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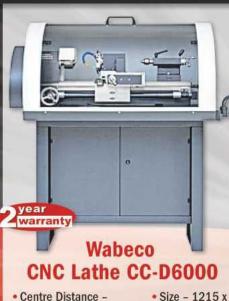
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On the **Editor's Benc**

Season's Greetings

When I was a youngster I used to get very confused by the fact magazines on sale were always dated a month early. Since then I've learned it's all about them sitting on the shelves for up to a month and the vendors not wanting them to appear out of date. At the risk of shaking the foundations of the publishing world, however, I've decided to

use this issue to send you the best wishes for Christmas and the New Year from everyone at Model Engineers' Workshop and MyTimeMedia.

Special thanks go to Dave, the ME forum's SillyOldDuffer for creating our cover image with the power of Photoshop – please don't write in with health and safety warnings about operating a mill adorned with fairy lights...

On My Bench

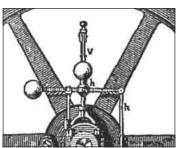
To confess, my bench is a scene of chaos at the moment – probably a good thing as it means I'm getting a bit busier with several projects moving forwards.

The recent weather inspired me to dismount my weather station (which hasn't worked for a few years) from it's very long pole. After removing various bits of wildlife (spiders, harlequin ladybirds and lichen growing in my anemometer!) the main problems were that the wind vane had lost its tail and the anemometer had seized completely. Forty minutes of ultrasonic shaking in corrosion remover freed up the aluminium body, but the ball races are well past redemption. I can salvage the body but the rest needs rebuilding.

I successfully cast a complex little governor bracket for a stationary engine, which then demanded some delicate machining. A thick base that was machined off at the end made this much easier, so the next job is the governor itself.

Naturally I'm sure you would be disappointed if I wasn't doing some 3D printing as well. My 1/6 Vickers Light Tank's turret is taking shape in stages, it's rather big so the main shell is in ten parts. I've discovered that a leading brand of superglue, despite being a gel does NOT have gap filling properties and have had to resort to epoxy instead.



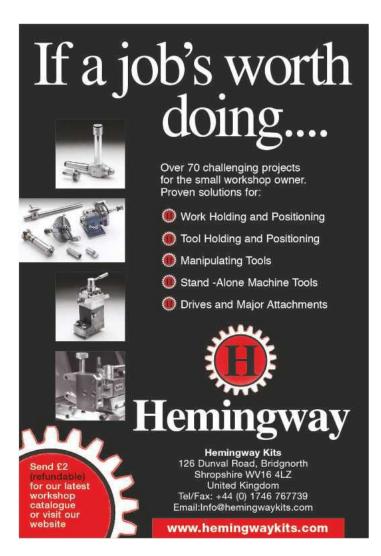


John Stevenson Trophy

I'd like to thank everyone who so generously contributed towards a John Stevenson Trophy. The details of the trophy competition will be announced in the New Year, in time for the first award to be made at the Doncaster show.

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050-110-25510	ER25	MT3	M12	£79.24
050-110-25520	ER25	R8	7/16" UNF	£83.40

ER32 Milling Collet Chuck Sets with 6 Collets



- Choice of Taper Shank.
- Collet Nut Type: T2.
- . Collet Nut Thread: M40x1.5.
- Collets Included: 6mm, 8mm, 10mm, 12mm, 16mm and 20mm.
- 'C' Spanner: Included.

Code	Size	Shank	Drawbar Thread	Price
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E. & O. E.

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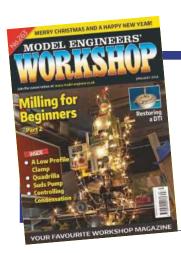
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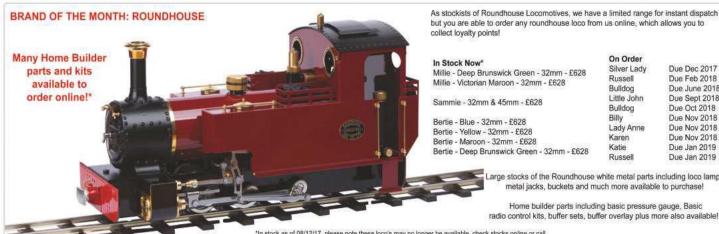
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A modern approach to Condensation Management



Silly Old Duffer uses an Arduino Uno Microcontroller to monitor and manage a condensation problem.

ondensation is quite a problem, **photo**2. Not only is it the bane of many a home workshop, it causes serious damage in warehouses, homes, factories, construction projects, museums, and other public buildings. I'm lucky; my workshop does not suffer from condensation. Unfortunately, my home's entrance hallway has become vulnerable since double-glazing and a well-sealed front-door were installed two years ago. A desire to stop mould and disintegrating wall-paper led to this project, but the principles apply to a workshop too.

Air contains water vapour and, in certain conditions, that moisture will condense on a cold surface. Condensation deposits water in the form of micro-droplets rich in dissolved oxygen. Air-born moisture is highly penetrative and capillary action finishes the job. Metal, glass, walls, ceilings, and electronics are all vulnerable. Corrosion,



RaspberryPi Data Logging the Arduino in a Damp Hallway



Condensation – a warning

water-damage, malfunctioning electronics and mould are all likely consequences. In serious cases there is risk to health. Metals are particularly vulnerable to condensation because of their good thermal conductivity.

Quite a lot of advice available on condensation can be misleading. Not that it's wrong, but rather that it comes from people who have dealt with their particular problem in their particular way. Many suggestions are based on experience and – as we all know – experience is built on a dung-hill! The underlying issue is that the method used to solve a winter condensation problem in a shed in Yorkshire is unlikely to work well in Florida, Sukkur, or Darwin. The advice might even be entirely the wrong thing to do.

As always in Engineering it is best to understand what lies behind a problem before trying to fix it. Once understood, root-causes can be tackled and a generic solution developed, **photo 3**.

>

There are four inter-linked factors that determine whether or not water vapour will condense on an object or not. They are: the temperature of the object itself and the temperature, relative humidity, and pressure of the air. Fortunately, air pressure has a relatively small effect and can be ignored for our purposes. Figure 1 graphs the relationship between dew point, air temperature and relative humidity. Air temperature and humidity are the main drivers but their relationship to the likelihood of condensation is not immediately obvious. However, if ambient temperature and relative humidity are measured, it's possible to calculate the dew point. Dew point is defined as the maximum temperature at which water vapour will start to condense. An object below dew point temperature will collect condensation from the air. Changes of temperature or humidity inside a workshop can cause condensation on any object below the new dew point. And moving metal or electronics from cold storage into a warm workshop is risky.

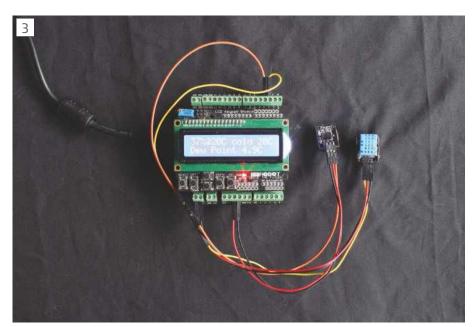
Writing this article at my dining table I see that the ambient temperature is 20°C and that the relative humidity is 41%. Those two numbers mean I'm physically comfortable. They also mean that the dew point in my dining room is about 5.9°C. From this I can predict that a cold drink taken out of my refrigerator at 4°C will collect condensation whilst a can from my larder at 10°C won't. Confirmation that the prediction is correct can be seen in **photo 4**.

At 25°C / 41% RH the dew point rises to about 9C: this suggests that whacking heat into a cold workshop is more likely to cause condensation than letting the room and its contents warm up slowly together.

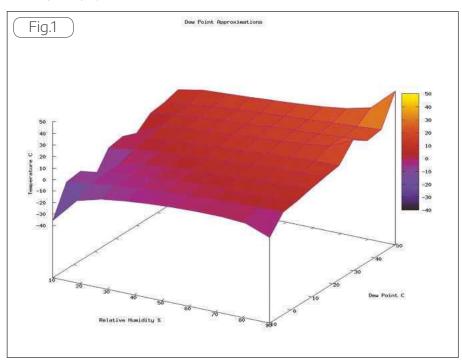
Temperature and humidity vary hugely outside my West of England dining room. Climate and weather make a huge difference as do man-made conditions in the room itself. Condensation occurs in hot humid countries as well as cold ones: it all depends on the dew point. Kitchens and Bathrooms are much more likely to be humid than an unoccupied bedroom. Apart from condensation, excessive humidity is bad for another reason. Life becomes very uncomfortable when high-humidity prevents sweat cooling by evaporation. Very few of us would choose to indulge our hobby in a sauna!

The most important point is that it is the combination of temperature and humidity relative to the temperature of an object that matters. A complication is that humidity and temperature are both influenced by a combination of natural and man-made factors. Both factors are changeable and, without measurement, it's difficult to know which individual countermeasure is appropriate. This is why simply heating a workshop sometimes controls condensation and sometimes it doesn't.

When it comes to counter-measures there may be obvious preventatives. Open flames and boiling water are prodigious



The completed project



dew point, Air Temperature and Relative Humidity

sources of water vapour, best avoided. Unwelcome visitors. Better ventilation will help. A vent near floor level works better than an open window because air laden with water vapour tends to sink. Self-contained oil or gas heaters are to be avoided; without a chimney water produced by combustion is dumped straight into the air in the room. A workshop suffering from rising damp, dripping plumbing, porous walls or a leaky roof needs to have these problems fixed first. Restricting airflow by keeping small tools wrapped up in boxes and by providing covers for large tools and stock will help. Wooden tool boxes are better than metal ones. Corrosion due to condensation can be reduced by keeping metal surfaces painted or well oiled. Some coolants are water based and their

evaporation should be reduced if possible. Chemical absorbent dehumidifiers and anticorrosion paper may help.

Varying the temperature of a workshop by heating is likely to cause condensation unless the temperature is never allowed to fall below 16°C. If heating alone is used it is important that the room be well ventilated. Proper ventilation is more than cracking open a window! It means that a flow of air will be maintained, and that incoming air will be dry. Cost is the chief objection. Keeping a well ventilated workshop permanently at or above 16°C could be expensive!

A newly built workshop is a special case. It may need to be thoroughly dried out before use. New concrete, plaster, and other construction materials are wet, wet, wet. A



Prediction Confirmed - Cold Can on the Right

period of ventilation, perhaps fan-assisted, is in order until the damp has dispersed. A lean-to workshop erected against the weather side of a house may be very damp until the house wall has had time to dry out.

Once basic counter-measures have been taken we can concentrate on dew point issues. Comparing the dew point and temperature of a condensation prone object will tell us when the combination of temperature and humidity is going to cause trouble. Sounding a simple alarm may be sufficient. Prompting the operator to improve ventilation by opening a window or turning an extractor fan on may be all that's needed. But beware - this makes the risky assumption that fresh air is less humid than workshop air!

Provided we understand what causes condensation and have a way of measuring the factors, an engineer can look at ways of preventing condensation with active controls. Possibilities include:

- 1) Heating to make individual objects warmer than the dew point. Keeping lathes and milling machines above the dew point by attaching a small electric heater to the body works.
- 2) Increase the dew point by cooling the air, not likely to be practical.
- 3) Reduce humidity by switching a on dehumidifier with a humidistat.
- 4) Maintain temperature and humidity with an air-conditioning unit.

Air-conditioning is much used in industry to prevent condensation. In humid climates air-conditioning is desirable in domestic buildings for comfort and might already be fitted to a home workshop. The main objection to air-conditioning is cost. Cost is particularly objectionable in moderate climates were condensation and high humidity are unpredictably intermittent. In these circumstances a portable dehumidifier is more appropriate, small units starting at about £60. A 300W humidifier capable of extracting up to 20



A 300W Dehumidifier

litres of water per day from a decent sized room costs about £150. Dehumidifiers work by blowing air through a chiller kept just below the dew point, **photo 5**. Water vapour condenses on the chiller and is collected in a tank. Dry air emerges on the other side and clean water is a useful byproduct. In larger rooms it is important to ensure that air is thoroughly circulated. If not condensation may still occur in remote corners.

It's important to ensure that dehumidifiers and air-conditioning units are not overstressed by asking too much of them. They can only control air-quality within a limited space. Open doors and windows will cause a dehumidifier to try and dry out the world. For this reason, joint use of good ventilation and a dehumidifier is a no-no.

Calculating the dew point

Wikipedia documents a number of formula for calculating the dew point. They are of varying accuracy. The simplest formula only works when humidity is greater than 50%. More accurate approximations involve the use of constants tweaked to improve dew point accuracy within a target temperature range.

Given accurate data the literature suggests that the approximation I used will vary from the actual dew point by no more than 0.4%. That potential is not achieved here because the temperature and relative humidity data delivered by the sensor I used are inferior. Small program changes would allow more accurate sensors to be used.

The calculation is (temperature in Celcius): constant b = 17.67 constant c = 243.5

gamma = log(relative_humidity / 100) + ((b * temperature)) / (c + temperature)) dew_point = c * qamma / (b - qamma)

Measuring relative humidity

Relative humidity may be calculated by comparing temperature readings from a matched pair of thermometers, one of which is cooled by keeping the bulb wet. Being wet, the bulb measures temperature at 100% humidity. The other thermometer measures actual temperature, and the difference between 'dry-bulb' and 'wet-bulb' measurements is proportional to the relative humidity of the air, from which the actual relative humidity may be calculated.

Another way of measuring humidity is with a hygrometer made from human hair. A strand of hair under load has the interesting property of lengthening with increasing humidity. In a typical instrument three twisted strands of hair about 200mm long move a pointer against a scale. The hygrometer is calibrated with web-bulb/dry-bulb thermometers but is less accurate.

In the good old days, chaps sat recording wet-bulb/dry-bulb temperature pairs manually and calculated humidity from them later. Later, rather expensive pen-recorders were used to collect the data, but the calculations remained tedious. We don't have to do that today. This is just as well, because I didn't fancy spending an uncomfortable night in my workshop, not at my age.

Table 1 allows dew points to be found from air temperature and relative humidity. It is handy when moving items from hot to cold environments.

The table is used as follows. Use the intersection of workshop air temperature in the left-hand column and select humidity from the top of the table. As an example, the intersection of 20°C°C and 45% RH is a dew point temperature of 9°C. Therefore, a sheet of metal moved into the workshop from a cold store below 9°C will collect condensation. The same metal sheet will not collect condensation if it is 11°C or warmer.

>

The Electronics

This project uses an Arduino Uno

Table 1

dew point from Air Temperature and Relative Humidity Table

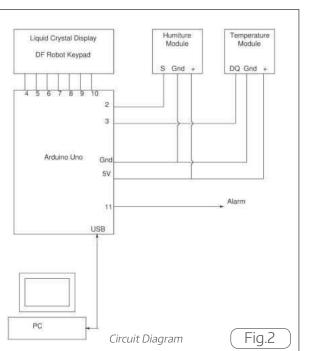
Relative Humidity %				
Air°C	100	95		

	пиннину	,,,												
Air °C	100	95	90	85	80	75	70	65	60	55	50	45	40	35
41	42	41	40	39	38	37	36	34	33	32	30	29	27	25
39	40	39	38	37	36	35	34	33	31	30	28	27	25	23
37	38	37	36	35	34	33	32	31	29	28	26	25	23	21
35	36	35	34	33	32	31	30	29	27	26	25	23	21	19
33	34	33	32	31	30	29	28	27	26	24	23	21	20	18
31	32	31	30	29	28	27	26	25	24	22	21	19	18	16
29	30	29	28	27	26	25	24	23	22	20	19	18	16	14
27	28	27	26	25	24	23	22	21	20	19	17	16	14	12
25	26	25	24	23	22	21	20	19	18	17	15	14	12	10
22	23	22	21	20	19	18	17	16	15	14	13	11	10	8
20	21	20	19	18	17	16	15	14	13	12	11	9	8	6
18	19	18	17	16	15	15	14	12	11	10	9	7	6	4
16	17	16	15	14	13	13	12	11	9	8	7	6	4	2
14	15	14	13	12	12	11	10	9	8	6	5	4	2	1
12	13	12	11	10	10	9	8	7	6	4	3	2	0	
10	11	10	9	8	8	7	6	5	4	3	1	0		
8	9	8	7	6	6	5	4	3	2	1				
6	7	6	5	4	4	3	2	1						
4	5	4	3	3	2	1								
2	3	2	1	1										

microcontroller, a temperature sensor and a humiture sensor to take readings and do the calculations. A humiture is a portmanteau word for a single sensor that measures both humidity and temperature. It is used to measure air temperature and

humidity. A separate temperature sensor is stuck to a suitable 'cold-object'. The microcontroller polls the humiture and temperature sensors at a set time interval (4 seconds), collects data, performs a

calculation, and reports results. It is also able to make decisions based on data, for example to raise an alarm if condensation is likely. The microcontroller is easily reprogrammed to add or refine functionality. The basic circuit, fig. 2, is simple. No soldering is needed if built as shown in photo 6 using an Arduino Uno, a terminal shield, an alarm module, humiture module and temperature module, with inter connections using female to male breadboard connector jump wires. (Search the web for breadboard connector or breadboard jumper).



Functions provided

The completed project provides some useful functions. Temperature, relative humidity and the resulting dew point are all displayed giving an immediate indication of the likelihood of condensation. The humiture may be moved into nooks and

crannies to search out sources of damp, though remember to allow a few minutes between each reading. If a condensation alarm is required, the body of the second temperature sensor should be bluetacked to a suitable cold object: one on which condensation is likely to occur. This could be a window pane, lathe, exterior metal door, or lump of metal in storage. Anything that has already attracted condensation is suitable.

Another useful feature is that the program outputs timestamped data on the Arduino's USB port. A terminal emulator or data capture program on a host computer can capture that data for later analysis. After 'Data Logging' it is possible to graph changing temperature and humidity over an extended period allowing the times that condensation occurs to be identified. Values are sent to the data logger once per minute.

