT swhell head & chitch, 30" x 9" table/powered.  BROOR 50 X VERTICAL 50 X 2 motors taper 0 x 9 table powered with selective 775 5200 rpm, cabinet 51 PR 50 x 9 millingdiffiling machine complete with accessories.  TOM SENIOR M1 hortoontal, 25" x 9" powered table, 1" after 10 x 9 table powered.  TOM SENIOR M1 hortoontal, 20" x 9" x 9" accessories.  TOM SENIOR M1 hortoontal, 20" x 9" x 9" accessories.  TOM SENIOR M1 hortoontal, 20" x 9" x 9" accessories.  TOM SENIOR M1 hortoontal, 20" x 9" x 9" accessories.  TOM SENIOR M1 hortoontal, 20" x 9" x 9" accessories.  TOM SENIOR M1 hortoontal, 20" x 9" x 9" accessories.  TOM SENIOR M1 hortoontal, 20" x 9" x 9" accessories.  TOM SENIOR M1 hortoontal, 20" x 9" x 9" accessories.  | 11,950 12,250 162,250 1725 17400 181,12250 181,1390 17500 181,1390 17500 181,1390 17500 182,250 182,250 183,25  |
| ADDIODX AND SHIFLET BIS increasative real Head, 30" x 8" powered table and feed gears, oce BOXFORD VMSD variable speed; 50 MT head, table 21" x 8" alwood vice and collect chock. BR DGEP OR 1 Series 1 - 2 HP Variable speed RS head, powered (grantox) table, 42" x 9".  BR DGEP OR 1 Series 1 - 2 HP Variable speed RS head, powered (grantox) table, 42" x 9".  BR DGEP OR 1 Series 1 - 2 HP Variable speed RS head, powered (grantox) table, 42" x 9".  CENTEC 28 Heritanna, 1" artor, table powered, 3 ph motor single phase main motor. CENTEC 28 Vertical Processes, quil feed 2MT head, 25" x 5" table, pedestal model.  ELLIDT DOWNHAM minis borer, very late machine complete with collects and chruik (power-down fee ELLIDT OF VMMIMIL 13 Minter taper quil unamental head, 25" x 7", powered table. LLIDT TRUTHET MLL RS-10 speed 70-3000 rpm, table 45" x 10" (powered).  EMOD FID 2 Vertical 6 gened quill teed head 25 MT, powered 24" x 6" table, full coolant tray and cable. ARRIESON Northoreal, 31" x 6" powered table. ARRIESON VERTICAL, 30 INT merel head 6, clutch, 30" x 6" table/powered.  RACKLAN VERTICAL, 30 INT merel head 6, clutch, 30" x 6" table/powered.  RACKLAN VERTICAL, 30 INT merel taper, 2 speed motor, variable selector 175 0000 rpm, cabinet 51 PRF30, millingdiffiling machine complete with accessories.  TOM SENIOR M1 hortcontal, 25" x 6" powered table, 1" after. Selection 11,2 TOM SENIOR M2 TOM SENIOR M3 for more taper quil feed motorised head, 25" x 6", table in examinely nose condition.  TOS SENIOR M1 hortcontal, 25" x 6" powered table, 1" after. Selection 11,2 TOM SENIOR M3 for machine complete with accessories.  FIGURE M4 years and m3  | 11,950 12,250 12,250 17,251 14,400 12,250 11,14,00 12,250 11,15,00 17,500 11,15,00 17,500 11,15,00 17,500 1  |
| ADDOORS AND SHIFLET RISH increasative real Head, 30" x 8" powered table and feed gears, ode SOXFORD VMSD variable speed (30 ft head, but 211% x 8" alwood vice and collect chock. BR DOGEP OR 1 Seriest 1 - 2 HP Variable speed RS head, powered (gearbox) table, 42" x 9".  BR DOGEP OR 1 Set head 2 speed (albort motice) head, R8 powered (gearbox) table, 42" x 9".  CENTEC 28 Heritannal, 1" artor, table powered, 3 ph moting single phase main motin. CENTEC 28 Vertical Plant (albort powered), 3 ph moting single phase main motin. CENTEC 28 Vertical Research (albort powered), 3 ph moting single phase main motin. CENTEC 28 Vertical 6 great great very late machine complete with collect and chick (power-down fee ELLIDT TO COMMINIAL 3 Rhiters taped 10" store than 1 km2, 28" x 7" powered 10" albort taped 10" store taped Quill bed head 2 MT, powered 24" x 6" table, full coolant tray and cell 3 phase and down not files a consenior to only HARINISON NAV 20 INT awheli head 3. chich, 30" x 6" table/powered 1 NARINISON VERTICAL 20 INT awheli head 3. chich, 30" x 6" table/powered 1 NARINISON VERTICAL 20 INT awheli head 3. chich, 30" x 6" table/powered 1 NARINISON VERTICAL 10" x 6" table power taped 1 Table 1 NARINISON VERTICAL 10" x 6" table power taped 1 Table 1 NARINISON VERTICAL 10" x 6" table power taped 1 Table 1 NARINISON VERTICAL 10" x 6" powered table 1." after 1 Table 1 NARINISON VERTICAL 10" x 6" powered table 1." after 1 Table 1 NARINISON VERTICAL 10" x 6" table 1 nation of table 2 x 6", table 1 from and fail, cool Table 2 x 6" x 6" table 1 from and fail, cool Table 2 x 6" x 6" table 1 from and fail, cool Table 2 x 6" x 6" table 1 from and fail, cool Table 2 x 6" x 6" table 1 from and fail, cool Table 2 x 6" x 6" table 1 from and fail, cool Table 2 x 6" x 6" table 1 from and fail, cool Table 2 x 6" x 6" table 1 from and fail, cool Table 2 x 6" x 6" table 1 from and fail, cool Table 2 x 6" x 6" table 1 from and fail x 60 table 2 x 6" x 6" table 1 from and fail x 60 table 2 x 6" x 6" table 1 from and fail x 60 table 2 x 6" x  | 11,950 12,250 12,250 12,250 17,255 11,400 12,250 11,11,100 11,150  |
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| FLANDFAST DIS 500 hearth.  Bridgepoor storting head.  Bridgepoor storting head.  Endogenor storting head.  Endogenor storting head.  ENDAFFIELD SID is well.  ENDAFFIELD SID in wells.  ENDAFFIELD SID SID SID IN SID   |   | years  |
|--|---|--|
| Dictors and miscellateous measuring bools  LAM EFACT DS 100 book such  MARICOT Document of the owner  KEMPOMAT 200 to water  KEMPOMAT 200   | Quantity of slor, height gauges, squares, straight edges, mic | cometers cubes, anoth plates, scales weights |
| FLAMERAT DS 500 hash.  Biologocot storing head  MARICOD tooching press  MARICOD tooching press  MARICOD tooching press  MARICOD tooching press  TANASARAT DS 16 12 10 winted bandsow complete with welder attachment.  JONES AND DEFINANCY 12 11 bench centres.  TOM STRUTT E 16 1/10 winted bandsow complete with welder attachment.  JONES AND DEFINANCY 12 11 bench centres.  TOM STRUTT E 16 1/10 winted bandsow complete with welder attachment.  JONES AND DEFINANCY 12 11 bench centres.  JONES AND STRUTT HOUSE AND DEFINANCY 12 11 bench centres.  JONES AND DEFINANCY 12 bench centres.  JONES AND DEFINANCY 12 11 bench centres.  JONES AND DEFINANCY 12 11 bench centres.  JONES AND DEFINANCY 12 b   | (kilos) and mirros/laeous measuring tools                     | Just in                                      |
| Bindipsoport skristing head  KRAINCOM 2010 to weller 190  KRAINCOM 2010 to   |   | \$745  |
| MARICO tooching press  (KAPCMANT 2019 by without a control service of the control   |   | £ 540<br>£750                                |