The Arduino is programmed to output high (+5V) on pin 11 whenever the dew point / cold object comparison indicates that condensation is likely. An asterisk appears on the LCD. Pin 11 could be used to sound an alarm (such as the YL-44 Active Buzzer Module) or to operate a 250VAC 10A relay relay module. This last would allow the Arduino to switch on a dehumidifier unit or a heater. I shall

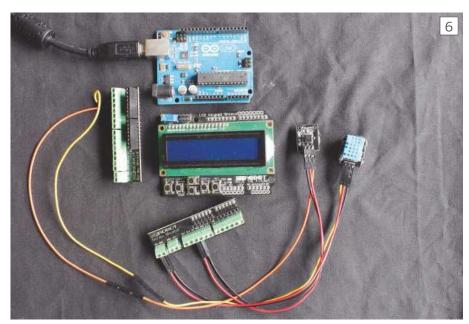
30	25	20	15	10
23	20	17	14	9
21	18	15	12	8
19	17	14	10	6
17	15	12	9	5
16	13	10	7	3
14	11	9	5	1
12	10	7	4	
10	8	5	2	
8	6	4	0	
6	4	1		
4	2			
2	0			
1				

provide no more than a circuit diagram, **fig. 3**, It is not difficult to build but constructors will have to provide their own understanding of mains powered safety issues and the need to provide a proper enclosure, appropriate components and suitably engineered wiring.

Arduino and sensors

The sensor is a DHT11 humiture device pre-wired into a Keyes module. Humiture modules are widely available from a variety of vendors. Mine came in a set from SunFounder via the web. The DHT11 is the most basic of a family of similar sensors, the others providing more accuracy and precision whilst operating over a wider range of temperature. The DHT11 measures temperature between 0 and 50°C ±2°C and relative humidity in the range 20 - 90% ±5%. This is sufficient for this project.

There are three connections to the sensor +5V, O (GND), and Signal. Some variants of the module have four connections, one of which is unused. The connections will be marked +, -, S or similar. The DHT11 spends most of the time asleep. It is queried by pulling the signal line down to zero volts and negotiating a short handshake. After a short wait the DHT11 replies by sending a 40 bit binary number back down the signal line. Binary O and binary 1 are differentiated by



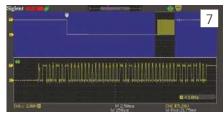
Project Ready for Assembly

the length of pulse: 26-28uS means 0, 70uS means 1, **photo 7**. At least two seconds should be allowed between queries.

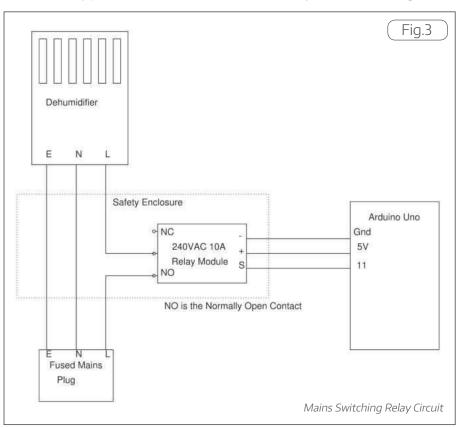
Programming the DHT11 is beginning to look like hard work now that we know that there's a handshake, time dependencies, and a requirement to decode 40-bit variable length numbers! Consequently, you will be pleased to hear that Arduino libraries are available to do the heavy lifting. I used the SimpleDHT library. It provides a function that queries the DHT11, decodes the 40-bit reply, and returns the temperature in Celsius and the percentage relative humidity, just like that.

The Arduino Uno was bought online from www.arduino.cc It is plug compatible with the screw terminal shield and Liquid Crystal Display used.

To be continued



Humiture Response Waveform, Magnified



Bulk Production of Toolholders



Richard T. Smith describes some approaches useful whenever you need to make a batch of matching parts.

revious articles described my prototype tooling system which included one insert holder. I subsequently bought a selection of inserts being three for steel with tip radii of 0.2, 0.4, and 0.8mm and two for aluminium with tip radii of 0.2 and 0.4mm - so I needed five more insert holders complete with pillars.

I started with the pillars. Their height is the most critical dimension – they all need to be the same height so that the handle clamps tight in the same place. The M10 thread of the clamp has a pitch of 1.5mm which corresponds to 360 degrees of position variation. So .01mm variation produces (360/150 = 2.4) degrees variation. Some variation up to ten degrees or so would not be a problem.

First thing was to check that the adaptor plate front edge (which the parting tool locates against) was square with the lathe, photo 1.

I bought some 11/4 ins. Diameter EN1A mild steel and cut off a piece and held it in the three-jaw chuck with 70mm sticking out and faced the end. Then I turned 55mm down to 30mm. dia. and drilled an 18mm diameter hole down the centre with the full bore to the same depth. As a guide I put a piece of tape on the tailstock quill to mark the start point and cut a piece of card to use as a depth gauge, **photo 2**. I changed to the parting off tool and cut off approximately 26mm, then changed back to the turning tool and faced the end, then back to the



Squaring the adaptor plate

parting tool to part off the second piece. I repeated this until I had a dozen parts - I decided to make some spares while I was

The problem then was how to finish these to an exact length and bore them to go over the 20mm diameter cylindrical nut. If I held them in the three-jaw chuck there

would be marking, unless something soft was placed around the part and this could lead to error. There is also the problem of measuring the part length while held in the chuck. I could have held the part away from the chuck face enough to get a calliper jaw into the gap although I really wanted to use a micrometer to measure. Each of the

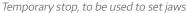


Card depth gauge



Grooving the soft jaw material







Facing soft jaws

dozen parts would have to be individually measured. I looked at articles about making 'spiders' as depth stops and I am sure I'll end up making one some day. In the end the soft jaw approach with a pocket to accurately locate the part seemed the best approach.

Looking around I found a short length of 11/2 ins. Square aluminium enough to cut three pieces slightly longer than the chuck jaws. A drawing confirmed that this could work. The first step was to mill a 20mm deep groove to fit over the jaws. Some time back I had bought a 10mm diameter endmill specifically for aluminium but had no way of holding it. All my cutters have been threaded shank and this was plain. I have not long made a spindle lock for the mill (see MEW 261) so was happy to buy a 3MT x 10 collet to hold this cutter. The spindle lock is functional but still needs tidying up, it wasn't drawn and evolved as I went along. The cutter was very impressive, and I made the groove a snug push over the jaws, photo 3. Next, I cut the piece into



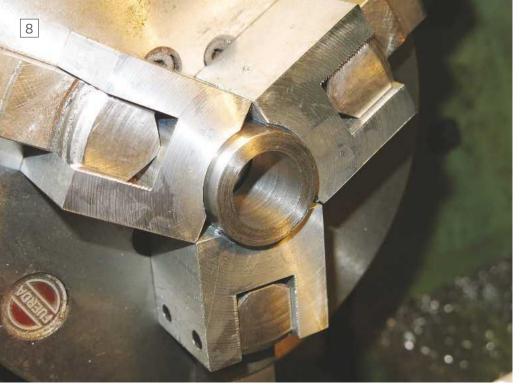
Setting with spacer



Trialling boring bar depth

three and drilled and tapped two M6 holes into each piece and fitted flat headed grub screws. To give the soft jaws something to grip on while the pocket was bored I needed something to be held right at the back of the jaws past the end of the pocket and about 8mm long. I got the diameter - 22mm, from the drawing and in order to position it and remove it decided to use an M6 screw into a central threaded hole. To make it easy to locate I made it stepped to a larger diameter. This was the next thing to make, **photo 4**. I fitted the soft jaw blanks to the chuck and gripped a piece of 25mm diameter aluminium tightly and faced off the ends. These faces locate against the chuck, so I cleaned up the edges and numbered them and then fitted them back on the chuck. I then tapped the jaws down against the chuck body then gripped the bar again tightened up the grub screws and faced off the second set of ends, **photo 5**. Removed the bar and put in the stepped spacer using the M6 screw to position it, photo 6, then removed the screw. Now I

>



Testing fit of part in soft jaws

could bore the pocket. Fitted the boring bar and set the saddle stop so that the boring bar wouldn't reach the stepped spacer, photo 7. Bored out until one of the parts just fitted then added a touch of depth with the topslide and faced the bottom of the pocket and slightly past the full diameter to relieve the corner.

To finish the parts I decided to trim them in two stages, the first to about 25.5mm and the second to final length. I positioned the tool approximately correct and zeroed the scale on the topslide handwheel, checked the topslide still had some movement and locked the carriage. Loaded the first part, photo 8, and took a cut and then removed it and measured it with the micrometer. There was a little variation around the circumference, but the basic length was 25.63mm. I repeated this for all the parts measuring each time and getting virtually the same results each time. I then advanced the topslide by 0.63mm and went through them all again. Unlocked the carriage and fitted the boring tool and bored the first part out until it slid over a test gauge. Zeroed the cross-slide scale and changed the part. Bored it out to the zero, filed the edge and used some emery tape to clean up the corners then checked with the gauge before removing the part. The inner end of the bore needed cleaning up and I used a small needle file and emery tape to deburr it. This was repeated for all the parts.

The insert holders are made from 40 x 20 bright mild steel bar and the nominal overall finished length is 75mm. I cut six blanks with the bandsaw 78mm long and squared one end in the lathe as the next one was sawing. The blanks were gripped in the 4-jaw chuck approximately centred and faced off. When all six were done I centre drilled the position of the 30 bore hole, holding them in the vice on the mill against

To mount the blanks in the four-jaw chuck I made some more soft jaws. The blank sits on the first step of the jaws and the jaw must not overlap the hole which is to be bored. Two jaws gripping the width of the blank are in line with the hole and needed packing (soft jaws) to achieve this. The sawn end of the blank was OK and gripped straight onto the blank. I made another soft jaw for the opposite end partly to avoid marking the machined end of the blank and partly to improve the balance. The jaws were made from 40 x 10mm aluminium as a tight fit over the steel jaws and with grubscrews in one side as backup,

The soft jaws were fitted, and the first blank positioned using the centre in the tailstock in the centre drilling in the blank to locate it, **photo 10**. I have a sharp 18mm drill which I used before boring out (300 rpm). The first blank I bored to size (800 rpm) then took a 0.4mm facing cut. This left a very ragged finish on the hole so subsequently I faced after drilling before boring. The facing cut was to provide a



Soft jaws for four jaw chuck



Positioning first blank

location at right angles to the bore which could be clamped to the mill table before cutting the insert seat. To change blanks, I loosened the sawn end jaw and one side jaw. Having finished the batch I realised that the holes were all very slightly off centre. I am not sure if the error was made drilling the centre holes or when clamping in the chuck.

In order to mill the step for the insert to sit on I clamped some guides to the mill table. The hole in the blank dropped over a stud so that the blank could be clamped down to the table. The main guide was aligned in the Y direction using a clock gauge. A separate stop located the machined end of the blanks. I marked the first blank at 61mm from the machined end and cut the recess to this mark using my 25mm insert cutter and repeated this for the other four blanks. The depth was 4mm using the depth stop. To cut the 7-degree slope on the locating face I put the vice back on the mill (aligned in the X direction with the clock gauge) and clamped the blanks



Setting angle of blank in vice



Matching blanks with inserts fitted

with a 7-degree tilt using my digital angle gauge, **photo 11**. I used a 10mm slot drill and aligned it by eye to just take out the corner so that the insert would sit nicely.

Next, I decided to do the clamp screw holes while I still had all the sides of the blanks to locate on. I put the M10 tapping drill in the mill and positioned the vice so that the drill would just miss the dovetail at the bottom. I rigged up a stop as before and located a centre drill on a marked up blank. First, I drilled the tapping holes in each block in turn, then changed to the 10.5mm clearance drill and set the depth stop to go just over halfway and drilled all the clearance holes. The plan was then to counterbore for caphead screws and this is where it all went wrong. I have a stepped drill for M10 which produce a nice 16.5mm diameter counterbore but has a long clearance drill so I couldn't use it. I thought I could get a 16.5mm diameter slot drill as a counterbore but couldn't find one, and soon realised that if I had I wouldn't have liked the price! I did have a 16mm slot drill, so I decided to use that and reduce the screw head diameter as necessary. Having loaded the cutter and started the bore I found I had run out of quill travel – which is a pain on a round column machine. I adjusted the head and tried to line up on the partial bore – and was partially successful. Next time I will use M10 x 40 bolts and go straight on to tapping the M10 threads.

Each of the five different inserts was fastened to a blank with an M4 screw, **photo 12**. The sixth blank is a spare. The holders were finished off as described in the previous article. The inserts are of two grades suitable for steel and aluminium and have tip radii of 2,4 or 8. I painted the flat ends with binary code for the radii and colours for the grades ie. blue for steel and green for aluminium, **photo 13**. ■



Cunningly colour coded blanks

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Restoring a Vintage Dial Test Indicator



Mark Noel brings an old DTI back to life.

dial test indicator is an important accessory in the model engineer's workshop, being vital in tasks that include tramming the milling machine column, aligning jobs on the X-Y table and positioning parts in a 4-jaw chuck. They are available in plunger or finger designs, with digital or mechanical displays. Each has a specific role to play, although clockwork analogue types are often favoured since tiny movements are more easily seen via 'ticks' of the pointer.

I was once given a John Bull Type 2N imperial dial test indicator that originally formed part of the positioning stage in a 1960s electron microscope, **photo 1**. This instrument had been decommissioned aeons ago, dismantled and the parts long forgotten in a university store. The impressive control panel with its umpteen

The impressive control panel with its umpteen knobs, neon bulbs and matrix display is now the centrepiece in my workshop...



John Bull DTI testing after restoration.



Tools used to restore the DTI. Home-made hand puller at bottom.



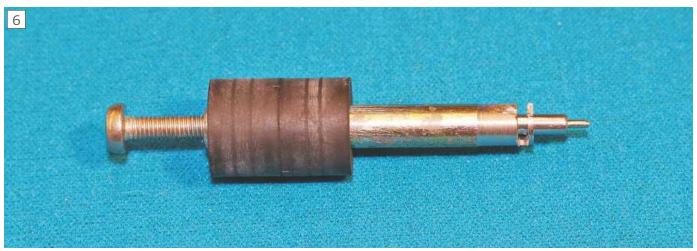
Rear of the DTI case, showing screws holding the cover plate and bezel.



The case opened, showing the clockwork mechanism.



Parts that make up the home-made hand puller.



Assembled hand puller.

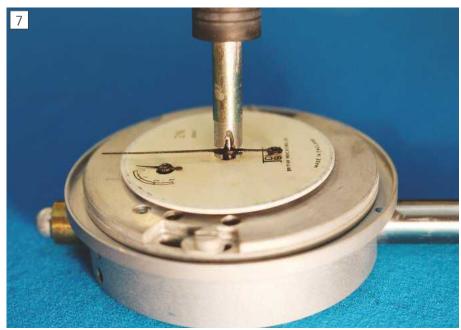
knobs, neon bulbs and matrix display is now the centrepiece in my workshop and impresses visitors more than the gadgets I make. During a recent deep excavation beneath my workshop bench I rediscovered this old DTI between a coal seam and a layer of dinosaur bones, and decided that now was the time to try to restore the instrument.

John Bull is frequently depicted in British folklore as a jolly rotund Englishman dressed in taut breeches and waistcoat, calling upon citizens to 'do their duty' for Queen and Empire. When not engaged in such noble activities he was putting his name to sweets, footwear, cutlery and other items where his dependable stature assured that these products were fit for the home and the colonies. This industrious chap even found time to create my quality dial test indicator, where his skill in watch making provides a resolution of 0.0001" or 2.5 microns, as inscribed on the dial. Nevertheless, the years spent languishing in the damp had taken their toll, with the hands partly rusted, the plunger sticking and flecks of mould on the face. The main pointer was touching the dial and this, together with scratches on the rear, suggested that someone had attempted a repair before.

Photograph 2 shows the tools that were

used in the restoration, most of which you will also have to hand, including instrument screwdrivers and a permanent marker pen. The only peculiarities are an interdental brush (from your supermarket or pharmacy and a pen oiler (from eBay or Amazon.

Also shown is a purpose made hand puller, more of which anon. The first job was to remove the four 4BA screws that held the back plate, then the six 10BA screws that secured the bezel and glass, **photo 3**. The gear train and main components could



Removing the DTI main pointer with the hand puller.

>

then be inspected, **photo 4**. Before the mechanism and case could be thoroughly cleaned I was still faced with the task of removing the hands - the main pointer and subsidiary pointer - before the dial could be taken off. Prodding, pulling and levering with fingernails and screwdrivers was to no avail and I was reluctant to apply excessive force owing to the risk of damaging the delicate bearings. A key problem was that the gap between the underside of the hands and the clock face is only about 0.5mm, making it difficult to insert a lever of sufficient strength without damaging the painted face. It became clear that the safest option was to apply a force between each hand and its supporting shaft (or 'pinion' in horological parlance. However, the difficulty was that neither pinion protruded through its respective hand, but was recessed by a fraction of a millimetre. Moreover, these pinions were only about 0.5mm in diameter and had become seized



Bending up the main hand to restore its shape and prevent scuffing.



Restored John Bull DTI testing runout on a milling machine spindle.

to the hands by corrosion. Special watch hand pullers are available from a number of horological suppliers and on eBay for a bargain. However, I was not convinced that the chunky fingers of the budget versions would fit beneath the DTI's hands, nor was I prepared to spend a significant sum on

Prodding, pulling and levering with fingernails and screwdrivers was to no avail, and I was reluctant to apply excessive force...

a pukka model since this might only be a one-off restoration.

Among the dinosaur bones were several parts from a Jurassic printer (they were clever you know!), including rollers, 6mm chromed shafts and some 3mm diameter chromed spindles with reduced ends, **photo 5**. A 40mm length of the 6mm shaft was drilled lengthways and tapped M3, then a narrow slot and groove ground at the end using a Dremel tool to form a pair of thin fingers that would fit just beneath the DTI's hands. Two of the rubber rollers were pressed onto the shaft to form a handle, then part of the thinner printer spindle passed down the shaft, with an M3 screw to propel it downwards. The completed hand puller is shown in **photo 6** and in action in **photo 7**; after the fingers are slipped beneath the DTI's hand, the screw is used to drive the spindle down against the pinion, releasing the hand. The operation was still a struggle and only



Scruffy old Baty DTI as purchased.

...nor was I prepared to spend a significant sum on a pukka model since this might only be a oneoff restoration.

successful after penetrating oil had been left to do its work for 24 hours.

Now the hands were free they were burnished with wire wool, repainted with permanent marker and given a thin coat of silicone oil to prevent further corrosion. The DTI face was cleaned gently with soapy water and put aside to dry, while the clockwork mechanism was thoroughly cleaned in paraffin aided by the various brushes shown in photo 2. Once the paraffin had completely evaporated all accessible pinions and sliding parts were sparingly lubricated with the pen oiler - a clever tool that will doubtless find other uses in the workshop wherever pinpoint application is required. The DTI rear cover and front face were then re-attached, and the hands pressed back on in zero positions with the plunger at the end stop. At this point it was noticed that the main hand was scuffing the dial but this was rectified by carefully bending the (spring steel upwards



Levering out the circlip on the Baty DTI to release the front bezel.

until the shape was restored and the hand was clear, **photo 8**. Scratches on the (plastic watch glass were removed using Brasso polish and the front reattached, finally restoring this vintage instrument back to working condition, **photo 9**.

Encouraged by this success, I decided to tackle another dial test indicator, this one made by Baty and purchased from eBay for a few pounds, **photo 10**. At first it seemed that the case had been swaged together preventing access to the seized movement.

However, closer inspection revealed that the bezel was secured by a wire circlip hidden in a deep groove filled with debris, **photo 11**. Removing this gunge and winkling out the clip has exposed the workings and now another restoration is underway!

Resources

Precision horological watch hand pullers: www.ofrei.com/page1678.html

Next Issue

Coming up in issue 264

On Sale 26th January 2018

Content may be subject to change

Look out for the February issue, 264, of Model Engineers' Workshop, for even more fascinating tales from the workshop:



By popular demand - **Jock Miller's** Taper Turning Attachment.



Bunker corners - **John Smith** shares his technique for complex 3D bends.



A heavy duty clamp-drill from **Stewart Hart.**

On the NEWS from the World of Hobby Engineering

Parting is such sweet sorrow! The end of an era, and the beginning of an exciting new one!



Back in 1995, Greenwood Tools invited the model engineering fraternity to "Wake up from your worst nightmare" with the very successful introduction of the innovative KIT-Q-CUT parting tool (based on the Sandvik Q-Cut system). Since then, the tool has received many accolades from model engineers and the model engineering press. People said it "changed their lives", and was "the best thing since sliced bread".

2018 brings the introduction of the replacement for KIT-Q-CUT. The groundbreaking new **KIT-QD** parting tool (based on the Sandvik QD system) has a better insert location, stronger body and improved insert design. Existing users of the original KIT-Q-CUT have tested the new KIT-QD with very positive results. John Roberts said "Changing the insert takes seconds using the new design application tool. The ease with which this tool parts off a variety of

materials is staggering. Highly recommended". Stuart Hardy tested the new tool on EN1A, EN8, EN25T, cast iron, 316 and 314 stainless steel, bronze, brass and aluminium bronze. He said "Generally speaking the KIT-QD is better than the KIT-Q-CUT. It cuts better, and inserting the insert is much better. A good step forward – it gets a 'thumbs up' from me"

The KIT-QD parting tool will be unveiled at the London Model Engineering Exhibition at Alexandra Palace from 19-21 January 2018, and will be your new 'part-ner' through thick and thin!

Users are reassured that inserts for the original KIT-Q-CUT will still be available for the immediate future.

Once launched in January you will find more details and order KIT-QD at www.greenwood-tools.co.uk/ or call them on 01527 877576.

REMAP to be at Ally Pally

Remap, the charity of volunteers that custom make bespoke engineered products for disabled people to help provide independence will be at the 2018 London Model Engineering Exhibition.

Remap started in 1964 when a design engineer custom-made some equipment for his disabled sister to make life a little easier for her. He soon realised there was a demand for such products, the charity boomed and now comprises of 70 local groups throughout the UK and over 900 volunteers!

Bespoke items are designed, created and made solely for the

individual such as an independent eating tool for a double amputee, an adapted saddle so that a little girl can still enjoy horse riding, a wheel chair that is compatible with a baby carrier so a mum can take her baby for a walk.

At this year's Exhibition Remap will be displaying some of their unique engineered designs.

The Exhibition is held at Alexandra Palace, London for Friday 19 to Sunday 21 January. For more information and tickets visit www. londonmodelengineering.co.uk.



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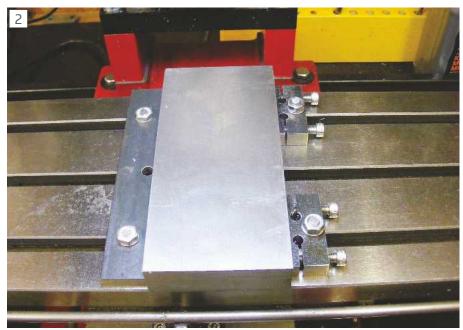
Low profile clamps for the mill table

This month Mike Cox describes an unusual but effective workholding device.

here are many kinds of clamps that can be used on the mill table to restrain the work piece during milling. The commonest is of course the milling vice. Vices are always restricted in size and not generally suitable for large work pieces. In this case the work piece can be clamped directly to the mill table. Most clamps clamp the work between the upper surface of the work and the mill table and such clamps must of necessity protrude above the upper surface. This is fine for making a slot because it is usually possible to arrange the clamps in position that are not in the way of the milling cutter. However, if, for example, it is required to fly cut the whole of the top surface then the clamps will be in the way.



The basic low profile clamp.



The clamp in use securing a large block of steel.

One way around this is to fly cut part of the surface with the clamps on another part and then move the clamps to the fly cut part and finish of the rest of the surface. This is a not always easy and there is scope for errors to occur. The way round this is to use low profile clamps to clamp the work by the edges. In this way the clamps to not interfere with a clear run of the cutter over the whole of the surface.

There are several designs of low profile clamp that have been published and several, by Harold Hall, have appeared in the pages of this magazine over the years. In this article I will introduce another style of low profile clamp. The advantage of this style of clamp is that it is very easy to make. They are attached to the mill table using a normal tee bolt or tee nut that puts little strain on the tee slots.

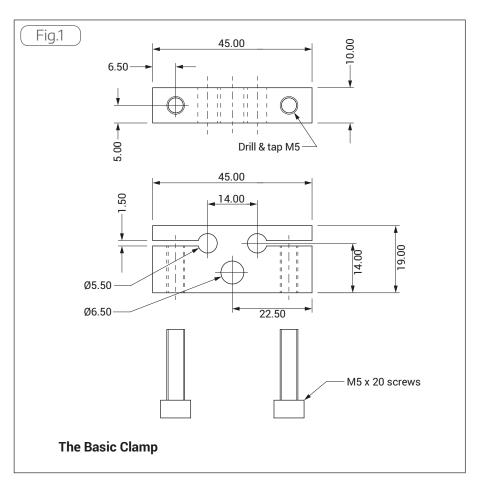
The basic design.

I made my first set of low profile clamps many years ago and they have been used frequently.

These clamps only work for clamping straight edges, but they are very simple to make and use.

I will illustrate the basic design by describing the construction of a clamp 10 mm thick, as shown in **photo 1**. The dimensions are given in **fig. 1**. The clamp was made from a piece of 10 mm thick steel that was cut out and milled on the edges to make a block 10 x 19 x 45 mm. The hole positions were marked out and drilled on the bench drill. The two slots were then cut using a 1.5 mm slitting saw in the mill. The final step was to tap the two holes for the M5 socket head screws. The tapping was carried out using a taper tap, followed by a second tap and a plug tap. The final step is to screw in the two M5 screws. If the screws will not screw in sufficiently because the hole is not threaded all the way through, then the end of the screw can be turned down.

Photograph 2 shows the clamps in use holding a large piece of steel. One edge of the work is supported against a fixed stop bolted firmly to the mill table. On the other side the low-profile clamps are butted up to the work and fixed firmly in position. The work is then clamped by tightening the socket head screws.



Some variations.

The basic clamp described above works very well but it does have some

Firstly, the tee bolt and nut stick up above the top surface of the clamp. This does not usually limit machining the top surface of an object, but it is a hazard because it is relatively easy to run the cutter into it whilst moving the table about. This can result in damaged cutters. For 10 mm thick clamps it is possible to counter bore the hole for the bolt that fixes the clamp to the mill table. This



A clamp with a recessed securing screw.

Fig.2 45.00 iii 30.00 **←**14.00 Drill M3 -10.00.50 38.00 6.00 Drill & tap M4 Ø2.5mm push rods 8 M4 x 6mm grub screws The Improved Clamp

is wider than the basic version and it has the slot rather than a hole for the fixing bolt. This enables it to be used parallel to the mill table tee slots, **photo 5**. Also note that because of the thinness of the clamp the clamping screws have been changed to M4 socket head grub screws.

The design of the new clamp is slightly modified, and the grub screws do not operate directly on the clamping pads but via two push rods, see **fig. 2** and **photo 6**.

Construction is straightforward and similar to the operations outlined above for the basic clamp. The only tricky operation is the drilling of the two deep holes for the push rods. This is best done in the mill with the spindle running at high speed, avoiding heavy pressure, using plenty of lubricant and pulling the drill out frequently to clear the flutes of the drill.

Conclusion.

These clamps only work for clamping straight edges, but they are very simple to make and use. The new style 6 mm clamp works well and has many advantages over the original basic clamp. It can be easily scaled up to make thicker clamps.

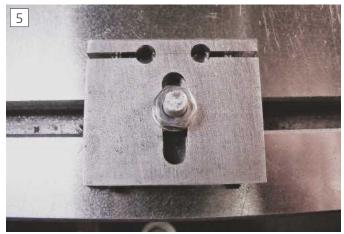
enables the use of a socket head screw and a tee nut to secure the clamp and then there is nothing protruding above the top surface of the clamp, **photo 3**.

Another problem with the basic clamp is that it can only be used at right angle to the tee slots on the mill table. This is because it is not wide enough to bridge the tee slot if placed parallel to the tee slot. The easy solution to this is to make the clamp wider. By making it wider it is also possible to use a slot rather than hole for the fixing screw. This allows greater freedom when positioning the clamp.

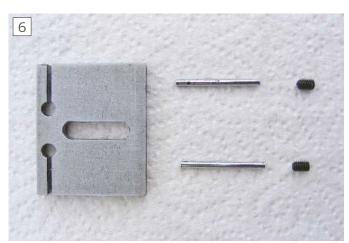
A further limitation of the basic clamp is that it is too thick for some jobs. I required a clamp that was only 6 mm thick for a specific job and a new clamp was designed to incorporate all the features discussed above, **photo 4**. This version



The 6 mm clamp.



The wider clamp with the slot can be used parallel with the tee slots.



The 6 mm clamp uses grub screws and push rods

January 2018

Milling for beginners



PART 2 - SPINDLE TAPERS AND TAPER TOOLING



This new series will build into a complete guide to using a milling machine. This month Jason Ballamy starts right at the beginning by taking you on a tour of the new SX2.7 bench top Mill

Spindle Tapers

On the vast majority of milling machines different tooling is attached using a hollow taper inside the machine's spindle. Rarer exceptions include some very small mills, such as the X0, which use a male taper in combination with a securing screw to hold small chucks. This month I will look at the common types of spindle taper and the tooling used with them.

Morse taper

Up until fairly recently this was the type of taper you were most likely to find on the smaller bench top milling machines, usually in size 2 or 3. Being quite a shallow taper (around 3 degrees included angle) it is what is known as a self-locking taper so will stay in the spindle under vertical loads but side loads and intermittent cuts could loosen the taper. For this reason, milling tooling should be held into the taper socket using a drawbar, this is essentially a long bolt that bears against the top of the spindle and threads into the end of the tooling's taper. Depending on the age of the tooling



Taper tooling and selection of drawbars



R8 and Morse Taper collets

and also if it is metric or imperial you will find that the thread can vary between M12 and 3/8 Whitworth so you may need two drawbars, photo 10.

The taper tooling can be removed in one of two ways; if the machine is equipped with a self ejecting drawbar simply by undoing the bar which after a turn or two will apply downward force which will break the grip of the taper. If the machine is not so equipped the quill should be locked and the drawbar undone about 1 full turn, then with a copper faced hammer give a firm tap to the head of the drawbar and that should loosen the taper without excessive force. Try to avoid putting a cold tool into a warm machine as the heat will transfer to the tooling which will expand slightly and become tighter in the socket and will require a lot more force to eject.

R8 Taper

This has been used on larger turret mills, such as Bridgeports, for a number of years



End Mill Holders and Weldon shank cutter



ER Collet chucks and bearing nut

and is becoming a lot more common on the mid-sized hobby machines due to the fact it is a lot easier to remove the tooling from the spindle as the steeper taper (about 16.5 degrees included angle) is not self locking so just a gentle tap on the drawbar or less effort is needed on a self extraction bar to break the taper's grip. The R8 spec also includes a keyway which engages on a small stud inside the spindle that makes tightening easier as the tooling does not rotate as the drawbar is tightened, this is of most use if using R8 collets.

INT/ISO/DIN Tapers

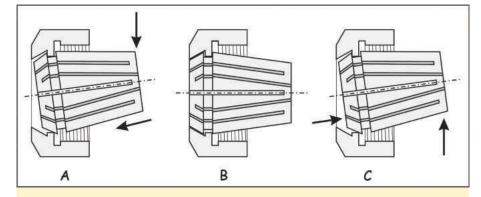
These are more the domain of larger commercial machines but the smaller 30 size does crop up on one or two bench top sized machines. They have a notched flange which will take the drive as well as a taper and short parallel section for alignment. There are slight variations between the various types as to the notches, parallel section and method of retention so make sure you know the details of your particular machine as it is quite easy to pick up a bargain tool at a show and then find it is not quite right when you get it back to the workshop.

Interchangeability with the Lathe As lathes also have Morse tapers in the head and tail stocks it is possible to use the same tooling between both machines, though I would not treat that as a major issue if choosing between a MT or R8 machine as you will find in time you acquire separate tooling for each machine or an adaptor can be employed for occasional use.

Tool Holding

Direct Fit/ Finger Collets

The simplest way to hold cutting tools is by using a collet that fits directly inside the mill's spindle which in most cases will be either Morse taper (MT) or R8. These are collets shaped to fit the relevant taper with several saw slots at the wider end and threaded at the other, so they can be drawn into the taper which will cause the wide end to close down onto the cutter. They only



Correct fitting and removal of ER collets

Inspecting the inside of an ER collet nut reveals an internal flange that has been machined eccentric to the main axis of the nut. This is not a machining error but is designed that way to lock onto the groove of the collet and aid its release from the chuck body.

For this feature to work properly, the collet must be mounted in the nut first before fitting the assembly into the chuck body. To mount the collet in the nut, insert it at an angle, turn slightly and push it into the nut until it clicks into place on the eccentric flange. The cutter may now be fitted and the assembly tightened hard into the chuck body.

To remove the cutter, slacken and undo the nut until resistance is felt. Then, using a collet wrench, further undo the nut until the collet is felt to release from the chuck body. Removal of the collet from the nut is the reverse of the mounting procedure.

hold items within a very small deviation of the nominal size so cannot be used to hold drills or imperial cutters in metric collets, so you will need a collet for each shank size you wish to hold. Their main advantage is the very minimal projection from the end of the spindle which can be used to advantage when room between table and head becomes a bit restricted and as the cutter is closer to the spindle bearings they give a very rigid holding method. There are a number of other collet systems often specific to a single manufacturer of machines or tooling which are too numerous to cover in this beginners' series, photo 11.

End Mill Holders

Also known as Weldon holders after the company that first put a flat on the shank of a cutter, these consist of a cylindrical

head on the end of a MT or R8 shank that is bored to take the common shank cutter diameters and has a threaded hole at right angles with a grub screw that bears against the flat on the cutter's shank. Like the direct collets these are one size only and should also only be used with cutters that have a flat on the shank so not ideal for screwed or plain shank ones though if pushed you could grind your own flat to get out of trouble. They do have the advantage of a smaller head diameter than some of the collet chucks which will allow access into smaller spaces and make seeing small cutters, that are sometimes obscured by a large collet nut or the machine's spindle, easier, photo 12.

Collet Chucks

The traditional collet chuck of choice was a "Clarkson Autolock" which used a collet

h used a collet



Typical ER starter set plus bearing nut

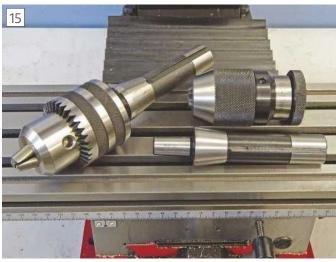
that was threaded at the upper end and when used with threaded shank cutters gave a very positive grip of the cutter which should it slip in the collet was pulled up tighter rather than pulled out of the chuck. As with the other types above these are one collet per shank size and you are limited to using threaded shank cutters.

The more versatile ER type collet chuck has seen a big increase in popularity both in industry and hobby use in the last 10 years or so. For our use it's biggest advantage is the fact that each collet will cover a range of sizes, mostly from nominal size down to 1mm less, or in the very small sizes from nominal down to 0.5mm less, which means they can be used for drills in incremental or fractional sizes and also for work holding with the right fixtures which we will look at later. The ER collets are slotted from both ends which allows full contact along the length of the tool giving a better grip than other collets, photo 13.

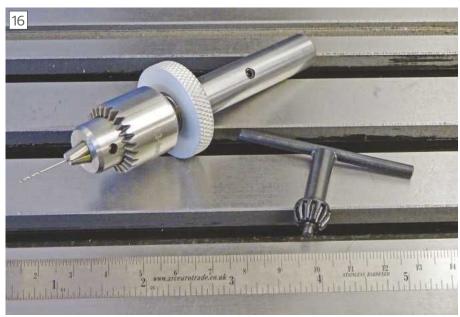
ER collet chucks come in a range of sizes from the very small ER11 to large ER50 sizes, the number indicates the diameter at the largest end of the main rear taper. As a general guide an ER 20 would be about right on a X1 size machine, ER 25 on a X2 and the ER 32 on a SX2.7 and SX3 mill. Purchasing the chuck with a basic range of six collets generally gives a saving over buying individually so it is a good way to start off and then additional collets can be added as and when required or when finances allow. I would also suggest that a ball bearing collet nut to suit the size holder is obtained at the same time as this makes tightening the nut a lot easier as less of your effort goes into overcoming friction between nut and collet, photo 14.