| KEMPOMAT 200 by eakers  TAMA SAIR TO 19 or Transing 100  START TRITT 16 by 10 vented handbow dompless with welfer attachment  START TRITT 16 by 10 vented handbow dompless with welfer attachment  START TRITT 16 by 10 vented handbow dompless with welfer attachment  START TRITT 16 by 10 vented handbow dompless with welfer attachment  START TRITT 16 by 10 vented handbow dompless with welfer attachment  START TRITT 16 by 10 vented handbow dompless with welfer attachment  START TRITT 16 by 10 vented handbow dompless with welfer 10 by  |   | 1425   |
| START FIRE 1 6 V - 10 venticed bandons complete with welder attachment.  JOHNS AND ENTERNA 4" x x" be well extended.  TOM SERVICE MINISTERS (MINISTERS AND   | KEMPOMAT 230 tis weither                                      | 5-95   |
| JONES AND SHIPMAN 4" RIL" bench center.  TOM SENDIN Storogy based STARTHITE 1-6-6 Woodwood of And Storogy Stor   | TRAN SA.RC 190 + Transtig 1901                                | 5425   |
| IDM SCRIPTION SOCIOUS AND SET ON STOCKED PARKET STATEMENT OF STOCKED PROCESS AND STATEMENT OF ST   |   | atachment                                    |
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| AURI DE 125 Financial, visible piped  SARAT AND EURA FICLAR (CM) M 2-FID DODE presses  An IRANO SMI for presses, visible piped  AN IRANO SMI for presses, visible piped  AN IRANO SMI for presses and independence   | STARTRITE 16-s 6 Woodworking / non-femous bandsaw             | 1950   |
| SMART AND BRI OWN / CCARNIXON NO-NO toggle pressed.  An international transported by the pressed of the pressed   |   | £345   |
| ARRAND SMT Long milling sprode.  An in MY GROD THE LYCKER Amperboard.  An in MY GROD Soldering for Street.  Justic TRAINFAH Robber.  Justic TRAINFAH Robber.  Justic TRAINFAH Robber.  Justic TRAINFAH Robber.  JUSTIC STANDAM ROBBER.  JUSTIC TRAINFAH ROBBER.   |   | 1345<br>Early 1705 1 1705                    |
| MERGED TILLELY CE ATMOSPHERIC and Singerial models.  As not PLANE PAST LIDBOS Solvering from Stove PLANE PAST LIDBOS Solvering from Stove ACM Solv   |   | As new 370                                   |
| PLANETERS LIDOOS Solvaring from Stove GRANITE SIY 22 Sordison Plane VIR ROSHEAM Nicholes  JUSTIS TRAININH Nicholes  TRAININH Nicholes  TRAININH PLANET ROSHEAM Nicholes  TRAININH PLANET ROSHEAM Nicholes  TRAININH PLANET ROSHEAM Nicholes  JUSTIS AND SOLPPAN Rose-bag Press - Stated. CARKSON Nicholes  ARIS Nicholes - Training Groups - Stated. CARKSON Nicholes  ARIS Nicholes - Training Groups - Stated. CARKSON Nicholes  SIY 7 bendalow, horizontal 6 coolests  SIY 7 bendalow, horizontal 6 coolests  SIY 7 bendalow, horizontal 6 coolests  Will LISAWI Rasillation.  Chicago Planet Carloshiam Coolests  SIY 7 bendalow, horizontal 6 coolests  SIY 7   |   | \$245  |
| GRANTE SF x 12° Sorfice Flate  Justin TRIMMEN Burnard 4 Jau Churic  TRIMMEN Burnard 4 Jau Churic  TRIMMEN Burnard 4 Jau Churic  TRIMMEN Burnard 5 Jau Churic  GRANTE SCON 18° I Flacture Chrone American  GRANTE GRANTE Grante Grante 1 Jau Churic  GRANTE F Tomording brech  Ser 7 I bardinan  GRANTE GRANTE Grante Grante 1 Jau Churic  MELLSAM Nachtaw  GRANTE GRANTE Grante Grante Grante Grante  MELLSAM Nachtaw  GRANTE GRANT   |   | Az new \$40                                  |
| VERTOS DELARA NICHAE  TRIAMPH FACE PLATE DM  Very Nic  ESEWAT hatchess Teams Type R  CONIS AND DELPAAN tropology Press - Stand  CONIS AND DELPAAN tropology Press -  ST Pandame, horts orania & content  Were Very Nic  CAR KKON into 1 mobile clonder & faculture  COLAR KKON into 1 mobile clonder & faculture  ST P Teardame, horts orania & content  Were Very Nic  ST P Teardame, horts orania & content  Were Very Nic  ST P Teardame, horts orania & content  Were Very Nic  ST P Teardame, horts orania & content  Were Very Nic  ST P Teardame, horts orania & content  Were Very Nic  ST P Teardame, horts orania & content  Were Very Nic  ST P Teardame, horts orania & content  Were Very Nic  ST P Teardame, horts orania & content  ST P Teardame, horts orania & content  ST P Teardame, horts orania & content  CONTENT & Content orania & content  ST P Teardame, horts orania & content  LIC CONTENT & Content & content  LIC CONTENT & Content  ST P Teardame, horts orania & content  LIC CONTENT & Content  | FLAMEFAST LD900 Soldering Iron Stove                          | 975  |
| TRILLIMENT FOR PLATE DAY  VANCO LINSTER  TARRIMENT FOR PLATE STOPE  VANCO LINSTER  TARRIMENT FOR TRADEST TENER Type R  COINES AND SEIDMAN Broaching Press - Stands  COAR (SCON Mis Pladus Growth Americans)  CAR (SCON Mis Pladus Growth Americans)  TLAN (TAST Troubling her was a standard or plant of the pla   |   | £140<br>Justin £425                          |
| TRIMMENT FACE PLATE DN Very Ninc Existence   |   | 1246   |
| SEWAY hardness Resir Type R  CARINGS AND SIPMAN Broaching Press - Stand  CARINGS No. 19 1 Placing Greeke Attachmen.  All Breatmer 64, hip shoots, waid up  PLANETAST rounding breach.  We say T branching, horsensial 6 doolsed.  We say T branching, horsensial 6 doolsed.  We say T branching, horsensial 6 doolsed.  We say T branching head.  STARTRITE and 35d valve 8 sees.  STARTRITE and 35d valve 8 sees.  SURFORD Freed only bread dail indicator.  BOXYFORD Directal only thread dail indicator.  BOXYFORD Directal only directal onl   | TRIUMPH FACE PLATE D'H  | 570  |
| CANES ON SERVINAN Broaching Presps - Stand. CLAR SSON Mis Fladus Chronic Americans. ASIB Inventor A.V., by motor, wised up FLAMETAST modising bench. SP 7 'S anclaims, horteontal & gooted.  SP 7 'S anclaims, horteontal & gooted.  WE ULSAY matched and servinal & gooted.  WE ULSAY matched and servinal & gooted.  WE TOTIO device plant of servinal & gooted.  WE TOTIO device plant of servinal & gooted.  SP 7 'S anclaims, horteontal & gooted.  SP 7 'S anclaims, horteontal & gooted.  WE TOTIO device plant of servinal & gooted.  SP 7 'S anclaims, horteontal & gooted.  MERINDRO, LO is serve colored church & colored.  SP 7 'S anclaims, horteontal & gooted.  MERINDRO, LO is serve colored church & colored.  SP 7 'S anclaims, horteontal & gooted.  MERINDRO, LO is serve colored on the serve for gooted.  MERINDRO, LO is serve colored on the serve for gooted.  MERINDRO, LO is serve colored on the serve for gooted.  MERINDRO, LO is serve for gooted.  MERINDRO, MINISTER & gooted & gooted.  MERINDRO, LO is serve for gooted.  MERINDRO, LO is serve for gooted.  MERINDRO, LO is serve for gooted.  MERINDRO, SP 9 'S anclaims of gooted.  MERINDRO, LO is serve for gooted.  MERINDRO, LO is serve for gooted.  MERINDRO, SP 9 'S anclaims of gooted.  MERINDRO, SP  | VANCO Linister  | Very Nice £345                               |