Drill Chucks

Surprisingly most new small mills are supplied with a drill chuck rather than a milling chuck, maybe it is due to the fact that a mill makes for a very accurate drilling machine when the X and Y axis dials or a DRO are used to position the holes. The supplied chucks are usually of the keyed variety and you may soon find that you



Drill chucks and drill chuck arbor



Micro Drill adaptor plus chuck

want to add a more convenient keyless one to your tooling collection. My personal preference is to have a slightly smaller 0.2-10mm keyless chuck as most of the time that suits the size of drills I use and the larger supplied chuck can be put to use for anything over that size.

Apart from some of the very expensive commercial chucks which have integral shanks you will need a drawbar type drill chuck arbor to mount your new chuck on, these have a suitable taper to fit your spindle on one end and a smaller taper to fit into the chuck body on the other. Your chosen chuck should specify the mounting taper either in the paperwork and/or on the actual chuck and is going to be a J or B followed by a number which signify the type of taper and its size. To mount the chuck on the arbor clean both mating surfaces then place the chuck onto the arbor's taper and with the chuck facing upwards bring the arbor down firmly onto your bench which will seat the taper. The chuck is generally left on its arbor for the rest of its life, but should the need arise

to separate the two then a pair of removal wedges should be used. These reduce the risk of bending or damage as they apply an even pressure behind the chuck, **photo 15**.

When using very small drills in the region of 1.0mm or less there is not a lot of feel back through the quill lever to indicate how the drill is progressing and breakages can result from applying too much pressure. One way to avoid this is to use a more sensitive drilling attachment or a micro drill adaptor which still uses the mill's spindle to rotate the drill but the up and down movement is achieved with finger and thumb around a knurled ring giving a lot more feedback to how the drill is cutting, photo 16.

Boring Heads

These consist of a two-part head where the halves are joined by a dovetail and a fine adjustment screw allows one half to move relative to the other. Therefore, by placing a cutting tool in the lower moving half of the head it is possible to alter the diameter of the circle the cutting tip is swinging at





Stub milling Arbor and Flycutter

Boring head set

which allows any size hole to be cut within the range of the head and its cutters. These heads are usually sold in a set complete with some cutters which can vary from HSS to Brazed carbide tipped through to holders that in turn take smaller HSS tool bits. Indexable insert holders are also available, **photo 17**.

As well as forming holes boring heads can also be used to machine curved surfaces such as the underside of a chimney saddle or shape the end of a tube so it will join another neatly. They will also "turn" the outside of a round item with a suitably shaped tool, don't be tempted to use one of the supplied tools for this by running the machine in reverse, as most of the small heads are only screwed onto their arbors and could come undone.

Boring and Facing Heads

These are basically a larger version of a boring head but with the added feature of being able to advance or retract the tool as

the head rotates which allows for machining large items that may not fit into a lathe.

Stub Milling Arbors

These are used to hold such things as slitting saws and gear cutters. The tapered or straight mounting shank has a parallel arbor sized to suit common cutter bores, a series a spacer rings allow for different thicknesses of cutter to be accommodated as well as their position along the length of the arbor to be adjusted. It is also possible to gang up cutters with suitable spacers between which is useful for things like cutting cooling fins. The tooling and spacers are retained on the arbor by either a nut or a screw at the end, the screwed type can be useful when using slitting saws to cut work standing vertically out of the milling vice as it allows the saw to get closer to the vice jaws which in turn means less unsupported work sticking out of the vice. Much like the boring heads don't be tempted to run these arbors in reverse

as it may loosen the retaining nut/screw, **photo 18**.

Fly Cutters

It's a bit debatable – is this is a cutting tool or tool holder? As they hold a HSS or insert tool I will include them here. The fly cutter is a very useful and economic tool for metal removal particularly when working on large surfaces and is capable of giving a very fine finish. The large head on the end of the shank is cut across at an angle and slotted to take the square shank of a tool, the larger ones having an offset head to counteract any imbalance. An HSS toolbit can quickly be touched up with a diamond stone to or reground with a basic bench grinder to give a sharp cutting edge many times over so keeping tooling costs down.

Shell Mill Arbors

Probably not used that much on the smaller machines but as the name suggests they are used to hold large diameter shell mills and will also take the more modern indexable face milling cutters. The load is transferred to the cutter by two lugs on opposite sides of the holder and a central screw keeps it in place, **photo 19**.

Do keep all spindle sockets and tooling tapers clean as any swarf will throw things out and can get stuck to one of the surfaces and can go unseen particularly if stuck in the socket. Also avoid having your tooling rolling about on a cluttered bench, small dents and bruises will raise a burr that will stop the taper engaging accurately. Either make or buy a rack with a series of holes in it or use a draw with suitable dividers to keep each item in.

For a full list and links to the items featured which are available from Arc Euro Trade, http://www.arceurotrade.co.uk, who also sell the X series of mills see the accompanying thread on Model Engineer Forum http://www.model-engineer.co.uk/forums/postings.asp?th=131318



Shell mill and arbor

Quadrilla

Michael Belfer 'improves his relationship with drills'

uadrilla has helped me resolve the love-hate relationship I have had with drills - both the bits and the devices, for around 60 years. That was when my grandfather gave me a threefold present. A small hand-drill, a flat blade screw driver, and my first beginner's Meccano set. Together these ignited my life-long passion for engineering designing and making things, anyway.

I love drilling because it always seems the easiest of the machining tasks and gets the quickest results with the lowest chance of messing the work up. What I equally hate, on the other hand, is the ease with which those who can free-hand grind the bits when their edges dull, somehow magically produce equal angled sides, of equal length. Try as I could, I could never achieve this, and trying multiple different drill grinding tools and attachments has improved my results, but not brilliantly so.

So my approach was to accumulate lots of bits so I could usually lay hands on one. Initially, I had only a small round stand for 1/16" to 1/4" bits. This wasn't too demanding on storage, but move on a few decades and we are talking about including Numbers 1-60, fractions to 1/2", letters, and eventually, metric from 1mm to 13mm in 0.5



Completed Quadrilla mounted on my drill Press



Storage for bulk drill bits, hex keys, and other items

mm steps about 125 sizes, if my arithmetic is correct, (Although I could never fathom why sizes A and E, having exact fractional equivalents, were ever included).

By and large, my sloppy habit of drill and drop – on the bench, the drill press table, or into a box "to be sorted and/ or ground eventually" drove me to the arrangement seen in photo 1, together with 4 drill indexes which together take up a sizeable amount of bench surface, as well as inviting themselves to be knocked over and requiring the picking up, sorting, and

replacing of their contents - not a trivial task with the smaller sizes.

Enter Quadrilla

Quite a few years ago I partially improved this situation with a rotating mount for the fractionals drill index, mounted off the side of the drill press at eye level (my drill press is bench mounted) and tilted forward to allow reading the sizes off the drill index and much more often returning the bit to its rightful place. (It was positioned and oriented in much the same place as

my current solution, the Quadrilla, seen installed and mostly populated in **photo 2**). This original rotating Fractions drill index still left the numbers, letters, and metric drill indexes occupying bench space with irksome access, however.

I found a light but rigid (due to pressed-down edging) piece of enamelled steel about 11" square by the roadside (placed there for recycling, no doubt) with rounded corners, seen in **Photos 3, 4** and **5**. It gave me the idea of checking my four drill indexes for easy placement around what I now thought of as a base plate. The Quadrilla concept was born – centres and outlines were marked on the base plate, together with measurements of the drill index centre holes, height above base and diameter, **photo 5**.

Clamping column

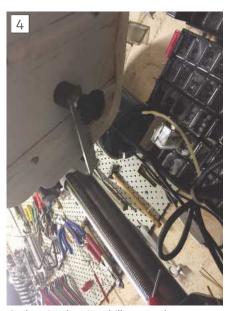
Photograph 7 shows the clamping column, topped by one of the four knobs liberated from roadside furniture a long time earlier, "just in case". This type has a hex socket moulded in, that conveniently captures the head of a hex 5/16" Whitworth (in my case) bolt that extends down through the outer tubing of the clamping column to screw into a cylinder nut drilled and tapped through 5/16 Whitworth. The disassembled parts of the clamping column can be seen in **photo 6**, noting that the wooden plug is just to keep all the parts radially aligned, and the shoulder on the nut is a free running fit in the drill index centre hole, but a little less in height than the thickness of the drill index plate surrounding its centre hole. **Photograph 8** shows trial assembly of two drill indexes onto the base plate, to check position, clearance at bottom, free turning when unclamped, and being held firmly when clamped by just a quarter turn of the knob. This had to be done for each clamping column as finished, because Murphy dictates that all drill indexes will have different dimensions,



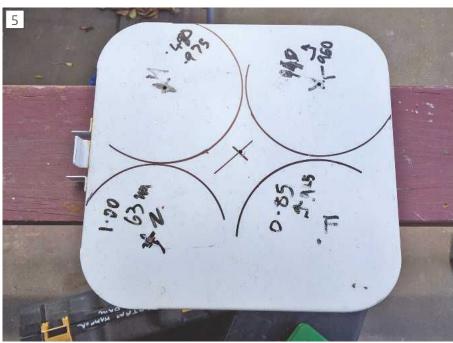
Components of a clamping column– Clamping Column



Underneath view of Quadrilla Baseplate



And again, showing drill press column



Baseplate marked for drill index positions and dimensions

of course. The cylinder nuts are at this stage already fastened to the base plate by short 5/16 Whitworth bolts, the heads of which are visible in photo 3, the underside of the baseplate. A washer trimmed to the outside diameter of the clamping column tube pushes down on the tube as the knob is turned, so that the drill index is clamped between the tube bottom and the baseplate.

The column height obviously determines how far down amongst the drills the hand has to reach for the clamp/unclamp action and I chose mine also to allow the use of standard length bolts readily to hand, allowing about 3 turns of engagement into the cylinder nut. The wooden plugs were bits of old broom handle.

There is no precision required in any of the dimensions other than the shoulder of the cylinder nut which must not be higher than drill index material thickness at its centre or the drill index will just spin and not be able to be clamped.

Mounting on the drill Press

A simple bent strap of steel is held to the column by some standard plumbing fittings, and the degree of baseplate tilt can be adjusted by a wing nut on the clamp. This is just obscured by the drill spindle in **photo 9**, from which it can possibly be guessed that the drill press feed handle will interfere with the drill tops while turning – if I find this too irritating I will swing the whole fixture around to the left of the drill press column from its current position on the right, no rework other than loosening and tightening should be required.

The underside baseplate views, photos 3 and 4, show the slightly different knob (same source) used for baseplate clamp/

>

January 2018

Ouadrilla is a tool that has given me much satisfaction in being a useful addition to my workshop...

unclamp. Besides being larger it has a moulded-in stud of I think 1/2W rather than the captive bolt head arrangement, this is more suitable for something that spends all its life upside-down. It clamps the supporting strap against a blob of metal made into a big brother of the clamping column cylinder nuts, tapped right through to suit this knob's thread, of course. From on top, the head of the short bolt attaching it to the baseplate is seen in **photo 10**. To prevent the blob working loose over time, aided by vibration, a 1/4" Whitworth bolt was fixed as a key through to the blob, seen with its hex abutting the larger bolt head hex as an additional but probably unnecessary action.

The Name

Obviously, Quadrilla came about as a



All in place



Trial assembly of one drill index and CC

method to manage four drill indexes, and its name describes this. But the arrangement that resulted, with the four in orbit at the corners of a square and each rotating in its corner, reminded me very much of four couples dancing, each in its own circle, in a corner of the square they slowly revolved around. This dance, seen often in period dramas from the 19th and earlier centuries,

> is called a Quadrille, and so I felt justified in borrowing the term in naming Ouadrilla.



It may seem that in use, it would be convenient to adjust each drill index clamping knob to a level of friction that allows the drill index to just be turned and leave it like that. Two things rule this out. One is that various friction forces tend to tighten and untighten the knob at inconvenient times if left only partially. The unbalanced weights of the drills around the index, together with vibration if any, will move around (dare I say dance?) so as to deposit the largest sizes facing towards the bottom of the baseplate tilt. This is not always convenient, but don't ask me how I know!

The keen sighted may notice that some of the metric drills have been deposited upside down in their index. This is because my metric drills above 10mm have reduced shank diameters, and a set of plastic plugs to match these diameters to



lostling for position



Another view of Quadrilla as currently installed

the index holes lies awaiting attention in my bucket of Round Tuits. Also, the trial assembly staged in photo 7 was mistakenly taken with the numbers clamping column on the Letters drill index, obviously the numbers clamping column is the one with shortest required column height. Oops.

Conclusion

Quadrilla is a tool that has given me much satisfaction in being a useful addition to my workshop that also helps with storage and space, those perennial foes. It has functioned exactly as first envisaged, and even better, was made almost entirely from recycled and/or liberated materials. I hope I may inspire any other home machinists wanting to tame their drill storage and access problems to do something similar. It was simple to construct, which took probably less time than writing it up. ■

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Mounting Items on a Faceplate

Andy Johnston makes an awkward task easy for you.



View of complete gadget mounted in vice



Two lengths of angle iron welded together



Centring an item using a dial gauge



Centring to a centre pop mark with a scribing block

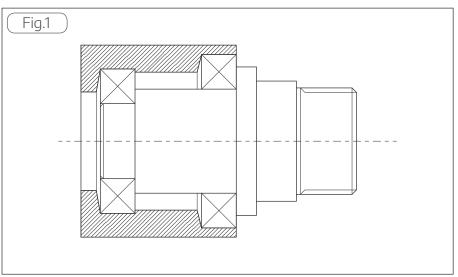
t is always awkward trying to mount items on a faceplate, we don't have enough hands, and is especially difficult when trying to centralise an item be it cylindrical, a bore or to a centre punch mark, **photo 1**.

The base for my gadget was sourced from some lengths of angle iron from an old iron-framed bedstead welded back-to-back with a revolving shaft mounted in a housing which is bolted to the base, **photo 2**. I used four small socket head bolts screwed into the bottom of the housing.

The shaft has a nosepiece turned to suit your faceplate, mine is for a Myford ML7R. There are two ball bearings mounted on the shaft which are a close fit in the housing. There is a hole drilled right through the housing and the shaft between the ball bearings for a locking shaft.



Setting up for balancing the faceplate



Sketch of housing and spindle (Uncropped)



Weight added

A workpiece is clamped in place and can be perfectly centred using a dial gauge. In this case it is a previously machined bore which was being centralised, **photo 3**. It could be an item which required centring on a centre pop and a scribing block can be used for this, **photo 4**.

Static balancing anything on a faceplate is now very easily done by turning the gadget upright, **photo 5**. Suitable weights can be added to balance the mass or at least reduce the out of balance forces, in this example the small weight is to the fore in **photo 6**.

Figure 1 is only what I can remember of the internals of the shaft and housing as I made it up as I went along about 30 years ago. The only thing holding the assembly together is Loctite Bearing Assembly Fluid on the top outer bearing raceway.

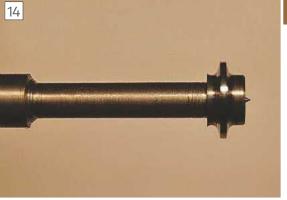
Odd items in a four-jaw chuck could also be set up with this gadget, the final accuracy being carried out once transferred to the lathe. I've used it extensively since it was made and wouldn't be without it.

Simple Cutters for Clock Pinions and Wheels



Ted Knight - Part 2

ring back the cross slide by distance Y, the pinion tooth height. This is the position for the final cut when the form tool feed is inwards. Then, without moving the top slide, use the cross slide for the feed and saddle movement for the cut, **photo 13**. Polish the flanks to take out any tool marks and break the sharp corners. Then reduce the shank diameter to about 5 mm, **photo 14**. I reduce the shank diameter because less heat is needed for the hardening process. This is also a good time to make a hardwood copy for polishing the pinions.



Reduce shank diameter

Next, we cut the teeth. I use a slitting saw in the mill to cut the teeth, **photo** 15. How many teeth you have is decided by the space needed between them for sharpening. I find that six or eight teeth give the best space. With the piece set up in the mill set the bottom surface of the saw blade on centre height using the previously turned centre cone as a guide, photo 16. To make the rake angle, lower the saw by a small amount. If you lower it by ten percent of the tooth height, Y in table 3, the angle will be close to six degrees. Take the first cut to form the pinion cutting surface then index around for the remaining teeth, **photo 17**. Lower the saw to cut the backs of the teeth. A straight edge resting on the saw will help guide for the best position, **photo** 18. Then take out the waste between, photo 19. Clean up, and de-burr ready for



Cut for final tooth height

backing off, hardening and final sharpening, photo 20. To cut the back-off I take a file and remove the sides and top at the back of each tooth. Leave a very small land at the back and sides of each tooth. Sharpening after, hardening, is to cut away with a diamond flat or oilstone at the cutting surface until the small land is cleared.

Making the wheel cutter.

Making the wheel cutter is very similar so I will only mention the differences.

The radius of the wheel teeth is different from that for the pinions, so a new form tool is needed, table 4. Set this form tool at an angle from the new cutter blank and cut the left flank, taking it into the shank making a semi-circle, as before Next, cut another semi-circle, at exactly the same depth, to the left of the first, photo 21. This will be the datum for the



Cut the teeth

Table 1 – Module Numbers and Drill Sizes

Module	Drill Size	Diameter
0.20	0.3	0.42
0.25	0.4	0.53
0.30	0.5	0.63
0.35	0.6	0.74
0.40	0.7	0.84
0.45	0.7	0.95
0.50	0.9	1.05
0.55	1.0	1.16
0.60	1.1	1.26
0.65	1.1	1.37
0.70	1.2	1.47
0.75	1.2	1.58
0.80	1.2	1.68
0.85	1.3	1.79
0.90	1.4	1.89
0.95	1.5	2.00
1.00	1.6	2.10

Table 2 - Cu	tter B	3lank	Sizes
--------------	--------	-------	-------

Module	Α	В
0.20	0.9	0.6
0.25	1.2	0.8
0.30	1.5	1.0
0.35	1.7	1.1
0.40	2.0	1.3
0.45	2.2	1.4
0.50	2.4	1.6
0.55	2.7	1.8
0.60	2.9	1.9
0.65	3.2	2.1
0.70	3.4	2.2
0.75	3.7	2.4
0.80	3.9	2.6
0.85	4.1	2.7
0.90	4.4	2.9
0.95	4.6	3.0
1.00	4.9	3.2

form tool when it is re-set for the right flank and must be an exact distance from the first. Set the form tool angled for the right flank into the new datum, **photo 22**. Do not move the top slide. Note the cross-slide position, this will be where the right hand cut finishes. Move the saddle to the right, first by the distance from the datum to the left flank and then by the distance P in table 4 to bring the tool to the final position for cutting the right flank. With the



Saw blade on centre height



The first cut



The waste removed.

right flank completed, **photo 23**, withdraw the tool from the final position by distance Q, the tooth height, in table 4. This is the

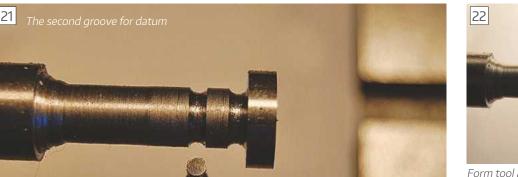


Straight edge guide.