| CLAIR STON Mis I Flacible Street Ameniums ABB Inventor 4, high protects ward up PLANETAST mouding bench SP 7 bandward, hortectual 5 gooden WELLSAW nachaw URLLSAW nachaw URLLSAW nachaw URLLSAW nachaw URLLSAW nachaw URLSAW nacha   | ESEWAT NATIONESS TESTET Type R                                | 1426   |
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| WELLSAW hapitalaw.  ORDINGEPORT CHE RITY high speed drilling head.  MTE ORID drivid high head.  STARTRITE and 250 drived the same.  DUPLEX dSS sockoot grinder.  EDWARDOS cant into next cold.  SOX PORD (Imperat only) thread dial indicator.  HOFFMAN RO SARTY (RABEE).  SARTWICE STARTY (RABEE).  SARTWICE ST   |   | 1 100  |
| ### ### ### ### ### ### ### ### ### ##   |   | New 1750                                     |
| MTFORD dividing heads SWARTRIE and 10d aut of 8 man DUFLEX dD9 subpost ginder EDWARDS cast into set of 8 man DUFLEX dD9 subpost ginder EDWARDS cast into set of 8 man DUFLEX dD9 subpost ginder EDWARDS cast into set of 8 man DUFLEX dD9 subpost ginder EDWARDS cast into set of 8 man DUFLEX dD9 subpost ginder EDWARDS cast into set of 8 man DUFLEX dD9 subpost ginder EDWARDS cast into set of 8 man DUFLEX dD9 subpost ginder EDWARDS cast into set of 8 man DUFLEX dD9 subpost ginder URIN DD0, 10 set of 9 man DUFLEX dD9 subpost ginder URIN DD0, 10 set of 9 man DUFLEX dD9 subpost ginder URIN DD0, 10 set of 9 man DUFLEX dD9 set of 9 pot MTFORD DD7 man subpost DUFLEX dD9 man tool post MTFORD DD7 man subpost MTFORD DD7 man subpost DUFLEX dD9 man tool post MTFORD Vertical side of 8 man DUFLEX dD9 set of 9 pot MTFORD Vertical side of 8 man DUFLEX dD9 set of 9 pot DUFLEX dD9 set of 9 man DUFLEX dD9 s   |   | Choice 1245 - \$345<br>1725                  |
| STARTER E and 15d and ell same UPPLEX XDS poolpoint grinder EDWARDS cast iron and softe EDWARDS cast iron set soft   |   | 1395   |
| EDWARDS cast ion set role EDXFFOR Dringerial only thread dial indicator  BDXFFOR Dringerial only thread dial indicator  BDXFFOR Dringerial only thread dial indicator  BDXFORD Dringerial only thread dial indicator  BDXFORD Dringerial only thread only the BDXFORD Dringerial only the State on State BURNERO, DIA 6 jay Chipter shade  BURNERO, DIA 6 jay Chipter only the State on State BURNERO, DIA 6 jay Chipter only the State on State BURNERO, DIA 6 jay Chipter on State on State State on State State on State State State on State   | STARTRITE se315d out off saw                                  | £750   |
| BOXPRIO (Imperationly) thread disinfectors HOFFFAAN ROS AFT YASES  ASTWOOD 6" sewwrith machine vice. East BURNERO, D. 25 5 jaw Chipset shark VARCO, 1" Institut restable vice. East BURNERO, D. 19 leave coloris thrulk vice. BURNERO, D. 19 leave thrulk vice.  |   | \$345<br>\$305                               |
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| ASWCOO 6" www.erist machine vice. East BURNERO, D. 18 6 is us dispress thank VANCO, 1" shieter's vertical + extractor BURNERO, Dhi shieter collect churk + collect VANCO, 1" shieter's vertical + extractor BURNERO, Dhi shieter collect churk + collect VERTEX Shieter or rotary tables:  WERTEX 6" - 6" - 10" rotary tables:  WERTEX 6" - 6" rotary tables:  WERTEX 7" rotary tables:  WERTEX 7" rotary tables:  WERTEX 7" rotary tables:  WERTEX 1" rotary ta   | HOFFMAN ROTARY TABLES   |  |
| VANCO, 11 Smither / vertical + extractor (IRININDRO, 10 Move collect chack + collect (IRININDRO, 10 Move collect chack + collect (IRININDRO, 10 Move collect chack + collect VERTEX 61 - 61 - 10 classy tablest  VERTEX 61 - 61 - 10 classy tablest  MYEGRID SAC / collect chack + collect  MYEGRID VERSIA SAC / collect chack + colle   | AEW COD 6" swive Pit machine vice                             | Earh (345                                    |
| ILBINITRO, DN lever collet chack + collets VERYEX Sinking head VER   |   | 1345   |
| INDITION OF New collect chart is collect VERTEX OF -5" - 10" otary tables: VERTEX OF -6" - 10" otary tables: May Flot BODFFORD Trans attachment of 5" - quartity of delit chucks: MYFFORD MYFFOR with the post. MYFFORD MYFFOR with the post. MYFFORD Werklad situle / flowed type (topy).  CLIVER - ADRIAN FILER .  MYFFORD Verifical situle / flowed type (topy).  LOCKWOOD quad headed 2mt Die Hebber. MYFFORD Werklad situle / flowed of the Die Hebber. MYFFORD Werklad situle / flowed of the Die Hebber. MYFFORD Werklad situle / flowed of the Die Hebber. MYFFORD Werklad situle / flowed Die Hebber. MYFFORD Werklad situle / flowed Die Hebber. MYFFORD Quad headed 2mt Die Hebber. MYFFORD Werklad situle / flowed Die Hebber. MYFFORD Grant flowed of the Die Hebber. MYFFORD Situle / flowed Die Hebber. MYFFORD MYFFORD werklad situle / flowed flower flowed werklad w   |   | \$465<br>\$400                               |
| VERTEX Or ** 10° colory tables  Proper Foot Decided Press of ** 10° colory tables  Proper Foot Decided Press   |   | 1400   |
| VERTEX 6" - 8" - 10" returns attachment 4"()" + quantity of defil chucks MYTRORD MAY 7 Super 7 mair tool port MYTRORD MAY 18 mair tool port MYTRORD Vertical side / Read type (bory)  OLIVER - ACRIAN PILLER  LOCKWOOD qual headed 2nd De Holder  LOCKWOOD qual headed 2nd De Holder  MYCON OOD gual headed 2nd De Holder  MYCON OOD gual headed 2nd De Holder  MYCON OOD feet 8 at / Since Somed  MYCON OOD feet   | VERTEX Dividing head  | New 1245                                     |
| MYTORID MAY 7 Super 7 mair tool port  MYTORID Vertical side / Read type (popy)  OLIVER - ACRIAN PILER  ADDITION OF STATE AND S   | VERTEX 6" - 5" - 10" rotary tables                            | New From 1 135                               |
| ### PROSIDE SEAS was been poet.  ### PROSIDE SEAS was been poet.  ### PROSIDE SEAS AND   |   | \$1025<br>\$40                               |
| METRORO Vertical situle / found type (pory)  LOCKW COD qual headed 2nt Cer Holder  DOCKW COD qual headed 2nt Cer Holder  M. LOCKW COD Test 8 at / 2nt Somed  LOCKW COD Test 8 at / 2nt Somed  M. MAGNETTC Abrulls 15 x 25 fine pole  DOCKW COD Test 8 at / 2nt Somed  M. MAGNETTC Abrulls 15 x 25 fine pole  METROR COLOR Test 8 at / 2nt Somed  M. MAGNETTC Abrulls 15 x 25 fine pole  METROR COLOR Test 8 at / 2nt Somed  M. MAGNETTC Abrulls 15 x 25 fine pole  METROR SENIOR Model II padematistand  UNION boot and outbut growner stand  HARDRIGG Capitan type teolopot  SIRRITEITE 202 recorder/thing band saw  STARTRITE 202 recorder/thing band saw  ACCOSA OF 00011 Right Method Funces  GAURIO 01 6000 2, 2x 1 Sec and Pan general use folder  METRORS Burned Calegor 3 Janc Challes  METRORS Burned Calegor 3 Janc Challes  Boot  COLCHESTER / HARRISCIN D13 Burned 4 Janc 3 light body independent checks  Blook  ROCK METERS and associated measuring tools  SELEN various  MICROM ETERS and associated measuring tools  SECAC Founder type person  HARRISCON LIS Metros Coacher.  Ass 11 TON MOSIL CERANE Manufactured 2000  As rew MITUTOTO grade a set of sites  MITUTOTO grade a set of sites  MITUTOTO 010-013 method set micrometers  MITUTOTO 010-013  | MTFORD 254S may tool post                                     |  |
| OLIVER - ADRIAN FILER  DOCKWOOD qual headed 2nd Die Holder  NA LOCKWOOD gual headed 2nd Die Holder  NA LOCKWOOD was Bar / and Somed.  NA MAGNETIC shurk - 16* x 6* fine pole.  TOM SENDIN todal it pedestal stand UNION social of cuter grader stand WARDING Color Reput Methog Furnace.  GARRIO 80 60001 Reput Methog Furnace.  Bore COLICHESTER / HARRISON D13 Burnerd 4 Jair 8* light body independent chocks.  Bore COLICHESTER / HARRISON D13 Burnerd 4 Jair 8* light body independent chocks.  Bore COLICHESTER / HARRISON D13 Burnerd 4 Jair 8* light body independent chocks.  Bore COLICHESTER / HARRISON D13 Burnerd 4 Jair 8* light body independent chocks.  Bore COLICHESTER / HARRISON D13 Burnerd 4 Jair 8* light body independent chocks.  Bore COLICHESTER / HARRISON D13 Burnerd 4 Jair 8* light body independent chocks.  Bore WICKON ETERS and associated measuring tools.  SCHAR STORM WHEELS, kilms and associated equipment.  S18 packaged  MICROR ETERS and associated equipment.  S18 packaged  MICROR ETERS and associated equipment.  Just to Second standard standard equipment.  Just to Second standard standa   | MYFORD Vertical sikle / fixed type (sopy)                     | 490  |
| LOCKWOOD Gust Park fam Stored.  DOCKWOOD Test Bark fam Stored.  MARGETTC Store 1 for 1 for pole  DOCKWOOD Test Bark fam Stored.  MARGETTC Store 1 for 1 for pole  DOCKWOOD Test Bark fam Stored.  MARGETTC Store 1 for pole  DOCKWOOD Test Bark fam Stored.  MARGETTC Store 1 for 1 for pole  DOCKWOOD Test Bark fam Stored.  MARGETTC Store 1 for 1 for 1 for pole  DOCKWOOD Test Bark fam Stored.  MARGETTC Store 1 for 1 fo   | OLIVER - ADRIAN FILER   | Now 949                                      |
| LOCKW GOD Test Bar / Ann Somed.  DOCKW GOD Test Bar / Ann Somed.  MAGNETIC church: 15' x 6' fine pole.  MAGNIOR Soci and custor greater stand.  MAIDING Copyrian type toolpoid:  SIRT Tooling, Selection.  SIRT TRITLE 20'C voochwinking bard slaw.  SIRT TRITLE 20'C voochwinking bard slaw.  SIRT TRITLE 20'C voochwinking bard slaw.  ALCOSA, OF 00011 Flaped Metting Furnace.  GARRIO 0'F 6002, 2x 9' Bord of Pan general use to lider.  MYFGRO Burned Grights 3' Jaac Churchs.  Bore.  COLCHESTER / HARRISTON DT3 Burned 4' Jaar 8' light body independent churcks.  Bore.  COLCHESTER / HARRISTON DT3 Burned 4' Jaar 8' light body independent churcks.  Bore.  COLCHESTER / HARRISTON DT3 Burned 4' Jaar 8' light body independent churcks.  Bore.  COLCHESTER S and senoclasted measuring tools.  SECAC Powder type press.  JUST BY WHEELS, lither and associated equipment.  SECAC Powder type press.  JUST BY WHEELS, lither and associated equipment.  JUST BY WHEELS, lither and associated equipment.  JUST BY JUST BY WHEELS, lither and associated equipment.  JUST BY JUST BY WHEELS, lither and associated equipment.  JUST BY JUST BY WHEELS, lither and associated equipment.  JUST BY JUST B   | LOCKWOOD quad headed 2mt Die Holder                           | New 140                                      |
| LOCKW GOD Test 8 at / 2 mt Borred.  MAGNETTC Study. 1 15 7 of the pole.  Never use TOM SENIOR Model II padems intact UNION soot and cutter groder stand.  MARDENGE Capitan type teologist 50 INT Toolog. Selection STARTISTE 14-3-0 eccoderating band saw. STARTISTE 14-3-0 eccoderating band saw. STARTISTE 14-3-0 eccoderating band saw. ALCOSA OF GOOT Reput Mething Furnace. GARRO 07 600 C Reput Mething Furnace. GARRO 07 600 C Reput Mething Furnace. GARRO 07 600 C Reput Stand the Second Padems I Second Colliches SETE / HARRISSON D13 Bernerd 4 Jan 3° Ight body independent chocks. Borre SIM 4' Limited (Build in Extraction).  KLINS windows.  MICROM ETERS and associated measuring tools.  SECOND FURNACE And associated measuring tools.  SECOND FURNACE And associated measuring tools.  AS INFORMATION OF TABLES. In the and associated equipment.  MARRISSON LIS Metric Gearton.  AS INFORMATION OF TABLES.  MARRISSON LIS Metric Gearton.  MARRISSON LIS Metric Gearton.  MARRISSON LIS Talteos.  NEW FIROM NEW ZEALAND. Machine vice, 55mm. Jaws precision ministure type deal tonertical six and small control of the second   | LOCKWOOD Qual readed 3nt De Moder                             | New \$40                                     |
| MAGNETIC churst. 19" of fine pole. Total SENDIO Model II polesmal stand. UNION sociand cuter grader stand. HARDINGE Captrain type todopost. 59 Int Tooling, Selection. 31ARTHITE 20" woodworking band staw. 31ARTHITE 20" woodworking band staw. ALCODA OF 0001 Rispet Metting Funace. GAURIO III 5000 _ 20" See and Pan general use folder. MYFORD Burned Grigor 3 Jaw Churles. Bore ALRIO BERT / MARRISTO D13 Burned 4 Jaw 8" light body independent churks. Bore RUH 4" Linisher / Veritaal (Build in Extraction). EXECUTED 11" WHEELS, white and associated measuring tools. SILINS various. MICAD ETERS and associated requirement. MICAD ETERS and associated requirement. MICAD III Metting Genetics. As III PARRISSON US Talesco. MICAD Floods type press. MICAD Floods type press. MICAD Floods type press. MICAD Floods MICE 2 EXALLAND. Stacktine vice, 55 mm. Jaws precision ministure type deal tonerical six and smaller milling machine of stage. MICHING TOO MICE 2 A SILING ASSOCIATED ASSOCIA   | LOCKWOOD Test 8 ar / 3 nst Borned                             | New 942                                      |
| UNION tool and outer ginder stand.  IARDENIES Capitan type toologist 50 INT Tooling, Selection STARTHIES 145-35 excolorating band slaw. STARTHIES 145-35 excolorating band slaw. STARTHIES 145-35 excolorating band slaw. ALCOSA OF 0001 flagged fleeting Funace. ALCOSA OF 0001 flagged fleeting Funace.  GAIRRO 87 6002, 347 800 and Pan genates use tolder.  MYFORD Burned Geter 3 Jack of husbs. Bore COLCHESTER / HARRISS IN D13 Burned 4 Jack 3* light body independent chocks. BURY 1 Limither / Vertical (Build in Estraction).  EXEMPLIES AND 145 Burned Amount of the Selection of the Selecti   | MAGNETIC abusk - 18" x 6" fine pole                           |  |