Start backing off

position of the form tool to bring the wheel cutter to the correct tooth height. For the rest of this wheel cutter, follow on in the





Form tool angled for the right flank

Table 3 - Module slide angle	- Pinion details Number of Leaves	х	Υ	Тор
0.20	6	0.77	0.41	70
0.20	7	0.79	0.45	73
0.20	8	0.80	0.48	75 75
0.20	10	0.81	0.52	78
0.25	6	0.97	0.51	70
0.25	7	0.99	0.56	73
0.25	8	1.00	0.60	75 75
0.25	10	1.02	0.65	78
0.30	6	1.16	0.62	70
0.30	7	1.18	0.67	73
0.30	8	1.20	0.71	75
0.30	10	1.22	0.78	78
0.35	6	1.35	0.72	70
0.35	7	1.38	0.78	73
0.35	8	1.40	0.83	75
0.35	10	1.43	0.91	78
0.40	6	1.55	0.82	70
0.40	7	1.58	0.89	73
0.40	8	1.60	0.95	75
0.40	10	1.63	1.04	78
0.45	6	1.74	0.92	70
0.45	7	1.78	1.00	73
0.45	8	1.80	1.07	75
0.45	10	1.83	1.17	78
0.50	6	1.93	1.03	70
0.50	7	1.97	1.11	73
0.50	8	2.00	1.19	75
0.50	10	2.04	1.30	78
0.55	6	2.12	1.13	70
0.55	7	2.17	1.23	73
0.55	8	2.20	1.31	75 70
0.55	10 6	2.24 2.32	1.43 1.23	78 70
0.60 0.60	7	2.32	1.23	70
0.60	8	2.40	1.54	75 75
0.60	10	2.44	1.56	73 78
0.65	6	2.51	1.34	70
0.65	7	2.57	1.45	73
0.65	8	2.60	1.55	75
0.65	10	2.65	1.69	78
0.70	6	2.70	1.44	70
0.70	7	2.76	1.56	73
0.70	8	2.80	1.67	75
0.70	10	2.85	1.82	78
0.75	6	2.90	1.54	70
0.75	7	2.96	1.67	73
0.75	8	3.00	1.79	75
0.75	10	3.05	1.96	78
0.80	6	3.09	1.64	70
0.80	7	3.16	1.78	73
0.80	8	3.20	1.91	75
0.80	10	3.26	2.09	78
0.85	6	3.28	1.75	70
0.85	7	3.36	1.90	73
0.85	8	3.40	2.03	75
0.85	10	3.46	2.22	78
0.90	6	3.48	1.85	70
0.90	7	3.55	2.01	73
0.90	8	3.60	2.14	75 70
0.90	10	3.66	2.35	78 70
0.95	6	3.67	1.95	70 72
0.95	7 8	3.75	2.12	73 75
0.95 0.95	10	3.80 3.87	2.26 2.48	75 78
1.00	6	3.86	2.48	78 70
1.00	7	3.86	2.06	73
1.00	8	4.01	2.23	73 75
1.00	10	4.07	2.58	75 78
1.00	10	4.07	2.01	70



The right flank completed

same way as for the pinion cutter except for cutting the teeth. Because this will be cutting brass there is no need for rake angle on the cutting face. Keep the slitting saw at centre height photo 16.

Using your cutters

The form tool will be very fragile in the smaller sizes. It will break if set slightly above centre height.

When you are making your pinion blank, remember to put a small cylinder on the end with a diameter the same as the cutter tooth width for easy centring. Finally, photo 24 shows how things can go wrong. The pinion cutter snapped at the shank because I foolishly put a sharp corner at the junction between shank and body thus making a stress raiser. The pinion with the bent leaf or tooth was because I was too hasty when parting off. ■



And finally.

Table 4 – Wheel Details

Module	Drill size	Form Tool D	Р	Q
0.2	0.47	0.63	0.94	0.63
0.25	0.59	0.79	1.18	0.79
0.3	0.71	0.94	1.41	0.94
0.35	0.82	1.10	1.65	1.10
0.4	0.94	1.26	1.88	1.26
0.45	1.06	1.41	2.12	1.41
0.5	1.18	1.57	2.36	1.57
0.55	1.30	1.73	2.59	1.73
0.6	1.41	1.88	2.83	1.88
0.65	1.53	2.04	3.06	2.04
0.7	1.65	2.20	3.30	2.20
0.75	1.77	2.36	3.53	2.36
0.8	1.88	2.51	3.77	2.51
0.85	2.0	2.67	4.00	2.67
0.9	2.1	2.83	4.24	2.83
0.95	2.2	2.98	4.47	2.98
1	2.4	3.14	4.71	3.14



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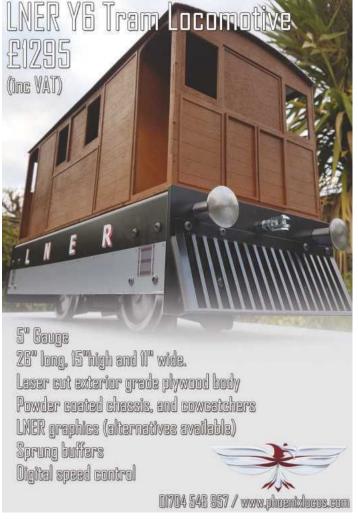


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SMEE Courses

Dear Neil, congratulations on your new articles on lathework for beginners. I'm sure they'll help many entering "the hobby" for the first time. Buying a lathe is a daunting task, and starting to use one a fascinating experience but many successful model engineers have started with very little previous knowledge.

At SMEE we've recognised that though many would like to make better models and develop engineering skills they haven't had training to make it possible. Few schools now teach the workshop skills once commonplace. Evening classes are hard to find.

So once again we're running courses to help newcomers start model engineering. Our Basic Training course starts in February 2018. Here experienced model makers discuss setting up a workshop, desirable equipment, and basics of using machines and hand tools. In fact, we'll be demonstrating using a Sieg lathe from Arc Euro Trade very similar to that in your article.

Each day session consists of lectures, discussion and demonstrations. All are held at the Society's base in South London with its meeting room, library and well-equipped workshop. We've had people come from as far as Doncaster and Dublin to join classes and participants have been very satisfied with training, going on to make interesting models or tooling, plus restoring classic cars and bikes.

Our second course starts in May 2018 and runs over six monthly sessions covering construction of a small oscillating steam engine and boiler. Our tutors demonstrate a variety of metal working techniques. Students make the celebrated "Polly" engine designed by "Tubal Cain". Techniques described are applicable to many other small engineering projects.

After each session delegates make parts in their own workshops in time for the next session. These courses are open to all but other SMEE courses including a milling course and the practical tool grinding course are for members only.

These courses are very popular as they demonstrate basic metal

work techniques now rarely taught in schools. They aren't 'hands on' courses but many participants have been inspired to enjoy model engineering and making metal components".

Techniques described or demonstrated include safe use of hand tools, turning parts, drilling and reaming, sheet metal work, soft soldering, silver soldering for strong joints and using a milling machine to cut slots and shape metal.

All our volunteer tutors are keen model engineers or toolmakers. I welcome enquiries. Further information on the SMEE website www.sm-ee.co.uk or write to SMEE Courses organiser courses@ sm-ee.co.uk

Allen Berman, SMEE Chairman



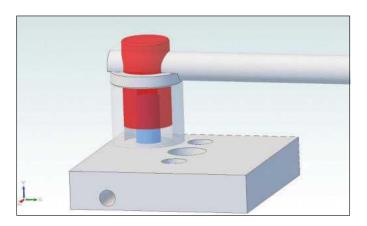
Fixed in my workshop

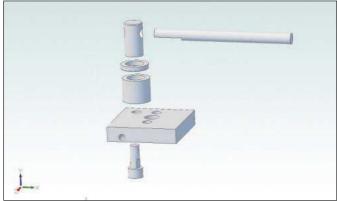
Dear Neil, in response to Gary Ayre's suggestion for examples of interesting domestic workshop tasks, here's a repair I did to the stripped spline on my shower knob. I made the brass flange and planed the spline on my lathe. Still ok after four years!

Mike Holmes, Derbyshire.









Toolpost Clarification

Dear Neil, I thought I should reply to Bryce Clifford's letter in the Autumn Special issue.

Because my lathe has a slot on top of the top slide to mount the original toolpost (MEW 255) I was able to easily fit an adaptor plate instead. I was therefore free to relocate the toolpost to minimise both the tip overhang and the arc through which it moves. The movement of the cross slide needed when tip is moved to a new cutting position is also minimised. The M10 caphead screw which serves as the toolpost is counterbored into the bottom of the adaptor plate.

To prevent it rotating there is a cross drilling in the adaptor plate in line with the head which contains a brass plug with an M8 screw behind it which clamps the head. To rotate the M10 caphead screw to change the handle locking position you loosen the M8 screw and rotate the M10 caphead screw and then reclamp it. The flats on the M10 caphead are simply there for convenience when doing this. In practice I have only had to make this adjustment once. If the washer or cylindrical nut or the M10 caphead wear and need to be replaced, then the adjustment will be handy.

The cylindrical nut is blind threaded M10 and does not reach the bottom of the caphead before the handle locks down the washer onto the pillar bolting it rigidly to the adaptor plate. The cylindrical nut is 20 mm diameter and was used as a gauge when boring the pillars which slide freely over it. The washer on top of the pillar is 5 mm thick and serves to spread the load from the two places where the handle passing through the cylindrical nut presses down and

to protect the top of the pillars. If the washer wears it can be simply replaced and if it is not exactly the same thickness as the original the handle will lock in a different position which can then be adjusted as described above.

There is only one critical dimension which is the height of the pillars as changing this changes the position the handle locks in – which is why all the pillars must be as near the same height as possible. As long as the pillars slide over the cylindrical nut they do not have to be a close fit to locate them. The insert holders are bored to fit the pillars so use one as a gauge and again the fit is not critical as the screw at the slit end will clamp it up tight.

I have attached two diagrams which I hope will make things clear. I have not included drawings because the dimensions will be specific to my lathe although I have mentioned the dimensions that I used. I am using triangular $TC^{**}16030^*$ inserts which have a 7-degree angle with tip radii of 2,4, and 8 (the last digit in the code).

I was pleased to see the letter from Peter Wilton in the August edition – it's nice to see someone has read the article! I had thought of adding an adjusting screw but because I have located my toolpost near the top left corner of my adaptor plate and the pillar is 1 mm from the edge there is nothing to screw against. In practice, having set the height once I have changed the inserts a few times without having to reset it (they are made to a tight tolerance).

Richard T. Smith

Hob(son's) Choice



For readers following Jeff Thyer's intersting series on Gear-Hobbing on the MYFORD lathe and indeed, those with a Jacobs Gear Hobber, may find it useful to know that a convenient source of constant-velocity joint for the blank/hob drive set-up is to buy or salvage a constant-velocity joint from a HONDA GXV120 (or similar models) self-drive lawnmower. The size is about right and there is ample load capacity. The last attachment illustrates the component.

I also have an appeal to readers: I wish to acquire accessories for my (now ancient) Taiwanese machine tools and recognising that the manufacturer would have exported to their immediate neighbours which means those in the Pacific rim area, I would like to assemble a contact diary of used machinery vendors from these countries: Taiwan, Hong Kong, Philippines, Vietnam, Korea, Vladivostok (Russia), Malaysia, Indonesia and Japan. I am seeking personal referrals from those who have had successful dealings with vendors in these countries. A general internet search is not a substitute for personal experience

as business in Asia is very much person-to-person. I welcome your e-mail and name contacts so please forward these directly to me at: pyralog@yahoo.co.nz

Andre Rousseau.

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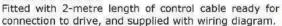
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A Suds Pump



John F. Firth makes a new suds pump for his Raglan 5" lathe.



Complete suds Pump

am a retired Mechanical Engineer with 32 years working in the Deep Mines UK Coal Industry in the UK. I started work as an Apprentice Mechanic at Rossington Colliery in Yorkshire in 1961. After 9 years as an Apprentice and a then a Mechanic (Fitter). I qualified as a Mechanical Engineer, and went on to a successful career as a Mechanical Engineer at four UK Coal Mines, then moved on to several other establishments in the coal mining industry.

My Father was Winding Engineman in the deep mined coal industry and he had always built steam models for most of his life, using various lathes.

He wanted to build a new 3 1/2" gauge locomotive and decided to acquire a Raglan 5" Lathe in 1964 for the Princely sum of £650. He continued to use it regularly until the mid 80's when age got the better of him and he passed it on for me to use in 1986. He had always complained that 'This Lathe' would be better if it had a coolant pump and system fitted, but he never got round to doing anything about it.

I installed the lathe in its new resting place in my workshop and made it ready for use. Over a period of some 12 months I completed several small jobs, but I quickly came to the same conclusion of my Dad, and that the finish I was getting was nothing like that I used to get when turning at my lathe at work in the 1960's. They were all fitted with a Coolant Pump system as standard, and it occurred to me that my lathe would benefit substantially from a retro fit of such a device.

So I decided that it was well overdue



Pump Motor

that I did something about it. This article is intended as a source of information and as a guide to anyone wishing to follow a similar route to a homemade suds pump, photo 1. Suds is the familiar term for a mixture of soluble oil and water used as coolant and cutting fluid for machining. The details shown in this article are taken from the actual used design for my lathe. What I consider to be the important points and measurements are referred to below.

It is left to the builder to interpret the needs of his own system requirements, however if this design is followed reasonably closely this pump configuration should perform perfectly well for many years. (This actual pump has been

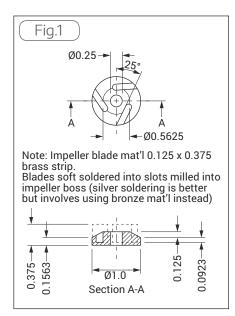
operating now for some 4/5 years, with only a need for cleaning the tank and pump suction once every year or so).

When I examined the Tray of the lathe I found it to be fitted with a suitable waterproof sump and drain for the use of coolant system, and when I looked at the documentation supplied with the lathe it was obvious that one was offered as an option with a new lathe purchase.

Obviously with the amount of time having elapsed it was going to be seriously problematic to acquire the actual pump system designed for this lathe, the makers of which had long-gone into liquidation.

This left me with several options. The first approach was to purchase a bespoke 'Off

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the Shelf' system (for example see Arc Euro Trade's Catalogue). This approach would solve the problem pretty well effectively and immediately, and I am absolutely sure it would have been a very effective solution.

The next was to research the internet looking for guidance and inspiration. As I expected there was a wealth of videos and ideas on the topic, all of which had resulted in a successful solution to this subject.

Having studied these for some little while I thought that many of the solutions (although beautifully carried out) were more complex, costly, and technically challenging than I wanted to spend time on.

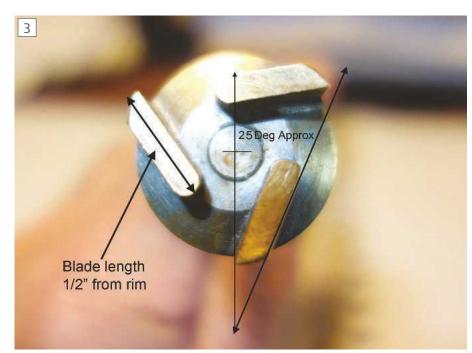
I needed something that I could have running from start to finish in less than half a day in the workshop, very simple in design, inexpensive to build using readily available parts but robust and reliable, with very simple electrics, no speed control and the ability to run for long periods either 'on snore' (with very little fluid coming through) or with the output valve closed without damage or problems. These requirements caused me to seek a rather different and hopefully simpler solution.

My approach was to design my own Pump System from scratch. The first consideration was finding a suitable pump, able to run continually on snore or against a closed valve without damage, using readily available parts from the scrap box (if possible).

The second consideration was how to power such a pump without recourse to the use of a 240 V supply, instead using a low voltage power supply. This would reduce the inherent risks of using liquid near to mains voltage.

A search of the scrap box and the internet did not really yield much in the way of suitability for my needs other than many bits of pieces of metal and screws that could be put to use if a suitable design could be developed.

However, a visit to my local electrical hobby store yielded 6 – 12V motors for £5, (83 pence each) sitting there in the shop window, and just waiting for someone like me. These



Impeller blade angles

motors were actually unused and brand new, and they were of a type normally designed and used in Battery type hand power tools and drills, **photo 2**. These were of really good quality and would be suitable to run at low loads such as these almost continually.

The Motor

The next task was deciding on the type of pump required.

- It had to be able to run at the high speeds developed by these types of motor.
- It had to be tolerant of a small amount of metallic debris entrained in suspension in the Coolant tank, without damage.
- It had to be self lubricating.
- It had to be self priming.
- It had to be able to run at a consistently lower voltage and -
- It had to be very low cost, easily installed and maintained.

• It had to be easily made in the workshop, hopefully in less than a day.

I considered that all these considerations could be covered by using a fully submerged centrifugal pump, made to large tolerances, using materials that would be able to withstand total immersion, with bearing materials that would allow the soluble oil content of the cutting fluid to provide sufficient lubrication to the pump impeller shaft. And, of course it had to last a long time without significant maintenance.