| IMAIDMGE Capitan lips toolpoid  5 INT tooling, Selection  ACCOSA, OF 00011 Rippid Mething Funded Saw.  ACCOSA, OF 00011 Rippid Mething Funded.  ACCOSA, OF 00011 Rippid Mething Funded.  ACCOSA, OF 00011 Rippid Mething Funded.  Born METRORS Demand Caliform Jaw Selection of Selection Selection.  Born METRORS Demand Caliform Jaw Selection.  Born All **Linisher* / Vertical (Build in Extraction).  KILINS various  FOR MEELS, siths and associated measuring tools.  Selection Frontier by person.  MAR RISSON LIS Maristo Capitan.  MAR RISSON LIS Maristo Capitan.  MAR RISSON LIS Talesco.  NAW FIROM NEW ZEALAND: Machine vice, 55mm. Jaws precision ministure type ideal tonertical six and similar milling machines.  Selection Frontier and Selection Selection Selection Selection Methods of Selection Methods of Selection Selection Methods of Selection Se   |   | 1150   |
| 59 INT Tooling, Selection STARTHITE 143-50 excoderating band slaw ACCOSA OF GOOT Repair Making Furnase. GABRO BF GOO 2, 24° Borr and Pan general use folder MTFGRD Burnerd Grigeru 3 Jase Ghales Borre RUH 4° Linisher / Verical (Build in Estraction). CDD KLHS sarbus  STB packaged POTTERT WHEELS, kiths and associated measuring tools STB packaged POTTERT WHEELS, kiths and associated equipment STB packaged POTTERT WHEELS, kiths and associated equipment STB packaged POTTERT WHEELS, kiths and associated equipment STB packaged STB POTTERT WHEELS, kiths and associated equipment STB POTTERT WHEELS Associated STB POTTERT WHEELS ASSOCIATED ASSOCIA   |   | 9 TOS  |
| STARTIBITE 202 woodworking band daw STARTIBITE 202 woodworking band daw ALCOSA OF 00011 Rapid Meting Funace.  ALCOSA OF 00011 Rapid Meting Funace.  ALCOSA OF 00011 Rapid Meting Funace.  Born MTGRDS burned Citylers 3 Jaws Chushs.  Born COLCHESTER / HARRISTON D13 Burned 4 Jaw 3" ight body independent chocks.  Born ALM 4" Limited / Wested (Buld in Extraction).  KLINS various  MCARM ETERS and associated measuring tools.  S18 packaged POTTERY WHEELS, silves and associated equipment.  Just in SECCAC Fronder type press.  HARRISTON LIS Metid Country.  HIDUTOTO grade a set of sitys.  MIDUTOTO grade a set of sitys.  MIDUTOTO 000-013 metids set micrometers.  HIDUTOTO 000-013 metids set micrometers.  HIDUTOTO 000-013 metids set micrometers.  HIDUTOTO 000-013 metids set micrometers.  WEERE 11, nor mobile garage crane, late blue colour  ELLIOTT 101 / LIS Screensy Head.  SYMPACE Screensy Head.  SYMPACE Screensy Head.  SYMPACE BLOCKS.  1 100 STURCIBIAL Vestical head.  LING 1 101 / LIS Screensy Head.  SYMPACE BLOCKS.  1 200 STURCIBIAL Vestical head.  Country Streens Truchert / Mar Streen Round head, floorplates, small / large.  DOWN HARLISTON AND STREEN Round head, floorplates, small / large.  DOWN HARLISTON AND STREEN Round head, floorplates, small / large.  DOWN HARLISTON AND STREEN Round head, floorplates, small / large.  DOWN HARLISTON AND STREEN Round head, floorplates, small / large.  DOWN HARLISTON HARLISTON AND STREEN ROUND HARLISTON AND STREEN R   |   |  |
| ALCOSA OF 0001 Rapid Meting Furnace.  GARDIO BY 5001, 24° Bott and Pan graneral use tolder.  MYFORD Bymed Gright 3 Jase Chucks.  Botte COLCHESTER / HARRISON D13 Berned 4 Jaur 8° light body independent chocks.  Botte RJM 4* Limiter / Vertical (Build in Extraction).  CLLNS various.  WILKS various.  Sit packaged POTTERY WHEELS, with and associated equipment.  Just in SFECAC Fooder type press HARRISON LIS Takebox.  As HARRISON LIS Metins Geartor.  As HARRISON LIS Takebox.  As HARRISON LIS Takebox.  As 100 Metins Geartor.  COMPARIS 24° hole cotter.  COMPARIS 24° hole cotter.  COMPARIS 24° hole cotter.  COMPARIS 25° hole cotter.  COMPARIS As 100 Metins Geartor.  ALAX 6° holestaw.  SURFACE States from 12° x 12° to 36° x 26°  Very note fit WEELS 11, no mobile garage crane, late blue colour.  ELLIOTT 100 STURCHARL Levitod head.  CLLIOTT 100 STURCHARL Levitod head.  SUBS / CEUCKES TERS STUCERT / MAS TERS Record head, faceplatest, medil large.  GOUNT STURGER STUDERT / MAS TERS Record head, faceplatest, medil large.  GOUNT STAN SAND SMITH 6° Hacketaw.  DOC ONLINEARS AND SMITH 6° Hacketaw.  DOC ONLIN   |   | 1975   |
| GARRIO DE 600 2, 20° Bors and Pan general use to bler MYFORD Browned Grights y Jane Chaules  Bore COLCHESTER / HARRISON D13 Burnerd 4 Jan 8° light body independent chocks  Bore RUH 4° Linisher / Vertical (Build in Estraction).  CLMS sarbus  MCROW ETERS and associated measuring tools:  S18 packaged MCROW ETERS and associated measuring tools:  S18 packaged MCROW ETERS and associated equipment  S18 packaged MCROW ETERS and associated equipment  S18 packaged MURITY WHEELS, kilns and associated equipment  S18 packaged MURITY WHEELS, kilns and associated equipment  Associated to Murity Country  MARRISON LS Marisock  NAM 910M NIW 2EALAND - Machine vice, 55mm, Javes precision ministure type deal towertical six and strails milling machines  S1° 1 TOWNOBILECRANE Manufactured 2000.  As re MITUTOTO grade A set of steps  MARLICO COUNTLES (champ type).  LOWARDS 20° tools colore  LINKS 5 no website crame + top hat  MITUTOTO 100-913 meets set miscometers  NORTON LEWARDS altop presset  LINKS 5 no website crame + top hat  MITUTOTO 100-913 meets set miscometers  NORTON LEWARDS altop presset  S18 ALAX 6° hadeaux  SUBFACE place from 12° x 12° to 36° x 26°  Very nice fit  WEERS 1'y not mobile garage stone, late blue colors  ELLIOTT 1'UV 3 champ Head  STELL STOCK Just amued.  10 oak  ELLIOTT UV 3 champ Head  SWOOL BLOCKS  SWOOL BLOCK   | STARTRITE 14-3-5 woodworking band saw                         | \$775  |
| MTRORD Burnerd Grigory 3 Jans Chuchs  COLICHESTER / HARRISTON D13 Burnerd 4 Jans 8* light body independent chocks  Blow  RUH 9* Linisher / Vertical (Build in Extraction).  \$120  MICRON ETERS and associated measuring soot:  S18 packaged  POTTERY WHEELS, silve and associated equipment  Just in  SFECAC Provider type press  HARRISTON LS flatteck  Ass HARRISTON LS flatteck  NEW STICKN NEW STICKN AND - Machine vice, 55 mm. Jians precision ministure type cleal towerted six and smolder milling machines  S2** 1 TOWNOSILECHARE Manufactured 2000  As rew  MITUTOTO grade is set of stigs  MARRICCO CAUSILEUTS (clear byte)  Full EDWARDS 24** hole cotter  LINKES 500 neither set of stigs  MITUTOTO 00-913 meetic set misconneters  NORTON / EDWARDS actor presses  SUBFACE places from 12* x 12* to 35* x 26*  Very nice fit  WEEER 11, no mobile garage crane, late blue colour  ELLIOTT 100 STURCHARL vertical head  SUBFACE places from 12* x 12* to 35* x 26*  Very nice fit  WEEER 11, no mobile garage crane, late blue colour  ELLIOTT 100 STURCHARL vertical head  SUBFACE places from 12* x 10* to 35* x 26*  Very nice fit  WEEER 11, no mobile garage crane, late blue colour  ELLIOTT 100 STURCHARL vertical head  SUBFACE places STURCHARL vertical head  ELLIOTT 100 STURCHARL vertical head  SUBFACE STURCES Just armised.  ELLIOTT 100 STURCHARL vertical head  ELLIOTT 100 STURCHARL vertical head  SUBFACE SUBCOX SUBCOX SUBCOX Mits of Theorems, New York of the Colour Sturf Church Subcox of Subc  |   | 9000<br>9005                                 |
| COLCHESTER / HARRISON D13 Burnerd 4 Jan 2* light body independent chocks Bore RJM 4* United (Build in Extraction).  ELRS surious Size of the Extraction of t   |   | Bored £250                                   |
| RUN 4* Unisher / Vertical (Build in Extraction).  (20)  MICAGN ETERS and associated measuring tools:  STR packaged POTTERY WHEELS, with and associated equipment.  STR packaged POTTERY WHEELS, with and associated equipment.  Just in SECAC Founder type press.  As: MARRISON LIS Marsic Coachor.  As: MARRISON LIS Marsic Coachor.  As: MARRISON LIS Marsic Coachor.  As: MARRISON MICW 22EALAND: Machine vice, 55mm. Jaws precision ministure type ideal tonertical six and smaller milling machines.  SP 1 TONMOBILECRANE, Manufactured 2000.  As res MITUTOTO Graphs A set of step.  MARLOO KNUFLUPS (citimp type).  J. EOWARDS 24* hole cross:  MITUTOTO 100-913 meters set micrometers.  MITUTOTO 100-913 meters set micrometers.  MITUTOTO 100-913 meters set micrometers.  SURFACE places from 12* x 12* to 35* x 36*.  Very nice in WEER 11; but mobile garage erane, late blue colour.  ELLIOTT 120 STURCHMILL vertical head.  One off (mar. MINUTOTO 100-913 meters placemal.  STREEL STOCK Just amued.  10 calls  STREEL STO   |   |  |
| MICROMETERS and associated measuring tools.  STEPACKEP WHEELS, kins and associated equipment.  Just in SPECAC Prouder type press.  Ass.  MARRISON LIS Messis Gearbox.  Ass.  MARRISON LIS Messis Gearbox.  Ass.  MARRISON LIS Teatrock.  NEW FRICKN NEW ZEALAND: Machine vice, 55 mm. Jaws precision ministure type ideal tonertical pix and smaller million machines and smaller million machines.  SP 1 TON MOBILECRANE. Manufactured 2000.  As res.  MITUTOTO Grade A set of step.  MARLOO KNUTLUDS (clamp type).  J. EOWARDS 24" hole outber.  Large bench vice.  LINK1 5 for website crame is top-hat.  MITUTOTO 100-919 messis set micrometers.  NORTON J EDWARDS after precision.  SURFACE places from 12" x 12" to 30" x 36".  Very nice fix.  WEER 11 by no mobile garage erane, late blue solow.  ELLIOTIT 100 STURCHMILL vertical head.  One off (mar.  AIRM Institet " wide bet, pademal.  STEEL STOCK Just amound.  10 calk  ELLIOTI 11" LIS Stomp Head.  STEELS CROCK A and U, many steel.  EDW SURFACE Macro Toneras, New Sets; 67 / 61 peoch.  EDWEST CRUCKS Grade A and U, many steel.  EDW SURFACE STOCK Sust amound.  10 Calk  EDWS CROCKS A subsequence of the sets of   | RJH 4* Linisher / Vertical (Build in Extraction)              | 1625   |
| POTTERT WHEELS, kites and associated equipment.  Just in SPECAR Fooder type press.  HARRISON LS Missis Geartor.  As HARRISON LS Missis Geartor.  NEW FRIGON NEW 2EALAND - Machine vice, 55 mm. Jiaws precision ministure type ideal tonertical six and smaller militing machines.  SP 1 TONIORISECRANE Manufactured 2000.  As remitted to the machine of the ministure type ideal tonertical six and smaller militing machines.  SP 1 TONIORISECRANE Manufactured 2000.  As remitted to the ministure of the ministure type ideal tonertical six and smaller militing machines.  SP 1 TONIORISECRANE Manufactured 2000.  As remitted to the ministure of the ministure type ideal tonertical six and s   |   | £200/(425                                    |
| SPECAN Founder type press  AARRISON US Mestic Gearbox.  MARRISON US Takenox  MARRISON US Takenox  MARRISON NIN TEALAND - Machine vice, 55mm. Saws precision ministure type ideal forvertical six and smaller milling machines.  SP 1 TON MOBILISORANE Manufactured 2000. As recommodified and smaller milling machines.  SP 1 TON MOBILISORANE Manufactured 2000. As recommodified and million of steps.  MARLOO COUNTLUTS (citimp type).  ALOWARDS 24" tole other.  Large bench vite.  LINKT 5 non vehicle crane + top hat.  MITUTOTO 100-913 meetic set micrometers.  MITUTOTO 100-913 meetic set micrometers.  Very nice fix.  MITUTOTO 100-913 meetic set micrometers.  Very nice fix.  WEBER 11, bin mobile garlage strone, see blue colour.  ELLIOTIT 100 STURROMELL vertical head.  STELLIOT UT 100 STURROMELL vertical head.  TONE OF (min MILLIO STURROMELL vertical head.)  STELLIOTIT 100 STURROMELL vertical head.  STELLIOTIT 100 STELLIOTIT 100 ASTER FOUND HEAD.  STELLIOTIT 100 STELLIOTIT 100 ASTER FOUND HEAD.  ST   |   |  |
| HARRISON LS Missis Gearbox.  As HARRISON NEW 2EALAND: Machine vice, 55 mm. Jaws precision ministure type deal towertical six and smaller milling machines.  SP 1 TON MORELECRANE Manufactured 2000.  As remaining machines.  SP 1 TON MORELECRANE Manufactured 2000.  As remaining machines.  SP 1 TON MORELECRANE Manufactured 2000.  As remaining machines.  SP 1 TON MORELECRANE Manufactured 2000.  As remaining machines.  IN TON MORELECRANE Manufactured 2000.  As remaining machines.  LINKT 5 too restricts est misconneters.  SP 1 TON MORELECRANES actor presses.  SP 1 TON MORELECRANES actor presses.  SUBSPACE places from 12" x 12" to 35" x 26".  Very nice for WEER 11, nor mobile garage crane, late blue colors.  ELLIOTT 100 STURCHMILL vertical hand.  SUBSPACE places from 2" x 12" to 35" x 26".  Very nice for WEER 11, nor mobile garage crane, late blue colors.  ELLIOTT 100 STURCHMILL vertical hand.  SUBSPACE places from 3" x 10" to 35" x 26".  STEEL STOOD STURCHMILL vertical hand.  ELLIOTT 100 STURCHMILL vertical hand.  ELLIOTT 10   | SPECAC Powder tipe press                                      | 1225   |