The Impeller

The first decision was to decide was decide on a suitable impeller/pump casing layout and size.

I have had much experience of using centrifugal multistage turbine pumps however for this pump high efficiency is not needed, so the pump impeller curves and



Finishing impeller to size

the delivery volute curves are not critical, when all we need to achieve is get a pump that actually pumps, so after some thought I chose a diameter of 1" for impeller body. This would be turned from a scrap piece of brass bar and bored and reamed to 1/4". No real attempt was made to create a drawing of the impeller using ACAD, but just relying on common sense to provide the right look and feel for the job, **fig. 1**.

The Blank impeller was bored and reamed to ¼" and Loctited onto a short stub of ¼" silver steel rod to allow it to be mounted vertically in the chuck of the Rotating table on the milling machine.

The three 1/8" Vane slots were then milled at 120° into the impeller blank at 25° to vertical and 50% into the depth of the impeller rim, **photo 3**. This depth is more than needed however needs to be enough to ensure that each blade is soft soldered securely into the impeller, each a tight fit in its own slot.

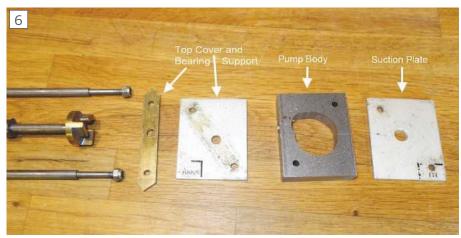
Following machining the blade slots, three blades were made by hand from 3/8" x 1/8" brass flat ready to solder into the Runner. Each blade was left some 30 thou long to be machined to length in the lathe later

The Runner was then removed from the machining mandrel using a little heat to soften the locktite, it was cleaned up and each blade was securely soft soldered into its slot. I should point out that I did seriously consider silver soldering for this part of the work, but I decided to make the blades a very good fit in the impeller with a harder soft solder, and the use of brass allowed me to use off-cuts of brass bar and strip and made the material used much less expensive.

In order to ensure that the pump always 'picked up' I decided it would be prudent to design the pump case to run fully submerged in the coolant tank, which involved making a long motor/shaft arrangement to place the motor outside (above) the tank, with the pump body well below the tank coolant level. This would ensure that the pump always



Details of the impeller in situ



Top cover, pump casing and bottom cover parts

picked up on starting.

The length of the Pump Casing/Motor support rod is really dependent on the size of coolant tank you wish to use. I had a suitable tank available and decided that a

pump shaft of 9" in length would give me a liquid level range of some 10 litres, which has proved to be more than adequate for a lathe of this size in my view.

At this point the 1/4" Pump Impeller shaft length was arbitrarily decided at 9" long. (But within reason this could be almost any length you want).

It was assumed that this length would allow the Motor assembly to be at some 2" above the top of the coolant tank, leaving some 7" available to be placed below water/coolant level. In the event, the pump motor face was mounted directly on the top of the tank and I actually got 8" submersion in the liquid.

The Runner was now refitted to the unfinished final pump shaft for machining in the lathe (again using Loctite). It was then placed in the lathe where it was faced up, and the vane tips and bottom edge were machined to finished size, **photo 4**.

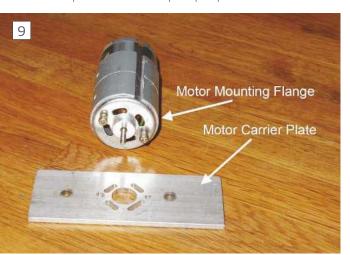
Sizes are not that critical here, as we need to make sure that the impeller can handle some small amount of swarf debris without binding or seizing up, but it should also be noted that if the impeller clearance to the bottom cover if too great there will be much slippage of liquid here and this could lead to poor pump performance.



Suction end



Expanded view of complete pump



Motor Mounting Arrangements

I suggest a clearance of some 20 thou to be about right. This has proved to work well

Also note the rounded leading edge on each impeller blade to allow smooth flow at the vortex hopefully preventing some cavitation noise.

Once again, the design of the pump casing and volute layout is not all that critical for such a small pump where efficiency is not all that important and clearances are deliberately left a little on the generous side due to the possibility of particles on entrained metal in the coolant liquid.

The pump casing is made from a 2 1/2" x 1/2" BMS cut off at 2" long. The actual size is unimportant really.

The blank casing was centred in the lathe and bored in the centre at 1.25".

The Impeller at 1" diameter is to be placed in the casing to create the 20 thou (+/- 10 thou) clearance shown in **photo 5**. This is the position that determines the final layout of the Pump/Motor position.

Once the hole is bored the pump casing it is transferred to the milling machine to cut the Volute relief area. This is not critical for this use and there is quite a lot of leeway in my view as to how it should look, but it just serves to create an area of slow flow and high pressure.

Care need to be taken that the remaining metal is thick enough to retain the outlet pipe, which in my case was drilled to suit a length of stainless steel pipe I had in stock, it was then to be Loctited in position later.

The outlet pipe position was marked out and drilled to line up with the centre of the thinnest case position above the volute space created. Once again this is not critical on placement.

The Pump casing covers (two) are once again non-critical parts, constructed from a piece of scrap aluminium plate from an old workshop low voltage power supply. These were cut to the same size as the pump casing to form the top and bottom covers.

The position of the top cover shaft gland was marked off to the position needed to create

the 20 thou clearance to the impeller. This position sets out all other points needed to ensure that the motor, impeller and casing are all aligned correctly.

The holes on the pump casing are set in 3/8" squared on the opposite corners, these are used both to locate both pump end plates and also the motor mounting columns above the pump.

From these holes the motor mounting plate can be marked out and machined for the motor then drilled for the support columns as well.

An impeller shaft bearing plate made from phosphor bronze strip was included above the Top cover to make sure that the impeller bearing position is maintained and properly controlled.

Top Cover, Pump Casing and Bottom Cover Assembly

Photograph 6 shows the items laid out in assembly order. Obviously, the length of the machined Pump Column ends is made to suit the layer thickness for the Bearing/ Pump Body Assembly. Photograph 7 shows these parts assembled.

It should be also noted that this type of pump could be left running for extended period with little or even no flow passing through the pump. It is important to ensure that is this event precautions are taken to ensure that some flow always takes place. In my case the hole for the impeller shaft in the top pump cover was made some 50 thou oversize, and the bearing strip was packed away from the top cover with a single 50 thou washer at each end.

This arrangement ensured that some excess flow was always forced through this gland area creating steady stream of coolant escaping from the gland and continually washing new coolant across the bearing. (Obviously care needs to be taken that this hole is not too big, otherwise significant flow could take place here, causing the pump to fail to create sufficient head at the nozzle).

All of the pump parts are shown in **photo 8**. The motor mounting plate layout is dependent on the motor fittings, dimensions and shaft sizes. The motor I used conveniently had tapped holes for end plate mounting.

This particular motor had a machined mounting stub at the shaft end of the motor. This enabled a fitting hole to be machined into the mounting plate to ensure secure positioning. The mounting plate was made from a scrap length of aluminium 1" x 1/8" strip, photo 9.

The marking out points for hole positions were transferred from the pump casing end of the pump to create the



PC Switched Mode Power Supply





12

20 Pin ATX PC Photograph Motherboard power Plug

centres for the three positions needed at the motor end.

You may note that this motor has four ventilation slots in the mounting end of the motor. You will also note that these slots have been transferred to the motor mounting plate to ensure that ventilation is maintained, and the motor does not overheat in extended running periods.

The motor used and tank available will all have a bearing on the top end arrangement for the pump, but I am pretty sure that nothing here is beyond the skill of many model engineers, especially as most of the fitting sizes are for the most part not that critical.

I have done a search on the internet using the search term 'Cordless Drill Motor' and there are literally hundreds of them available at voltages up to 24v, so supply should not be a problem. A recent search for the 'Johnson 550 DC Motor' rated at 12v and 21000 rpm or a generic type of product of similar size seems to come near the mark for this project, but once again the type is not critical here.

Setting Up

Obviously, the impeller has to run confined in the casing between the top and bottom plates. In order to prevent the impeller seizing up, and to create the back clearance need to ensure sufficient slippage of liquid out of the back seal, the impeller needs to be reduced in width.

I made the impeller 20 thou thinner than the 1/2" space created for it between to two pump plates. The setting of the impeller is important by careful adjustment at the motor shaft coupling, to prevent binding on either plate and make sure of a free running pump. This setting is maintained by the motor bearings. There is a little thrust applied to these bearings by the reaction to the pumped water on the impeller, but as the pressure is only around 2 psi the amount of thrust on the impeller is only just over 1.5 lbs force. This has not been a problem so far after 3 years of running.

At full flow and 12volts supply this motor was taking 4 A at 3V. A recent measurement of output at full flow with my new flexi tube fitted has shown a measured flow rate of

Fig.2				
(orange) (orange) (black) (red) (black) (red) (black (grey) (purple) (yellow)	+3.3V +3.3V GND +5V GND +5V GND PWR_OK +5VSB +12V	1 Pin 11	+3.3V -12V GND PS_ON# GND GND -5V +5V +5V	(orange) (blue) (black) (green) (black) (black) (black (white) (red) (red)

ATX 20 Pin Motherboard Connector

30 fluid ounces per minute (1.5 pints/Min). I my view this is more than enough for most turning jobs on a lathe of this size.

The finished pump was shown in photo 1, and a video of the completed suds pump running can be seen here.

https://www.youtube.com/ watch?v=gyHTgDIn3Ts

Videos of the Suds Pump Test Runs may he seen here

- 1. https://youtu.be/q7P-4zai-Y4
- 2. https://youtu.be/RJXYnblT4K4
- 3. https://voutu.be/BDx29YoDs2k

I have decided to include a description of the actual power supply solution I used for my Suds Pump system. Readers will be all too well aware of other ways to supply power to a pump designed such as this and may well desire to create a different solution to this problem.

Power Supply

My DC power supply for this project was one of the many uses I have found for old PC switched mode power supplies, **photo** 10. It was first set up to power my two 12volt LED spot lamps.

I originally set up the power output board with three terminals at 3, 5 and 12 volts.

Many have utilized a PC power supply for things other than powering a computer and I have seen several articles on the uses and conversion of a PC switched power supply. Such articles may be a rich source of information on the details for anyone wishing to undertake such a conversion. They commonly have voltage outputs of 3, 5 and 12 volts, mostly at moderate to high amps of up to some 35A.

I chose to strip down the power supply and solder every 3, 5 &12 volt rail lead together to bring a common high amp output for each voltage. These were then taken to four terminals on an output plate with a low voltage power supply on/off switch.

The terminals were Ov, 3v, 5v. & 12volt. I have tried all three for this pump but mainly use 3 and 5 volts and vary the output if needed. The PC switched power supply is turned on and off with a small DC switch connected to the control power signal.

My ATX Plug was of the type shown below, and the power switch is between pin Pin 14 (Green) and any ground pin e.g. 3, 5 or 7 (Black), fig. 2, photo 12.

It should note that this low voltage switch only controls the output from the power supply. It does not remove the power from the power supply and isolate it from mains voltage. The main board remains live for as long as the mains power to the power supply is left switched on. Most of these types of switched power supplies have a built-in mains switch, but the power must be disconnected from the power supply before the case is opened for working on the circuit inside.

These details can be resourced on line by looking for a 20 pin ATX Power Connector. Other types of power supply are widely available and suitable information should be consulted prior to carrying out any work.

Notes

This kind of work entails working in the mains voltage side of a power supply (even though only the low voltage leads are the ones needing any alteration). Proper precautions should be taken to ensure that you remain safe when carrying out electrical work. If you are not skilled or proficient at this kind of work, please ensure that you seek the help and guidance of a professional electrician.

Should any reader want to address points of clarification or have questions or helpful comments, I can be contacted at iffirth@ btinternet.com where I will endeavour to reply promptly. ■

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One Man and his Many Lathes



Stan Nesbitt recalls his workshop companions over fifty-two years in the workshop.

he period covered by this article amounts to 52 years and is greatly condensed but hopefully still contains the essence of my experience. Sadly, I do not have photographs covering the earliest years. Many of the other photos are from old prints, so apologies if they do not reproduce well. Whilst I have often struggled to purchase lathes, they have always repaid me with their increased sale value.

Home Made Wood Turning Lathe

Whilst stationed at RAF Laarbruch from 1964 to 1967 (now Weeza Civil Airport) in Germany and living in a local town called Kevelaer, I was friendly with a local chap. He knew I was interested in Lathes and he said his father had made a lathe which was now just sitting in his back garden and he said I was welcome to have it. It was constructed from angle iron and heavy steel tubing but had roller bearings in the headstock. The maker had been captured in Russia in 1943 and did not return home until 1953. As there was a spare room in our flat I was able to use this machine there and was given basic instruction by a pal who was an aircraft fitter. The lathe was shipped back to RAF



Arundel Wood Turning Lathe

Ballykelly, my final posting. Eventually I sold this lathe to my brother for £5 and he quickly adapted to the wood turning craft. The lathe is still in his shed but he seldom uses it now. I wonder what the maker would think if he knew his creation was still operational so many miles from his home.

Unimat Lathe

Purchased on easy payments from my wife's Freeman's catalogue! Living in married quarters I had to operate this lathe on the kitchen table but I still found it very useful. This lathe was sold in 1969 to a pensioner living in a small terrace house in Belfast for £40.



Karger plain lathe, modified with ex-wagon brake lead screw!



Harrison Union Graduate wood turning lathe





Parts of the 19th century lathe

Harrison L5a

Living in married quarters I had to operate this lathe on the kitchen table but I still found it very useful.

Myford ML4

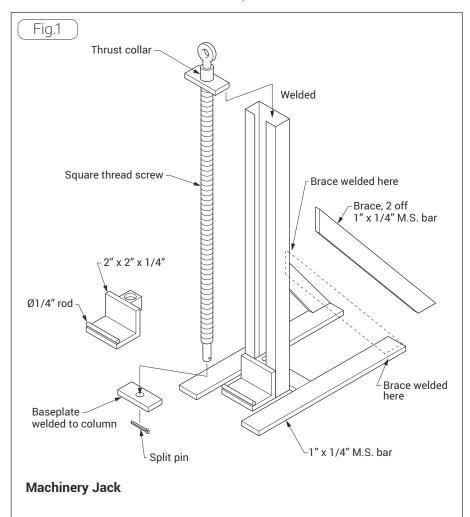
I spotted this lathe in a small engineering works in Limavady Co Londonderry and the proprietor agreed to sell to me for £20. Back then c1969, when credit cards were unheard of, he agreed to accept a post-dated cheque. Those were bleak years when a corporal's take home pay was about £15 per week, post dated cheques were often resorted to. When I was demobbed in June 1969 this lathe moved with me to Ballymena where I had started a job of Training Supervisor at the new Michelin factory. When dismantled the bed could be carried by one man. I used this machine for several years, but I found the gear setting up quite tedious and tended to limit my activities to plain turning. As I was becoming more interested in wood turning I sold this lathe for £40 c1973 and bought a new Arundel Wood Turning lathe.

Arundel Wood Turning Lathe

This lathe, **photo 1**, paid for itself many times over and turning could be done on both ends of the headstock. I still have this lathe and recently when I was without a metal turning lathe I made a metal turning attachment using an adapted cross vice.

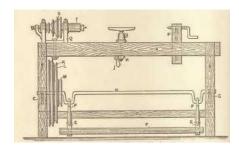
German Plain Metal Turning Lathe (Karger)

After about 4 years with Michelin I secured a position as a Training Officer with a new factory opening in Craigavon making Printed Circuit Boards. This appointment involved 4 months training in West Berlin at the parent factory in 1974. The Berlin



Wall was very much in evidence at that time. One day when I was passing an unused room in the factory I spotted a small plain lathe sitting unused on the floor. My German was good enough to ask one of the Directors if I could buy the lathe. He very kindly said I could have it at no cost. On my Friday afternoon off I crated up the lathe carefully bolting it to the bottom of the crate. The proprietor's PA arranged for it to be shipped from Hamburg to Belfast. However, when I returned home I had to pay £70 to the Belfast shipping agent for import duty

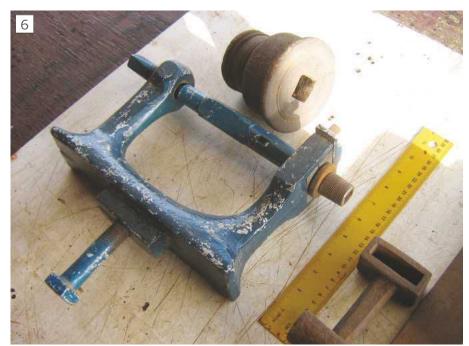
etc. I made a number of modifications to improve this plain lathe. The flat belt pulleys were replaced with 3 step vee pulleys. A lead screw (an ex wagon brake control screw) was fitted to enable longitudinal feed without the use of the top slide, **photo 2**. The large face plate hanging on the wall behind the lathe was obtained as follows. I made wooden pattern at home and when I was attending a Home Office training course in Wakefield I had a casting made by Blackgates Engineering. The fitting to the headstock was carried out by a local engineering firm.



When I acquired the Harrison L5A I sold this lathe to a chap who made jewellery, for £200.

Harrison Union Graduate Wood Turning Lathe

I was lucky to acquire this top of the range, long bed wood turning lathe from a government surplus sale, **photo 3**. During that period, I turned newell posts, balusters and billard table legs for a local joinery works. Although it was already a large lathe, I added a bed extension to cope with 6 feet of material between centres. Material which is six inches square and six



The simple headstock



Reverse of the headstock



Parts offered up to reconstructed wooden bed

feet long rotating at 500 revs can be quite scary when roughing out. Hence the use of the 4-jaw self centring chuck which is more secure than a prong centre. However, when automatic lathes started to appear, this type of work dried up. I sold this lathe for £400 which enabled me to purchase the Harrison L5A.