| NEW PILOM NEW ZEALAND: Machine vice, 55 mm. Jaws precision ministure type deal towertool six and smaller milling machines.  39° 1 TON MORILEC RANE Manufactured 2000.  As rew MITUTOTO Grade A set of step: MARILECO CNUMILLENS (cleared type).  F.J. ECWARDS 24° hole screer.  LINKT 5 ton website chare a top-hat MITUTOTO 100-913 mests set misconneters.  NORTON / EDWARDS actor presset  LINKT 5 ton vehicle chare a top-hat MITUTOTO 100-913 mests set misconneters.  NORTON / EDWARDS actor presset  ALAX 6° has lease.  SURFACE places from 12° x 12° to 36° x 26° Very nice fa WEBER 11's nor mobile garage crane, late blue colory.  ELLIOTT 100 5 TURCINIAL vertical head.  ELLIOTT 100 5 TURCINIAL vertical head.  ELLIOTT 100 5 TURCINIAL vertical head.  SWAGE BLOCKS.  J 8 S Universal grading vice.  EDW 5 CALLES: Grade A and 0, many steps.  EDW 6 CALLES: Grade A and 0, many steps.  EDW 6 CALLES (Charles A mod 0, many steps.  EDW 6 CALLES TO CALLES (Charles A mod 0, many steps.  EDW 6 CALLES TO CALLES (Charles A mod 0, many steps.  EDW 6 CALLES TO CALLES (Charles A mod 0, many steps.  EDW 6 CALLES TO CALLES (Charles A mod 0, many steps.  EDW 6 CALLES TO CALLES (Charles A mod 0, many steps.  EDW 6 CALLES TO CALLES (Charles A mod 0, many steps.  EDW 6 CALLES TO CALLES (Charles A mod 0, many steps.  EDW 6 CALLES TO CALLES (Charles A mod 0, many steps.  EDW 6 CALLES TO CALLES (Charles A mod 0, many steps.  EDW 6 CALLES TO CALLES (Charles A mod 0, many steps.  EDW 6 CALLES TO CALLES (Charles A mod 0, many steps.  EDW 6 CALLES TO CALLES (Charles A mod 0, many steps.  EDW 6 CALLES TO CALLES (Charles A mod 0, many steps.  EDW 6 CALLES TO CALLES (Charles A mod 0, many steps.  EDW 6 CALLES TO CALLES (Charles A mod 0, many steps.  EDW 6 CALLES TO CALLES (Charles A mod 0, many steps.  EDW 6 CALLES (Charles A mod 0, many steps.  EDW 6 CALLES TO CALLES (Charles A mod 0, many steps.  EDW 6 CALLES TO CALLES (Charles A mod 0, many steps.  EDW 6 CALLES TO CALLES (Charles A mod 0, many steps.  EDW 6 CALLES TO CALLES (Charles A mod 0, many steps.  EDW 6   | HARRISON LS Metric Geartex.                                   | As is \$250                                  |
| and smaller milling machines \$PT 1 TON MOBILE CRANE Manufactured 2000. As res MITUTOTO grade a set of stept. MASTLCC KNAST LERIS (clamp type). F.J. EDWARDS 24' hole enter. Large bench vise LINKE 5 ton website crane + top-hat MITUTOTO 103-913 medic set micrometers.  MITUTOTO 103-913 medic set micrometers.  TOTO 103-913 medic s  |   | \$245  |
| SP 1 TONMOSILECRANE Manufactured 2000. As rem MITUSTOTO protect A set of 1 style.  MARILOD KNUFFLER'S (clamp type).  F.J. EGWARROS 24" hole cotter.  LINKT,5 non vehicle crane * top hat MITUSTOTO 009-919 mestic set micrometers.  NORTON / EDWARROS abor presset.  MITUSTOTO 1009-919 mestic set micrometers.  Very note for WEEER 11, non mobile garage crane, late blue colour.  SURFACE plates from 12" x 12" to 36" x 36". Very note for WEEER 11, non mobile garage crane, late blue colour.  ELLIOTT 100 STURFORML vertical head.  One off (nan RUH finisher 4" wide bet, pedemal.  ELLIOTT 101/LIS Storing Head.  STEEL STOOK Just armed.  10 calls  ELLIOTT 101/LIS Storing Head.  STEEL STOOK Just armed.  10 calls  ELLIOTT 101/LIS Storing Head.  STURMOS BLOCKS.  E 105  SURFACE BLOCKS.  E 105  SURFACE STUDENT VAS STER Rese Sett; 67 / 61 pede.  EST STUDENT VAS STER RESPONDED to 12" of 1000 pede.  EST STUDENT VAS STER RESPONDED to 1000 pede (12" of 1000 pede).  SERIES STUDENT VAS STER Rese Sett; 67 / 61 pede.  EST STUDENT VAS STER RESPONDED to 1000 pede (12" of 1000 pede).  Med COUCHES TER STUDENT VAS STER ResPort Intend, floopblett, small / large  GUALTERS AND SMITH 6" Hackslave.  DOON Histories Bed Clamps (pair).  Special HEACH T-GAUGES by Chemisters.  Fig. TIAN SWAYU STEP Converter.  ELLIOTT 70M Shaper, 70" stervie.  Fig. TIAN SWAYU STEP Converter.  ELLIOTT 2001 STEP Converter.  ELIAN SWAYU STEP Converter.  ELLIOTT 2001 STEP Converter.  ELIOTT 2001 STEP Converter.  ELLIOTT 2001 STEP Converter.  ELLIOTT   |   | 444  |
| MITUTOTO grade A set of step.  MARILOD SUPPLICIPS (charge byps).  Full EXPERIENCE 24' hole cutter.  Large beach view.  LINKT 5 ton webbite crave = top-hat  MITUTOTO 103-919 seeks set micrometers.  CTO  AJAX 6' hackness  EXPERIENCE States from 12''x 12'' to 36'' x 36''  Very nice fit  WEEER 11', ton mobile garage crave, late blue colour  ELLIOTT 10' X 5' and seeks and the blue colour  ELLIOTT 10' / 10' 5 tomay Head  STEEL STOCK Just armed.  ELLIOT 10' / 10' 5 tomay Head  STEEL STOCK Just armed.  ELLIOT 10' / 10' 5 tomay Head  STEEL STOCK Just armed.  ELLIOT 10' / 10' 5 tomay Head  STEEL STOCK Just armed.  ELLIOT 10' / 10' 5 tomay Head  STEEL STOCK Just armed.  ELLIOT 10' / 10' 5 tomay Head  STEEL STOCK Just armed.  ELLIOT 10' / 10' 5 tomay Head  STEEL STOCK Just armed.  ELLIOT 10' / 10' 5 tomay Head  STEEL STOCK Just armed.  ELLIOT 10' / 10' 5 tomay Head  STEEL STOCK Just armed.  ELLIOT 10' / 10' 5 tomay Head  STEEL STOCK Just armed.  ELLIOT 10' / 10' 5 tomay Head  STEEL STOCK Just armed.  ELLIOT 10' / 10' 5 tomay Head  STEEL STOCK Just armed.  EDO COUCHESTER STOCK Just A STEER Revolute head, floorpletex, small / large  EDO COUCHESTER STUCKNIT AN STEER Revolute head, floorpletex, small / large  GOON Machine Bed Clamps [pair].  Special  HEROST GAUGES Steep (A steele Steep   |   | As rew 1375                                  |
| F.J. COWARDS 24" Role cutter. LINKT.5 too webbile careve = 10p-hat MITUTOR 0.103-919 seeks set micrometers UNKT.5 too webbile careve = 10p-hat MITUTOR 0.103-919 seeks set micrometers  (275 AJAX 6" hackness SURFACE places from 12" x 12" to 36" x 36" Very nice fit WEEER 11, ton mobile garage cares, late blace colour ELLIOTT 100 51 WRIDINGLU vertical head AUH insther 4" wide bet, padestral STEEL STOCK Just armed. ELLIOT 101 (10) Screen Head SWINGE BLOCKS.  2 to 30 2 & 90 reversal gending vice EDIT 4 (10) Screen Head SWINGE BLOCKS.  EDIT 50 CAUCHESTER STUDENT AND SERVING STOCK ST   | MITUTOTO grade A set of stes                                  | 1245   |
| Large bench vise LINK1 5 to webble crace = top-hat MITUTOTO 100-919 meetic set micrometers NITUTOTO 100-919 meetic set micrometers SURFACE places from 12" x 12" to 35" x 36".  Very nice for WEER 11 by on mobile garage crace, lare blue colour ELLIOTT 100 STROMBILL vertical head.  One off (nan AINH finisher 2" wide beit, pademal.  STEEL STOCK Just amued.  10 calle ELLIOT 11" kill 5 change Head.  STEELS TOCK Just amued.  10 calle ELLIOT 11" kill 5 change Head.  STEELS TOCK Just amued.  10 calle ELLIOT 11" kill 5 change Head.  STEELS TOCK Just amued.  10 calle ELLIOT 11" kill 5 change Head.  STEELS TOCK Just amued.  10 calle ELLIOT 11" kill 5 change Head.  STEELS TOCK Just amued.  10 calle ELLIOT 11" kill 5 change Head.  STEELS TOCK Just amued.  10 calle ELLIOT 11" kill 5 change Head.  STEELS TOCK Just amued.  10 calle ELLIOT 11" kill 5 change Head.  STEELS CALLES Change A and U, many steel.  ELLIOT 11" kill 5 change Head.  10 calle ELLIOT 10" kill 5 change Steels  |   |  |
| LINKT 5 ton vehicle crane = top hat  WITUTOTO 103-913 meetic set micrometers  NORTON / EDWARDS autor presset  \$75  AJAX 6* haclesse  SURFACE places from 12* x 12* to 36* x 36*  Webst 11, ton mobile garage crane, late blue colors  ELLIOTT 200 51WRDMRL vertical head  AJAH finisher ** wide bet, padersal  ELLIOTT 100 51WRDMRL vertical head  TO call  ELLIOTT 101 / US disming Head  STEEL STOOK Just armoid  ELLIOTT 101 / US disming Head  SWAGE BLOCKS.  \$ 120  3 \$ 0 diseased grading vide.  BOX TABLES: Grade A and 0, many steel  BOX TABLES: Grade A and 0, many steel  BOX TABLES: Grade A and 0, many steel  COLCHESTER STUDENT VM STEP Report head, faceplates,mall large  GUALTERS AND SWITH 6* Hacksize.  Boxing Heades 2.7 shows, R8 Taper, Mar. Capacity 416* sound bar.  DOON Machine Bed Clamps (pair).  Special  BEROST GAUGE Shaper, 70 sterles  DE Boxes  Fra  TIAN SWAYE 5518* Converter  TIAN SWAYE 5518* Converter  ENA SWAYE 5518* CONVERTER C  |   | \$505  |
| MITUTOTIO 100-913 meetic set micrometers  NORTON I EDWARDS a More presses  276  AJAX 6* hackesse  SURFACE places from 12" x 12" to 36" x 36"  WEEER 11y bit mobile garage state, less blue online  ELLIOTIT 100 STRUBGRIEL vertical head  One off (nan AJM 1 institut of wide beit, pedicitat  STEEL STDOK Just armed  ELLIOTIT 104 Strong Head  STEEL STDOK Just armed  ELLIOTIT 105 Strong Head  STEEL STDOK Just armed  EULIOTIT 105 Strong Head  EULIOTIT 105 Shaper, 105 strong  EULIOTIT 105 Shaper, 105 strong  EULION HEAD STORY STRONG  EULION HEAD STORY STRONG  EULION HEAD STORY STRONG  EULION HEAD STRONG STRONG  EULION HEAD STRONG STRONG  EULIOTIT 105 Shaper, 105 strong  EULION HEAD STRONG STRONG STRONG  EULION HEAD STRONG  | LINK1.5 too webble crave + too har                            | 970  |
| AJAX & hadistaw SURFACE plates from 12" x 12" to 36" x 36" Weep nice for WEER 11, ten mobile garage crane, lete blue colour ELECTT 120 on mobile garage crane, lete blue colour FURI similar 4" wide beit, padermal STERLS STOCK JUST Amuel STOCK JUST Amu   |   | 1276   |
| SURFACE places from 12" x 12" to 36" x 36"   | NORTON / EDWARDS arbor pressed                                | \$75/\$145                                   |
| WEEER 11, for mobile garage crane, lase blue colour ELLIOTT 100 STURDINGHLU vertical head  One off (man Ruhl insther 4" wide beit, padecrail  STEES, STOOK Just arrand  ELLIOT U17 (10) Skrming Head  STEES, STOOK Just arrand  ELLIOT U17 (10) Skrming Head  STEES, STOOK Just arrand  ELLIOT U17 (10) Skrming Head  Mer COUCHESTER STUDENT VIA STEER Round head, floopletext,amell / large  ELLIOTT U17 (10) Skrming Head  ELLIOTT U17 (10) Skrming Head  ELLIOTT U18 Shaper, 10) strole  DE Boxes  Fin ELLIOTT U18 Shaper, 10) strole  ELLIOTT U18 STEAP Converter  ELLIOTT U18 CONVERTER  ELLIOTT U18 CONVERTER  ELLIOTT U18 CONVERTER  ELLIOTT U18 CONVERTER  ELLIOTT U17 (10) Converter  ELLION SWAY (10) Converter  | AJAX 6" hacksaw   | \$405  |
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| Right insther ** Wide bet, padestall   STEEL STOOK Just arraned   10 call   ELLIOT U17 U2 Setting Head   10 call   ELLIOT U17 U27 U27 U27 U27 U27 U27 U27 U27 U27 U2   | ELLIOTT 1250 STURDIMILL vertical head                         | One off (max) \$1005                         |
| STETL STOCK Just arreid.  ELLIOT UT / US Straing Head.  SWAGE BLOCKS.  J & S One-mail greating wee.  SECT TABLES (drack A and U, many steel  | Pully fnisher 4" wide belt pedestal.                          | 1345   |
| SWAGE BLOCKS.  \$ 130 SWAGE BLOCKS.  \$ 130 SWAGE BLOCKS.  \$ 140 SWAGE SWAGE A and \$ 0, many step \$ \$ 150 \$ 15 | STEEL STOCK Just arrived                                      | to callers only                              |
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| HERORT GAUGES by Chememan, Shardow, Moore and Wright Fro ELLIOTT 10M Shaper, 10" stroke DE Boxes FR THAN SWAYE 316" Conventor THAN SWAYE 356" Conventor THAN SWAYE 556" Conventor THAN SWAYE 556" Conventor THAN SWAYE 556" Conventor THAN SWAYE 756" CONVENTOR THAN THAN THAN THAN THAN THAN THAN THAN  | ODONI Machine Bed Clamps (pair)                               | Special 124 50                               |
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| TRANSWAYE TEX: RT sotary conventors. CROWPTON PARKINSON V <sub>4</sub> HP, estillent mount, Bootbel / Myland Super 7 Type motor. Ne  | TRANSWAYE 55HP Goowley  | New 1305                                     |
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- Very solid counter with easy to read green LED disput
- Models available for Lathes and Milling Machines
- 2 & 3 Axis systems
- Auxiliary display for dine information on all settings
- Resolution 0.005mm

Standard scalle units with high accuracy

- Top quality rubber lips t avoid **contamination**
- Reading head with notbust
- Armoured signal cable (3m standard længth)

#### Scale reference points at 50mm pitch to determine datum point

- Most models available for Lathes and Milling Machines
- **Enhanced vibration**



- Centre height: 105mm
- Maximum swing: 210mm
- Distance between centres:
- 435mm
- Spindle bore: 20mm
- Spindle taper: MT3
- Spindle spe 125 - 2000 RPM
- Range of metric threa 0.4-3mm
- Range of imperial thread 10-44tpi
- Tailstock taper: MT2
- Topslide travel: 75mm:
- Crosslide travel: 110mm

 Tailstock travel: 70mm Motor: 3/4 HP

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Including VAT & UK Delivery

- Weight: 125kg
- 3 Jaw chuck
- 4-Way toolpost
- Lathe tools
- MT3 and MT2 steel centres
- Hardened and groun bedways
- Vee bedway
- 4 Jaw chuck
- Steady rest
- Follow rest
- Tray and splashguard



- Swing over bed: 420mm Distance between centres: 500mm
- Mill drill spindletteper: WIT3
   Tailstock barrel travel: 80mm
- 7 speeds 60 1300 RPM
- Swing over slide: 160mm
- Spindle taper: MT3
- Draw bar: M12 Cross slide travel: 180mm
- Motor: 3/4 HP
- Net weight: 155kg
- 4" 3 jaw chuck
- 2 dead counthess
- 1/2 drill chuck
- Change gears MT3 chuck arbor



- Swing over bed: 250mm
- Swing over cross slide:
- Distance between centres: 550mm
- Spindle bore: 19mm
- Taper in spindle no
- Motor: 1/2 HP
- 6 speeds 125 2000 RPM
- Speed range variable: 100-2500 RPM



- Net weight: 130kg
- Spindle taper MT3
- Head travel: 215mm
- Speed variable
- Range: 0-3,000 RPM
- Motor: 1/2 HPNet weight: 45kg

Call today for our latest **Tool Catalogue** 01244 - 531631

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