Harrison L5A

When I lived in local village during the early 1980s there was a small precision engineering works directly across the road from my bungalow. On one of my visits to his shop I spotted this lathe, an ex-technical school model, which was not in use. He offered to sell it to me for £400 and a local farmer delivered it, leaving it on a pallet in the middle of my garage. It was a very heavy machine which included its cast iron base with attachments, **photo 4**. I fitted a castor on each corner and easily wheeled it into position. The seller provided two ¾ inch soft wood boards and advised that if the lathe was positioned on the boards



Arrangement for headstock nose bearing adjustment







The tailstock is strange to modern eyes





Maker's plate

Drummond Round Bed Lathe

there would be no need to bolt it down. From a local scrap yard, I obtained a vertical style car jack and modified it for lifting heavy machinery capable of lowering to 1/2 inch and withdraw, fig. 1. This machine was a proper professional geared head lathe with automatic feeds and a large capacity, but it was quite noisy in use even after I had renewed the Headstock bearings. I changed the 3-phase motor to single phase and repainted the whole machine. When I removed to my present location the castors burst through my trailer floor.

Over the years I have found that a lathe can prove a useful investment and nearly always increases in value.

Initially the lathe was installed in a large wooden shed until the house was built. During the years when I was manufacturing hardwood garden furniture, this lathe was very useful when maintaining my other machinery. When I decided to sell the Harrison, I advertised it in a local newspaper as was usual at that time. I received a few phone enquiries from a Belfast man and he eventually arrived with his son to view the lathe. They had been dropped off by relative who had gone off shopping. I switched the lathe on and it was obvious that the older man had been a lathe operator. He was beaming as watched the lathe and moved various levers. However, after a few minutes his son started moving other levers as his father continued



The lathe advertised in Model Engineer



The snappily named CJ0623B 9x30 lathe



Headstock of the lathe showing gearbox ratios

to operate. Alarmed by this development I stopped the lathe and asked them to leave my property. Although the father would have liked the lathe, he had no money and I gathered that his son never really intended to purchase the machine. It was a dark winter's evening and as I live in the country devoid of any street lighting, they were obliged to set off on foot, telephoning for their lift to pick them up. Some days later the man rang to apologise for the occurrence. Now I know why many advertisers append their adverts with the words "No Time Wasters". This lathe was sold for £800 and the lifting device mentioned earlier went as part of the sale. Over the years I have found that a lathe can prove a useful investment and nearly always increases in value.

Antique Lathe c.1870

Many years ago, when visiting a local scrapyard I asked the proprietor if he had any old lathes. He sold me the subject lathe for £5.00 but it didn't seem worth while trying to restore it due to it's crude construction, photos 5 - 11. However, it may have more merit than first impressions would have suggested. I now understand that it was manufactured about 1870. This design, a two-speed lathe, was intended for turning wood and light metal. The 1919 book on Lathe Design, Construction & Operation by C Perrigo describes this type of lathe with a wooden bed and a headstock with babbit metal bearings and square taper mandrel, figs 2 and 3. The old "chain lathe" has a tailstock of similar design. Perhaps one day I will find the time to restore this lathe, if only to sit as a display model and as an example of this stage of lathe development.

Drummond Round Bed Lathe

One of my work mates acquired this lathe and traded it to me for some work completed, **photos 12** and **13**. Sadly, there are pieces missing, the mandrel, the stepped pulley, bearings and gearwheels. This lathe merits a thorough restoration and when time permits I hope to bring it



This view shows the impressive capacity of the lathe.

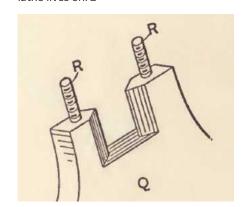
back to life if only to sit as a showroom model and as another example of a stage in lathe development, **photo 14**.

CJ0623B9 x 30

This machine, my present lathe, purchased from Amadeal, may be considered as a bargain basement lathe, **photo** 15. However, when one considers the specification, this design is very competitive at the price. The variable speed from 50 to 3,000 rpm forward and reverse, the Norton type gearbox for imperial and metric thread cutting and its adequate proportions are its main attributes, photo 16. Unfortunately for a relatively large large lathe, photo 17, the tailstock locking mechanism is inadequate. The two stems of the cams flex under load and one must resort to tightening the holding nut which is tedious. I am aware of modifications to correct this and hopefully I will soon

attend to this problem.

Lathes will normally outlive their owners and be passed on to another good home. Even when a lathe suffers rough usage, neglect or abandonment, it may eventually become a "barn find" and perhaps a restoration project and so the lathe lives on.



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Readers' Tips ZCHESTER MACHINE TOOLS



Sucker for punishment





We all lose tine parts from time to time; Bob Lamb wins this month's Chester Vouchers with a tip for finding those elusive little objects.

I discovered this yesterday and thought I should share it with others. No matter how often I tell myself to carefully dismantle anything OVER A RECEPTACLE I don't always do it. Last night was no exception and, as I was changing a tool bit, I dropped the tiny torx screw onto the floor.

The floor is, of course, stained and multicoloured so it is difficult to find anything that I drop. I did my normal sweep first with a broom and then with a magnetic pickup tool - no success. I have to add that there are many small nooks and crannies for things to get lost in and I nearly gave up. It then occurred to me that I could use my Henry vacuum, but I didn't fancy rummaging through the bag to try and find a tiny screw amongst all the other debris.

The solution was to take the nozzle off the end of the hose and replace it after covering the end of the hose with a small piece of white cotton rag. It was still easy to push on the nozzle with the thin rag in place. I switched on Henry and after hoovering every crack I could see I switched off, took off the nozzle and checked the rag OVER A CONTAINER. Bingo the screw was there together with a few other nuts and washers.

Simple - and it encourages cleanliness.



Bob Lamb

We have £30 in gift vouchers courtesy of engineering suppliers Chester Machine Tools for each month's 'Top Tip'. Email your workshop tips to neil.wyatt@mytimemedia.com marking them 'Readers Tips', and you could be a winner. Try to keep your tip to no more than 400 words and a picture or drawing. Don't forget to include your address! Every month I'll chose a selection for publication and the one chosen as Tip of the Month will win £30 in gift vouchers from Chester Machine Tools. Visit www.chesterhobbystore.com to plan how to spend yours!

Please note that the first prize of Chester Vouchers is only available to UK readers. You can make multiple entries, but we reserve the right not to award repeat prizes to the same person in order to encourage new entrants. All prizes are at the discretion of the Editor.

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Improving a Small Horizontal Bandsaw



Norman Billingham fits a sub-vice to his bandsaw





The drill vice as purchased

The bandsaw vice as supplied

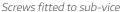
he small horizontal bandsaws available from most suppliers of machine tools for model engineers are invaluable bits of kit, especially if you are getting on in years. Cutting discs from the end of a piece of 2" mild steel bar by hand is not something you'd want to do too often. I bought my saw from Chester Machine Tools a few years ago when it was on special offer, but they are widely available. Mine is the smallest size. It was remarkably cheap and is pretty crude, but since I replaced the cheap blade which came with it with a better, bimetallic one, it has served me very well.

However, they do have limitations. In particular, the short, swivelling, moving jaw of the vice is fine for the intended job of cutting lengths from long pieces of bar stock, but it's a serious limitation when you want to cut a short piece or need to hold a part close to the blade. Photograph 1 shows the vice on my saw as it was supplied (plus a bit of rust - the saw lives in the



The bandsaw vice rear jaw after removal of the jaw plate and drilling for sub-vice mounting





garage and is neglected!) The distance from the vice operating screw to the blade is about 4.5", which means that something like 6" of bar has to be available for it to grip safely. If, like me, you often buy metal in the usual 12" lengths sold by ME suppliers, then you can only use about half the length before it becomes too unstable to hold.

I found I could get round the problem by using a second vice, taking advantage of the fact that a small



The new sub-vice mounted and ready for use

drilling vice will fit nicely vertically through the throat of my small saw. I don't claim any originality for this idea, but it's helped me a lot.

Photograph 2 shows the cheap vice which I bought; I think I picked it up at one of the shows for few pounds. It's a pretty nasty device by engineering standards but it's only 65 mm wide and drops vertically through the throat of the saw without fouling.

Photograph 3 shows how I removed the (largely useless) rear jaw plate from the saw vice and drilled two 8mm clearance holes in the rear jaw. I checked the positions fairly carefully then drilled the holes by hand using an electric drill. Not hyper-accurate but it didn't need to be.

The vice I bought has a steel base plate set into the casting at the jaw end, so I removed it, clamped it to the saw vice rear jaw, spotted the two holes through then drilled and tapped to take two M8 cap screws and refitted the plate to the drill vice, **photo 4**. The vice can then be mounted vertically on the saw, photo 5. The mounting holes were positioned so that the saw blade just clears the vice jaws, by about 1 mm.

In use, the moveable blade guide has to be retracted to clear the

sub-vice and allow the blade to be lifted, but this has never been a problem and the set-up makes the saw much more versatile. Of course, the maximum diameter which can be gripped safely is smaller, but this is not much of a limitation and more than compensated by much greater versatility. The sub-vice can easily be removed in a couple of minutes and the saw returned to its original design.

ISSUE MODEL EXTISS ENEXTENGINEER SUE N

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- Out and About
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- Otago LBSC Memorial Run Jim Woods reports from Otago on their LBSC 50th Anniversary Run.
- A Day Out in York
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- LNWR Tool Chests
 Chris Rayward makes the lids for his Webb tender tool chests.
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 Ray Griffin makes the valve chest and piston valve for the Stuart steam hammer and adds the lever assembly.

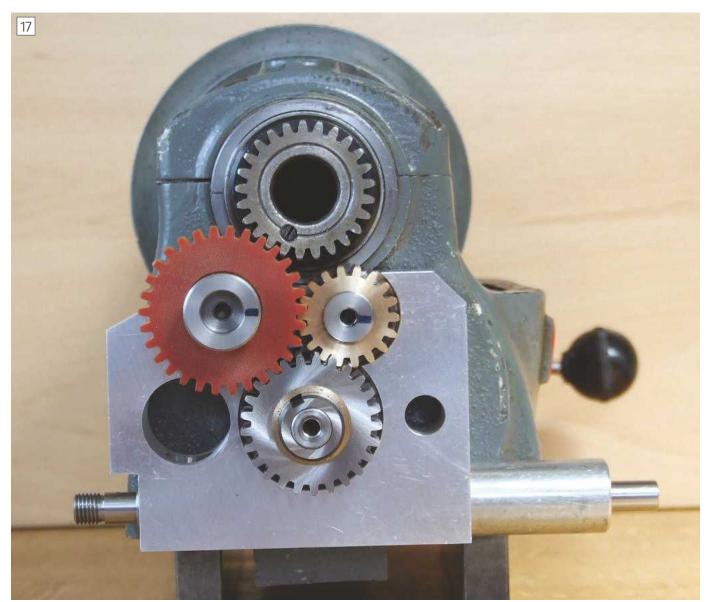
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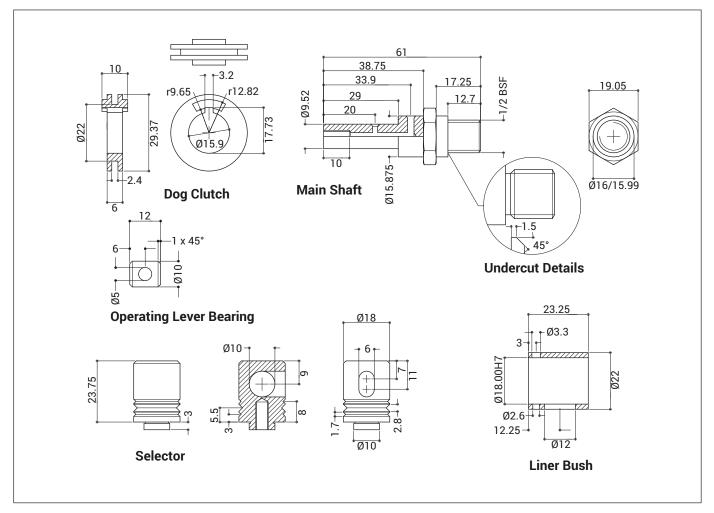
The development and design of a

Screwcutting Clutch for the Myford ML7

Graham Meek recounts how he came to revise his design for the ML7 and gives advice on its making and use - Part 3



Trial assembly



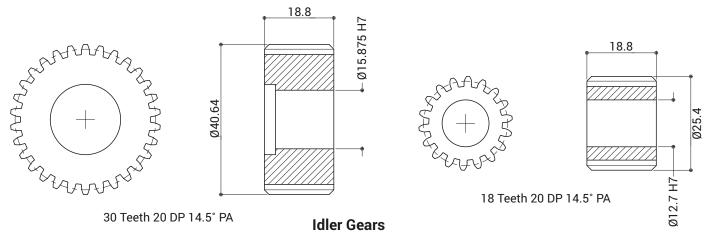
he basic dimensions of this bush for those who wish to order one are, 12 O/D, 8 I/D by 12 mm long. This could quite easily be turned from phosphor bronze, PB, but it will not have the porous nature of sintered bronze or the oil retaining properties. Therefore, an oil hole needs to be provided for the occasional squirt. Might I suggest a hole in the side of the main body extension rather than on the top where dirt and dust will congregate which will more than likely migrate into the bearing. Another Oilite bush is used at the rear of the main body for the operating shaft. This time the bush sizes are 1/2" O/D x 3/8" I/D x 5/16" long. This bush again can be manufactured from PB with a similar oiling arrangement. However, this bush needs to be fitted after the operating shaft is installed so any oil hole will need to be predrilled and lined up with the corresponding hole in the main body. It goes without saying that the 1/2" hole in the main body needs to be a reamed or bored hole in order for this bush to be a good fit. This bore also wants to be in-line with the opposite end and this can be achieved by gripping on the boss once this has been pressed into the main body. A good chuck is required for this operation. If the readers chuck is at all suspect then I would recommend using a 4-jaw chuck. Clocking the extension boss to ensure concentricity and then running the clock along the two sides of the main body

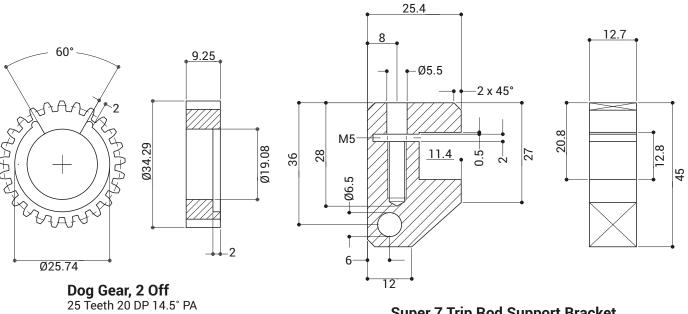
to ensure these are parallel with the lathe centre-line.

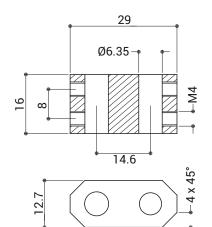
Connecting the operating shaft to the selector is the operating lever. This is locked into the operating shaft by a short pushrod and an Allen grubscrew. The length of the push rod depends on the length of the Allen grubscrew used, and is therefore ascertained on assembly. The operating lever turns the radial movement of the selector shaft into the linear movement of the selector by means of the operating lever bearing. This bearing allows the operating lever to slide within the selector as the respective centres change due to the angular or radial displacement of the operating shaft. The operating lever was made from silver steel, it does not have to be. Mild steel, (BMS), would serve equally as well and would possibly make tapping the M3, (or similar) hole in the end easier. The size of the BMS wants to be close to 5 mm diameter, 0.01 mm undersize will give a nice easy fit in the phosphor bronze operating lever bearing. The diameter of the lever bearing would also benefit from being about 0.01 mm undersize. I had better point out at this stage that these tolerances only apply provided the respective holes for the various parts have been reamed. I cannot recommend any clearance for a drilled hole which really is not suitable for this type of work. D-bits are a very good alternative to expensive reamers and are easily

sharpened when dull. These clearances will allow the bearing to rotate freely in the selector as well as slide laterally to accommodate any misalignment between the relative hole centres. The purpose of the M3 tapped hole in the operating lever is to aid insertion and extraction of the lever. The lever is threaded onto an M3 capscrew about 35 mm long and this then makes things a lot easier. Once the lever is locked in place the capscrew is removed. It will also be found a whole lot easier if the shank end of a 4.9 mm diameter drill is used to align the holes in the operating shaft and the operating lever bearing prior to inserting the operating lever. To make the operating lever even easier to insert the end is chamfered with a 15-degree chamfer about 0.5 mm wide.

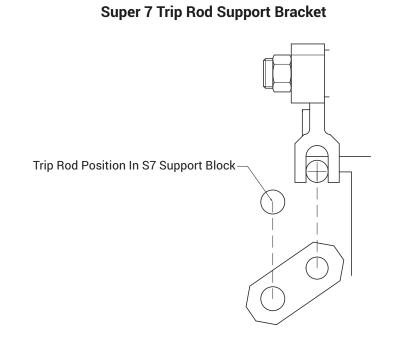
A good chuck is required for this operation. If the readers' chuck is at all suspect then I would recommend using a 4-jaw chuck.







Suggested Connector Block



On the operating shaft sits the trip lever which connects the trip rod assembly to the operating shaft. The manufacture of this part needs no description from me as it is pretty straight forward. The 2 mm diameter dowel hole does need to line up with the operating shaft and some constructors might like to do these two items together. Alternatively, the holes could both be drilled using coordinate location to the pre-reaming size and then reamed to size on assembly. Again, although a 2 mm diameter dowel hole is specified the reader could with advantage use a 3/32" dowel if preferred. However, I do need to point out that on no account should this dowel be omitted. This little dowel is all that is stopping a collision between the tool and the chuck. Relying solely on the nut alone to hold this lever against the force of the trip rod is a recipe for disaster.

Attaching the trip lever to the trip rod running along the bed is accomplished by a ¼" diameter connecting shaft running between the headstock casting and the countershaft casting. On most machines there is just enough room for this to pass through easily. Should this not be the case on the reader's machine then three options are open. One is to shim the countershaft casting away from the headstock casting. Another is to reduce the size of the connecting shaft, to say 6 mm or 7/32". Finally use a rectangular section mild steel connecting link. In the original design a block to connect the connecting shaft with the trip rod was designed. This was intended to lie at an angle of 45 degrees to the vertical when fitted. Should options 2 or 3 be taken then this block will need modifying in line with the chosen option. The length of the connecting shaft has not been specified, purely because I have not received this information from any constructor. The maximum length of the connecting shaft is determined by the connecting block missing the rear of largest faceplate fitted to the spindle. This position being reached when the operating ball handle is pushed fully towards the left. The trip rod length is also not specified as this will vary with the between centres dimension of each lathe variant and the position of the connecting block.

The trips are exactly the same as those used on the S7, they are intended to fit such that they impinge on the carriage casting, just below the wiper, see photo 18. A more general picture of how things are designed

I would most certainly recommend slower speeds to start off with until your confidence level rises.



Earlier Wiper assembly, courtesy of Ken Willson

to go together is shown in photo 5, but this is for the S7 so it does not have the ML7 'Dog leg' connector block. At this location the trips are easy enough to adjust and see. The bracket which sits at the tailstock end is also borrowed from the S7 unit, it can just be made out in photo 5.

When setting up to machine a thread the stop has to be set in advance of the actual finishing point, this is where the 'Handwheel Dial' is a great help. Let's consider setting up to cut a thread, with the motor off, engage the ball handle in the direction of travel, let us say towards the headstock, ensuring full engagement by turning the chuck by hand. The handwheel dial is set to zero at the end of the thread in hand and the stop provisionally set. Return the ball handle to neutral, wind the saddle back towards the tailstock a little and start the motor. Again, engage the ball handle to the left, then using the handwheel continue to feed towards the headstock until the leadscrew stops revolving. The distance from zero is the amount the stop has to be moved towards the headstock. If the travel is beyond zero then this is the amount the stop needs advancing towards the tailstock to get the saddle to stop at the zero mark on the Dial. Adjust the stop and recheck the setting, carry out the same procedure at the beginning of the thread, i.e. tailstock end in this case. Finally checking both settings with the clasp nuts engaged, as moments of inertia need to be taken into account, settings vary with mandrel speed and pitch of screw being cut. This sounds a long and protracted method but in practice it is quick and quite simple really. Further as you get to use the attachment more and more, the amount of travel required to trip the clutch will become a known quantity and can be dialled in from the outset, I seem to recall the Hardinge was around 5mm, but do not quote me on this as it is now nearly 30

years since I last operated one.

One thing that is important is that care should be exercised when using the tailstock to support any workpiece, as clearance is needed between the saddle casting and the tailstock base to avoid collision and therefore damage to the lathe.

Whilst theoretically it should be possible to screw cut at 2000 RPM using this set-up I would not want to prove the theory, there could be some expensive scrap. It should be possible to screw cut at about 210 RPM when cutting ME threads, coarser pitches would probably require backgear, and at the end of the day it is down to the user with regard to what he or she feels happy with. I would most certainly recommend slower speeds to start off with until the confidence level rises. You will know when you have reached this level when you are prepared to contemplate cutting an internal thread: the unit works in exactly the same way.

Just for information the bottom speed of the Hardinge, which has an infinitely variable speed range, is 125 RPM, but increasing the speed after setting the stops would alter the stop/start thread setting slightly and was therefore to be avoided. I mention this just to put those on their guard who have inverter drives. It should be pointed out that an undercut should be provided for the tool to run into, alternatively if the tool is allowed to dwell it will cut its own Vee or Acme style undercut depending on the thread being cut, it will not weaken the thread, as the root diameter is constant.

Vee threads finished in this way can be found on some commercial parts today produced on a CNC. More often than not the CNC feathers out the thread, something the old timers used to do manually. Obviously, the CNC lathe has superseded this unit today, but those with screw cutting boxes might wish to add this unit to

simplify their screw cutting.

65 January 2018



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Fair Rosamund 5" gauge designed by N.Evans

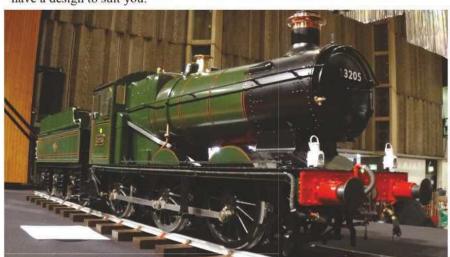


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Dean Single 5" gauge designed by P.Rich





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Shaping Up

Bill Morris describes the origins and functions of shaping machines.

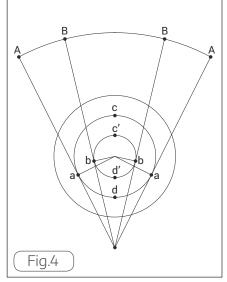
Figure 4 analyses the geometry of the shaper stroke. When the crank pin is set at position "b", the stroke takes place over the arc "B-B". When the pin is moved futher from the centre of the bull wheel to position "a", the stroke takes place over the longer arc "A-A". The cutting stroke is over the longer arc a-c-a or b-c'-b and the return stroke is over the shorter arc a-d-a or b-d'-b. Since the return stroke takes place over a shorter arc, it is also quicker. Conversely, for a given stroke rate, as the cutting arc gets longer, it has to traverse a longer distance in the same time, so the cutting speed rises.

Structure of the ram

The ram is a massive casting with generous dovetail vees below, photo 11. The front end has a circular seat machined on it for the base of the tool slide and ways on the under side to guide the upper end of the top link as the initial position of the ram is set. The upper link locked into place by the ram anchor nut. **Photograph 12** shows the very generous proprtions of the ram dovetails. Alongside the ram is a 700 mm long straight edge that I made as a set of three tested against each other, to guide my scraping when I first restored the machine 22 years ago.

The flat and the left hand edge of the dovetail slide for the ram are machined on the top of the body casting and adjustment is made on the right hand side by means of a heavy gib strip which is held down on top of the base by three stout keeper bolts whose position is adjusted by three screws and lock nuts., photo 12. When I first acquired the machine, I was puzzled by my inability to remove all shake from the ram, a very necessary condition if dovetail slides with parallel edges are to be produced on the machine. This was in spite of my tightening the gib screws hard. Eventually, I discoved that none of the gib screws had been tapped all the way through. Presumably the shaper had been used only

The slide itself is of conventional dovetail slide construction with a gib strip and locking screw.

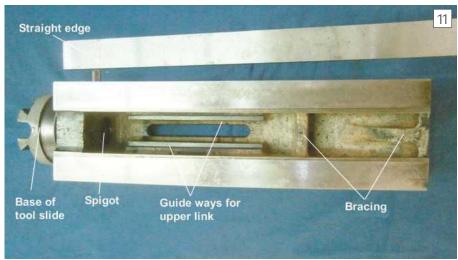


Stroke diagram

can be machined, though the width of such surfaces is limited by the travel of the slide, which is 90 mm. The slide itself is of conventional dovetail slide construction with a gib strip and locking screw. It is necessary to have a locking screw for the slide as, once the position of the slide is set, the force and vibration of the cut tends to move the slide down and increase the depth of cut without being asked. The feed screw is provided with an adjustable thimble so that the depth of cut can be monitored. As an aid to setting up for shaping truly vertical surfaces, I machined a flat on the left hand side of the tool slide, parallel to its axis of movement. This is visible in photo 19 and can be set to vertical off the machine table using a large square.

Clapper box, photo 14

The clapper box base has on it two stout shoulders through which a fixed shaft



Underside of ram.

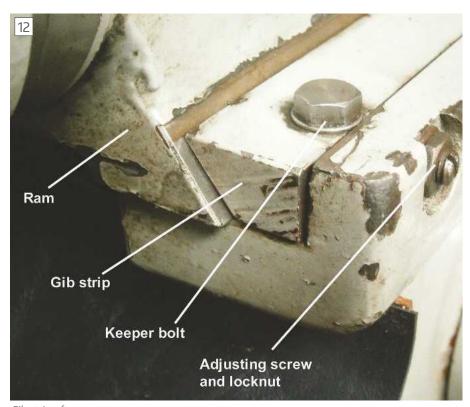
as a hack machine for this to have remained undiscovered by previous owners. Even so, adjustment of this type of strip needs some patience. The keeper bolts have to be tightened enough to allow sideways movement of the strip by the adjusting screws while not locking up the ram when finally tightened hard.

The cutting end

The tool slide, **photo 13** has a large spigot that fits into the end of the ram and is locked against the ram and prevented from rotating by a cam operated by the squared-end tilt-lock shaft. It is possible to rotate it through 90 degrees each way from the vertical so that angular surfaces

passes to form an axis about which the clapper rotates in short arcs. The clapper fits closely between the two shoulders and carries a lantern toolpost. The base is secured to the tool slide by a screw for an axis and can be set over about 15 degrees either way, when it is locked in position by the set-over locking bolt. On large shaping machines, the set over is aided by means of a worm and toothed sector.

On the cutting stroke the clapper is forced back firmly against the base by cutting forces, while on the return stroke, its inertia causes it to swing forwards about its shaft, so lifting the tool away from the work piece. At the beginning of the forward stroke, inertia again forces it back against





Tool slide and clapper box

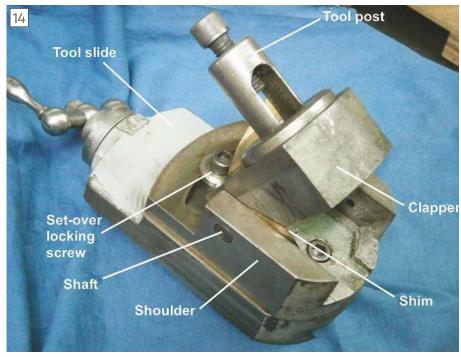
Gib strip of ram.

the base with a "clap". For good work, it is important that the clapper should be a close fit in its base, but there is no means of adjusting this, presumably because no wear was expected, given that the side faces are never moving when loaded. However, I found that there was slight sideways play, either through wear or generous manufacturing tolerances, so I inserted a thin brass shim to take up the play. In some jobs, it is necessary to lock the clapper box and I drilled and tapped a hole through one of the shoulders for a locking screw.

Cross table feed

Now that we have the ram and its attached tool reciprocating, we can turn attention to the means of feeding the workpiece across below the tool to generate a surface,

photo 15. The end of the bull wheel shaft has a driving disc attached to it which rotates with the bull wheel and acts as a crank. A tee slot is machined across the disc to accept a tee bolt that carries a hardened drive pin. The drive pin is locked into its chosen position by a clamp. Running on the drive pin is a two-piece connecting link that is adjustable in length according to whether the table is high or low, and the far end of the link runs on another crank pin in the form of a shouldered bolt. Larger machines usually have a sun and planet gear, each with an equal number of teeth interposed between the bull wheel shaft and the driving disc, so that the centre distance between the driving disc and crank remains constant. As the driving disc rotates, the connecting link oscillates back and forth, providing that the drive pin is somewhere other than



Clapper box details

centred, and this causes the crank at the other end of the connecting link to rock back and forth. The crank has a stout spring-loaded pawl that can be rotated to drive the ratchet wheel in either direction and which can be withdrawn from the ratchet wheel to stop the feed. It is important that the feed should take place on the non-cutting stroke of the ram. The feed per revolution is increased by moving the crank pin further out along the driving disc and four steps of feed are possible, between 0.006 in to 0.025 in

(0.15 to 0.63 mm) per stroke of the ram. The mechanism is shown exploded in **photo 16**.

The ratchet wheel is pinned to the threaded cross shaft which runs in bearings in the apron and passes through a feed nut. This latter carries a spigot which sits in a hole in the back of the table and drives it along the cross rails machined on the apron. The cross shaft has a squared end for a handle used to move the table by hand and the other end has a fine thread so that the shaft

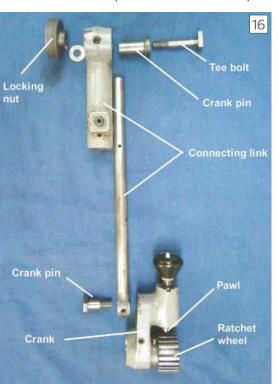
Ideally, both keepers should be equipped with soft-faced locking screws, an omission I have planned to make good for 22 years.

can be adjusted by means of a nut and locknut, to have enough drag to prevent the ratched wheel going backwards as the pawl passes over the teeth of the ratchet wheel. **Photograph 17** shows the details. Note how a portion of the feed screw is bare of threads at each end so that feed automatically stops if the operator is distracted at the end of a run.

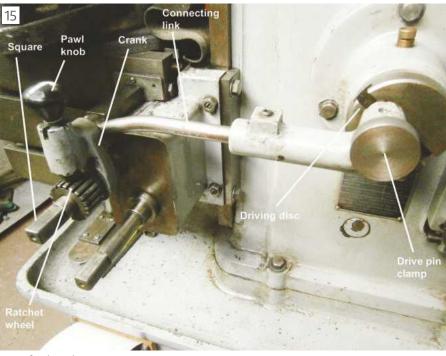
The table hangs, as it were, on the cross rails of an apron, and gib strips top and bottom at a right angle to each other remove all play. It is usual for shaping machines to have rectangular cross rails, as dovetail ways would have a wedging action under the intermittent load.

Vertical table feed

The squared end of the vertical feed shaft has been noted in photo 4, and photo 18 shows some details. The other end of shaft carries a helical "skew" gear pinned to it and this gear drives another one at right angles to it. Though free to rotate, the latter gear is held captive in the apron by two locknuts and is threaded for a vertical drive shaft, itself held captive in the base of the body



Cross feed mechanism exploded.



Cross feed mechanism

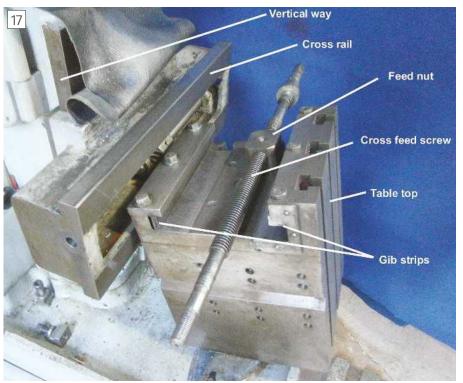
and locked against rotation. Thus, when the skew gears rotate, the vertical one climbs or descends the stationary vertical drive shaft, carrying the apron with it.

The apron is carried on rectangular vertical ways machined on the face of the body and are made accurately at right angles to the plane of the ram movement. It is held against the face of the ways by substantial keeper plates on each side and there is an adjustable gib stip on the right hand side, photo 19. Since the slides do not usually move when under cutting load, no wear is to be expected, so that once the keepers are

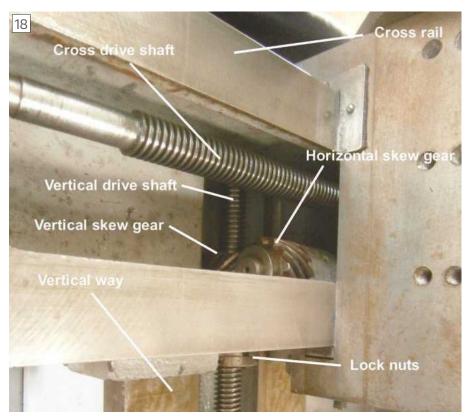
adjusted using shims and rocking taken out by means of the gib, they should need no further attention. Note that in photos 18 and 19 the original scraper marks are still clearly visible on the table slides. Like the table cross movement, vertical movement should be adjusted to be a little stiff so that movement under load is reduced to a minimum. Ideally, both keepers should be equipped with softfaced locking screws, an omission that I have planned to make good for 22 years.

The table

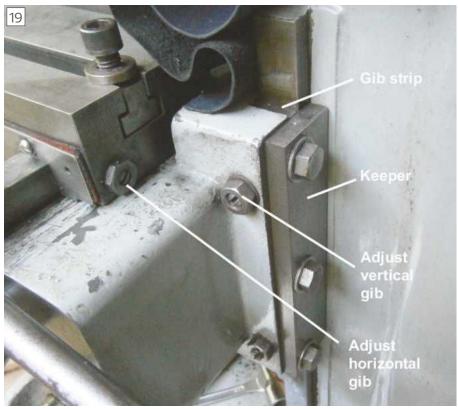
The table, which measures 260 mm (10.2



Cross slide feed screw and nut.



Elevation of apron.



Gib strips of apron.

in) long, 175 mm (6.9 ins) wide and 190 mm (7.5 in) high has already appeared in several of the photos. A ribbed box casting, it has tee slots on the top and right hand side with a vertical vee on the left hand side for attaching shafts. What is not easily apparent is that it is in two parts, a thinner part that connects with the apron ways and

the main part that is secured to the other via a central spigot and three large securing bolts, **photo 20**. This arrangement allows the table to be rotated through a limited range of angles or even to be re-positioned so that a different face is uppermost. This is not something that I would recommend to be done except in case of dire need, as

I took a possibly easier way out by screwing a surface-ground wear strip to it and carefully shimming it to the correct contour.

getting the table back to its normal position is rather like adjusting a lathe tailstock when the set-over has been disturbed: even with the aid of a dial indicator one tends to move back and forth, eluded by the happy "just right" central position.

Bolted to the underside of the table is a fitting that carries a support leg to resist some of the downward cutting forces. It is locked in position by a bolt bearing against a flat machined on the leg and the lower end runs on a guide surface machined on the base. Inevitably, this surface wears concave with repeated hammering from the cutting forces and then, if adjusted to run on the concave part, it tends to raise the table a little in other parts, so that the face of a workpiece may end up convex. The surface could of course be filed and scraped flat and parallel to the table movement, but I took a possibly easier way out by screwing a surface-ground wear strip to it and carefully shimming it to the correct contour.

In the next article, Bill will describe how he set up and aligned the shaper. ■



Table adjustments.

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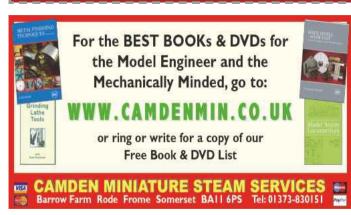




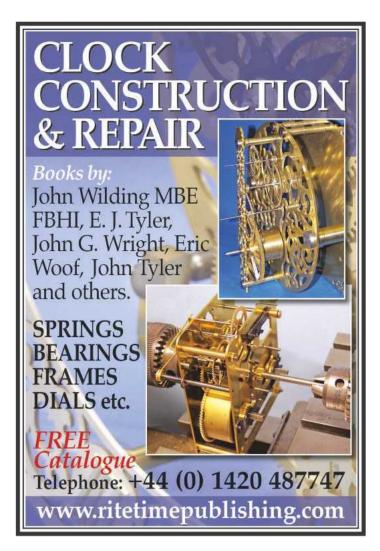
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